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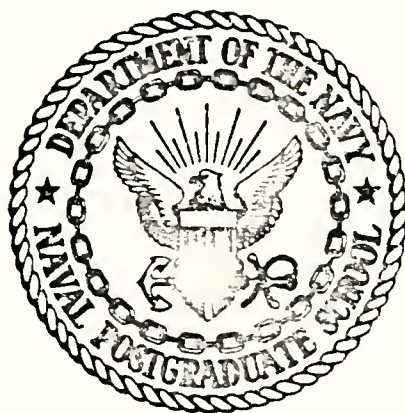
VALIDATION OF THE NONLINEAR SIX DEGREE OF  
FREEDOM MATHEMATICAL MODEL OF THE XR-3  
CAPTURED AIR BUBBLE SURFACE EFFECT SHIP  
IN CALM WATER

George Thomas Forbes

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# NAVAL POSTGRADUATE SCHOOL

## Monterey, California



# THESIS

VALIDATION OF THE NONLINEAR SIX DEGREE OF  
FREEDOM MATHEMATICAL MODEL OF THE XR-3  
CAPTURED AIR BUBBLE SURFACE EFFECT SHIP  
IN CALM WATER

by

George Thomas Forbes

December 1974

Thesis Advisor:

A. Gerba, Jr.

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Validation of the Nonlinear Six Degree of Freedom  
Mathematical Model of the XR-3 Captured Air Bubble  
Surface Effect Ship in Calm Water

by

George Thomas Forbes  
Lieutenant Commander, United States Navy  
B.S., United States Naval Academy, 1965

Submitted in partial fulfillment of the  
requirements for the degree of

MASTER OF SCIENCE IN ELECTRICAL ENGINEERING

from the

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December 1974



## ABSTRACT

The non-linear, six-degree-of-freedom, mathematical model of the XR-3 captured air bubble surface effect ship is validated by comparison of measured testcraft performance with computed variables in the digital computer simulation. Data processing methods implemented on hybrid and digital computers are presented. Improvements are made on the structure of the mathematical model of the XR-3 by program subroutine modifications and justification is given for the changes made. Close agreement is obtained between measured and computer simulated variables over a variety of operating conditions in calm water.



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## TABLE OF SYMBOLS AND ABBREVIATIONS

ac	alternating current
A-to-D	analog to digital
CAB	Captured Air Bubble
CG	Center of Gravity
$\zeta$	Center Line
db	decibels
dc	direct current
deg	degrees
D-to-A	digital to analog
FXPWAV	drag force in direction opposite to craft motion due to drag between pressurized air and water surface
g	gravitational acceleration
Hz	Hertz
kts	knots
lb	pounds
NPS	U.S. Naval Postgraduate School
NSRDC	Naval Ship Research and Development Center
RMS	Root Mean Square
psf	pounds per square foot
sq ft	square feet
$\rho$	density
$\delta$	rudder angle
$\theta$	pitch angle
$\phi$	roll angle



$\psi$	yaw angle
plenum	cavity beneath the wet deck of the XR-3, formed by the sidewalls and the bow and stern seals, into which pressurized air is blown
hump speed	speed at which testcraft overcomes large low velocity drag and begins to operate on the cushion of captured pressurized air



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## I. INTRODUCTION

### A. BACKGROUND

The Captured Air Bubble surface effect ship presents a new concept in shipping for the surface force of the U.S. Navy. Within a few years these vessels, supported partially by a cushion of air and partially by the more conventional hull buoyancy forces, will be joining the Fleet. In preparation for that event it is of extreme importance for detailed studies to be undertaken so that the capabilities and limitations of such vessels may be fully understood.

The term surface effect ship applies to a broad spectrum of different types of vessels. Among them are the Air Cushion Vehicle (ACV), the Ground Effects Machine (GEM), the Semi-Submerged Ship (SSS), the Captured Air Bubble (CAB), and others. This study is concerned with the CAB surface effect ship.

The Captured Air Bubble craft consists of two rigid sidewalls which resemble catamaran hulls and flexible seals between the water surface and hull structure across the bow and stern of the craft. The enclosed volume is a plenum chamber into which air is blown by a lift fan system. The pressure in the plenum chamber acting over the area of the plenum provides a lift force sufficient to support a large proportion of the total craft weight. The remainder



of the supporting force is made up by conventional hydrodynamic forces acting on the sidewalls, plus some lift forces due to the bow and stern seals and aerodynamic lift at higher operating speeds.

In the "on bubble" mode of operation, at the higher operating speeds, approximately two-thirds of the total craft weight is supported by the air cushion, and therefore relatively shallow sidewall immersion is required to support the remaining weight. The shallow draft produces a lower hydrodynamic drag and thus higher speed for a given power than could be obtained for a displacement hull.

The XR-3 is a CAB surface effect ship of approximately three tons displacement. The XR-3 was built by the Naval Ship Research and Development Center (NSRDC) in 1966. Following periods of testing by NSRDC, Annapolis Division NSRDC, and Aerojet-General Corporation, the XR-3 was delivered to the Naval Postgraduate School (NPS), Monterey, California in March 1970 for the investigation of basic and advanced surface effect ship technology.

In addition to the XR-3 there exist other CAB test craft. Among these are the Aerojet-General 100-A and the Bell Aerospace Systems 100-B, both of approximately 100 tons displacement. These two vessels were constructed as prototypes of a 2,000 ton ship. To date speeds in the 80-knot range have been attained by these vessels.

Under a U.S. Government contract, Oceanics Incorporated developed a digital computer simulation of the



CAB ship loads and motions for the Surface Effect Ship Project Office (SESP0) in Washington D.C. This loads and motions program with the mathematical model of the Bell Aerospace Systems 100-B with six-degrees-of-freedom has been in use at the W.R. Church Computer Center at NPS since October 1972.

In December 1973, LCDR. D.G. Leo, USN and LT. R. Boncal, USN produced a mathematical model with six-degrees-of-freedom of the XR-3 test craft derived from the above-mentioned simulation model of the 100-B (Ref. 1). The modular construction of the 100-B simulation program facilitated the re-modeling of the program where necessary to fit the design differences between the 100-B and the XR-3.

## B. OBJECTIVES

It is the objective of this thesis to validate the non-linear, six-degrees-of-freedom, mathematical model of the XR-3 CAB test craft in a comprehensive manner by direct comparison between instrument-measured variables on the XR-3 and computed variables produced by the simulation programs. In the process of carrying out this objective, subroutine modifications were made to the simulation program to improve on the structure of the simulation model and justification is given in the sections that follow for the changes that were made.

The data taken on the XR-3 measured in real-time, analog fashion using FM modulation was filtered, converted to



digital form, and processed in such a manner that it could be interfaced directly with the simulation program and a time history of true differences for each variable could be produced at each operating condition.

The present study is limited to operation of the test craft in calm water conditions at the test site located at Lake San Antonio Reservoir, California. The range of operation of the test craft includes:

1. Straight runs at various speeds with various locations of the center of gravity. The center of gravity was shifted by placement of two 125 pound water tanks at different locations on the deck of the test craft.
2. Straight runs at various speeds in an unladen condition.
3. Runs made at various speeds with various rudder angles applied to validate turning performance.



## II. COLLECTION OF DATA

### A. INSTRUMENTATION ON THE XR-3

In order to support the continuing studies being undertaken at the Naval Postgraduate School on Captured Air Bubble vessels, the XR-3 has been instrumented with devices capable of measuring and recording time histories of many different variables for later, post-run analysis (Ref.2). The general configuration of the XR-3 is shown in Figure 1. Table I shows a listing of the measurable parameters, the range of measurement, and the accuracy with which the measurements may be made. The locations of the measuring instruments are shown in Table II. The measured data are recorded on a Pemco Model 120-B magnetic tape recorder which features 14 tracks for recording data and an edge track for voice annotation during measurement runs. Each of the 14 tracks on the tape recorder is capable of recording  $\pm 1$  volt RMS with a tolerance of  $\pm 0.5\%$ .

### B. POWER SUPPLIES

The tape recorder is powered from a 110 volt 60 cycle auxiliary power unit, located on the aft weather deck as shown in Figure 1., through a Pemco a.c. to d.c. converter which provides a 26 volt d.c. power source. The three accelerometers for measuring vertical, lateral, and fore-and-aft accelerations are powered from a 12 volt storage battery through a d.c. to d.c. converter which provides a



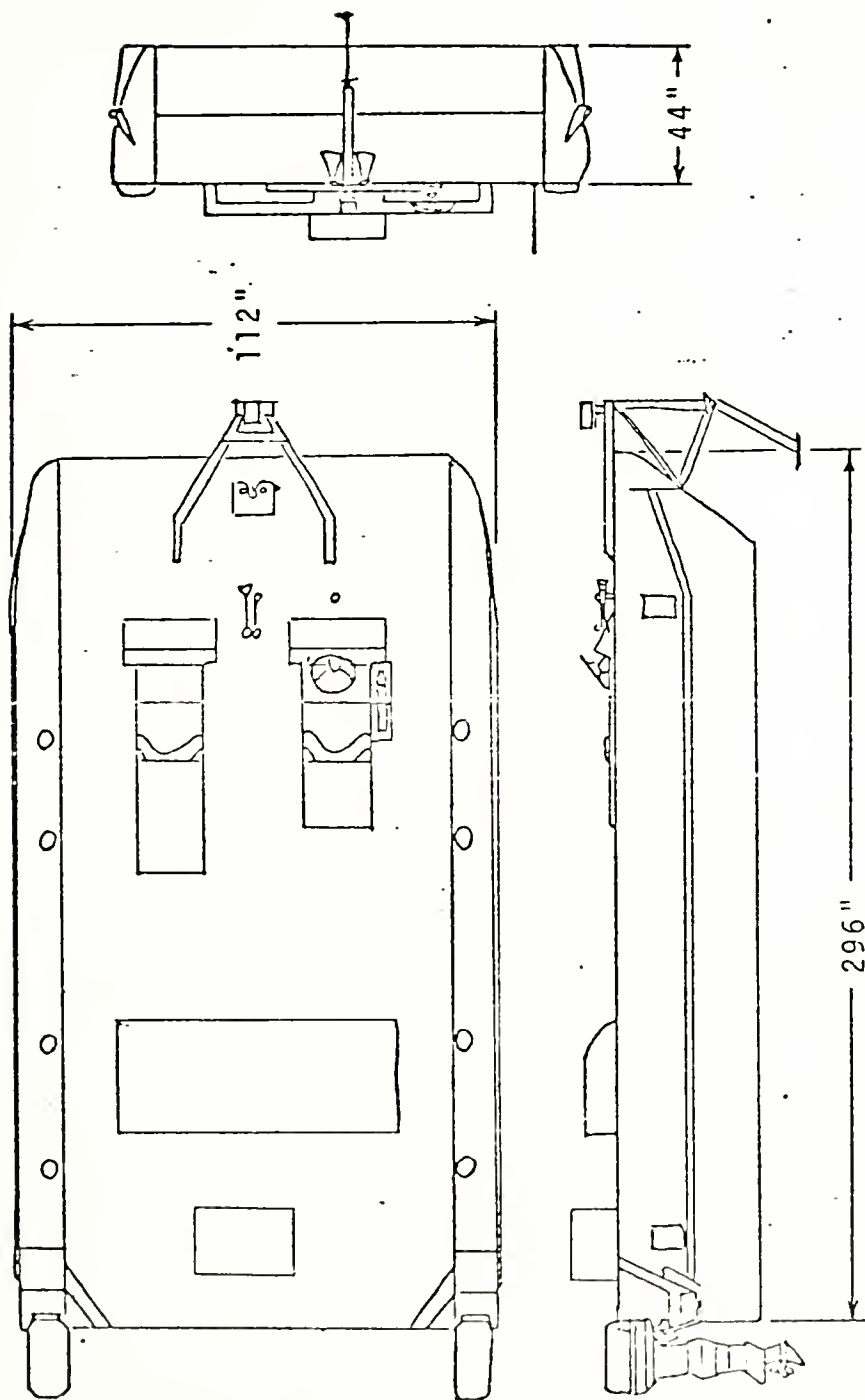


FIGURE 1. GENERAL CONFIGURATION OF XR-3



Table I. XR-3 Measurable Parameters

Parameter	Simulation Program Name	Range	Accuracy
Port Thrust	THSTP	0-500 lbs	$\pm 5$ lb
Starboard Thrust	THSTS	0-500 lbs	$\pm 5$ lb
Velocity	VEL	0-40 kts	$\pm 1$ kt
Height	None*	$\pm 2$ feet	$\pm 0.1$ in
Bowseal Press.	PBARB	0-60 psf	$\pm 0.5$ psf
Plenum Press.	PBAR	0-60 psf	$\pm 0.5$ psf
Sternseal Press.	PBARS	0-60 psf	$\pm 0.5$ psf
Pitch Angle	THETAR	$\pm 15$ degs	$\pm 0.5$ deg
Roll Angle	DPHI	$\pm 15$ degs	$\pm 0.5$ deg
Yaw Angle	DPSI	$\pm 180$ degs	$\pm 0.5$ deg
Pitch Rate	PDEG	$\pm 30$ degs/sec	$\pm 0.5$ deg/sec
Roll Rate	QDEG	$\pm 30$ degs/sec	$\pm 0.5$ deg/sec
Yaw Rate	RDEG	$\pm 30$ degs/sec	$\pm 0.5$ deg/sec
Rudder Position	DELRS	$\pm 45$ degs	not available
Longitudinal Acceleration	None	$\pm 0.2g$ units	not available
Lateral Acceleration	ACCLAT	$\pm 0.2g$ units	not available
Vertical Acceleration	ACCEL(3)	- 0.8 to +1.2g	not available

\*Height is used to compute Draft as explained in text.



Table II. Location of Sensors

Sensor	Distance Forward of Transom	Distance from Center Line
Pressure Transducers		
Bow Seal	18'4"	£
Plenum	12'4½"	£
Stern Seal	1'6"	£
Velocity	21'9" 4'9½" down from deck	£
Height	24'1" 6" down from deck	£
Gyros		
Pitch	12'6"	2'4½" Port
Roll	13'	2'4½" Port
Yaw	12'6"	2'4½" Port
Port Thrust	0	5'6" Port
Starboard Thrust	0	5'6" Starboard
Vertical Accelerometer	13'6½"	1'9½" Port
Lateral Accelerometer	13'6"	1'9" Port
Longitudinal Accelerometer	13'5½"	1'8½" Port



28 volt d.c. supply. The three gyros which measure pitch, roll, yaw, pitch rate, roll rate and yaw rate are powered by the 12 volt storage battery. The gyros also receive a 1 volt d.c. excitation signal from the 110 volt a.c. power supply fed through an a.c. to d.c. converter.

The height sensor mounted forward of the bow is powered directly from the 110 volt a.c. auxiliary power unit. The height measurement signal is converted to a  $\pm 1.0$  volt d.c. signal by a height sensor conditioner. The velocity probe, mounted on the same assembly as the height sensor, extends into the undisturbed water forward of the testcraft. The 28 volt d.c. power source for the velocity probe is the 12 volt battery through the d.c. to d.c. converter. The rudder position measurement is made by means of a load cell which receives a 12 volt d.c. supply from the battery.

The two load cells for measuring port and starboard thrust and the three pressure transducers for measuring bow seal, plenum, and stern seal pressures are all powered by a 28 volt d.c. supply from the 12 volt d.c. storage battery through the d.c. to d.c. converter. All five units also receive a 5 volt d.c. excitation signal from an amplifier-transducer package.



### III. DATA PROCESSING

#### A. ANALOG TO DIGITAL CONVERSION

To provide measurements for validation of the mathematical model, data-gathering runs were made with the XR-3 testcraft on four different days at the Lake San Antonio, California test site. The data was recorded on magnetic tape using FM modulation, then processed into a suitable form for comparison with corresponding values computed in the XR-3 simulation program on the IBM 360/67 Digital Computer.

The data was converted from analog to digital form on an XDS-9300/CI-5000 hybrid computer at the NPS Computer Laboratory. From previous experience in data reduction by the XR-3 Research Group in the Aeronautical Engineering Department at NPS, it was found that filtering of the analog signal was required to remove unwanted high frequency noise from the recorded data. To provide this required filtering six Krohn-Hite digitally-tuned filters were assembled so that six tracks of recorded data could be processed simultaneously.

#### B. DESCRIPTION OF EQUIPMENT

The analog tape containing raw data from XR-3 test runs was mounted on a Honeywell Tape Recorder/Reproducer, Model 96 for playback. Connections were made through trunk lines to lead the output from the six selected tracks



to the COMCOR CI-5000 Analog Computer as shown in Figure 2. Each channel of recorded data was then passed through an amplifier with a gain of 5 before being led out of the CI-5000 to one of the filters. The filters were operated in the low pass-maximally flat mode which provided a four-pole Butterworth response with an attenuation of 24db per octave from the cut off frequency. Cut off frequencies were set at 10 Hertz for all channels except port and starboard thrust which were set at 1.0 Hertz. Each signal at the output of its respective filter was led back into the CI-5000 for another amplification by a gain factor of ten. A Brush 8-Channel Recorder was also patched into the system at this point so that each of the six selected data tracks could be continuously monitored. Figure 2 shows the signal flow patch through the hybrid computer system for analog-to-digital conversion.

For analog-to-digital conversion, digital-to-analog conversion, and other applications, the CI-5000 Analog Computer and the XDS-9300 Digital Computer are interconnected through trunks. For A-to-D conversion in this application a sampling frequency of 200 Hz was chosen. In steady-state calm-water runs with the XR-3 none of the measured parameters can be expected to vary at frequencies greater than 10 Hz. Therefore, selection of a 200 Hz sampling frequency more than satisfies the requirements of the Sampling Theorem.



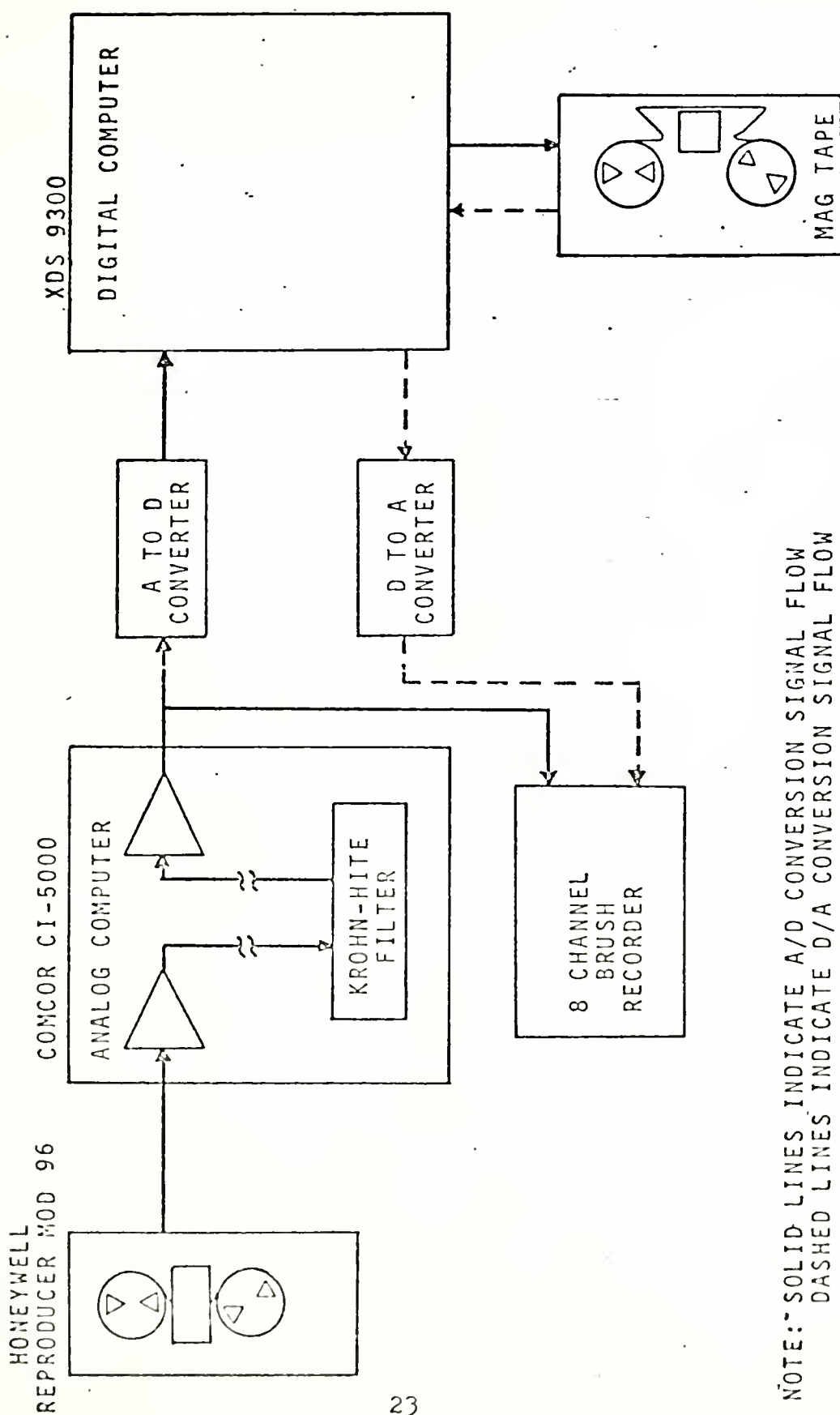


FIGURE 2. SIGNAL FLOW DURING ANALOG TO DIGITAL CONVERSION



The first step in the A-to-D process was to zero all possible bias errors in the system. Calibration steps are recorded on separate channel strips on the analog data tape which indicate zero and maximum signal readings for each sensor. Bias potentiometers at the input of the first stage amplifier on the CI-5000 were adjusted to properly zero all channels during the pre-test run calibration of the XR-3 sensors. Each signal was monitored on a digital voltmeter during the calibration procedure.

Execution of the FORTRAN program listed in Appendix A on the hybrid computer system enabled selective conversion from analog to digital form of specific time periods of analog data. Continuous monitoring of the voice edge track on the data tape provided a reference as to what the XR-3 conditions were at all times. After each file of data had been digitized and written on the digital magnetic tape, the tape was re-wound and that file most recently recorded was run through the digital-to-analog conversion. The D-to-A signal was monitored on the Brush Recorder and compared with the analog signal to verify the validity of the conversion process. The finished product of the A-to-D conversion was a reel of 7-track digital tape consisting of many files of digital data. Each file on the tape contained a time history of six selected variables measured for a specific operating condition on the XR-3.



### C. INTERFACE WITH IBM SYSTEM 360/67

Introduction of the 7-track tapes into IBM System 360/67 at the W.R. Church Computer Center at NPS entailed some further processing of data. In the XDS 9300 a binary number is represented by considering its octal representation, made up of 3-bit digits, whereas in the IBM 360 the same number is represented by hexadecimal, made up of 4-bit digits. As an example of this difference, a decimal number  $(668)_{10}$  is  $(1234)_7$  octal and  $(29C)_{16}$  hexadecimal. It was necessary, then, to write a FORTRAN program to read each record in a file from the 7-track tape, make the conversion from octal to hexadecimal, store the data in hexadecimal form on a temporary storage disk, and to print out a portion of each record in decimal form. A listing of the program is included as Appendix B. The program uses the pre-compiled assembler language subroutine FORM to convert the data to its hexadecimal representation. Figure 3 shows the flow of information through the IBM System 360/67 computer in this validation.

The printed output from the conversion program is representative of the data in its original measurement form multiplied by a gain factor of 50 in the A-to-D conversion process. At this point in the process the numbers printed out were compared with the signals recorded on the Brush Recorder during A-to-D conversion to insure that the accuracy of the data had been preserved. This was indeed the case with the exception of some small amplitude,



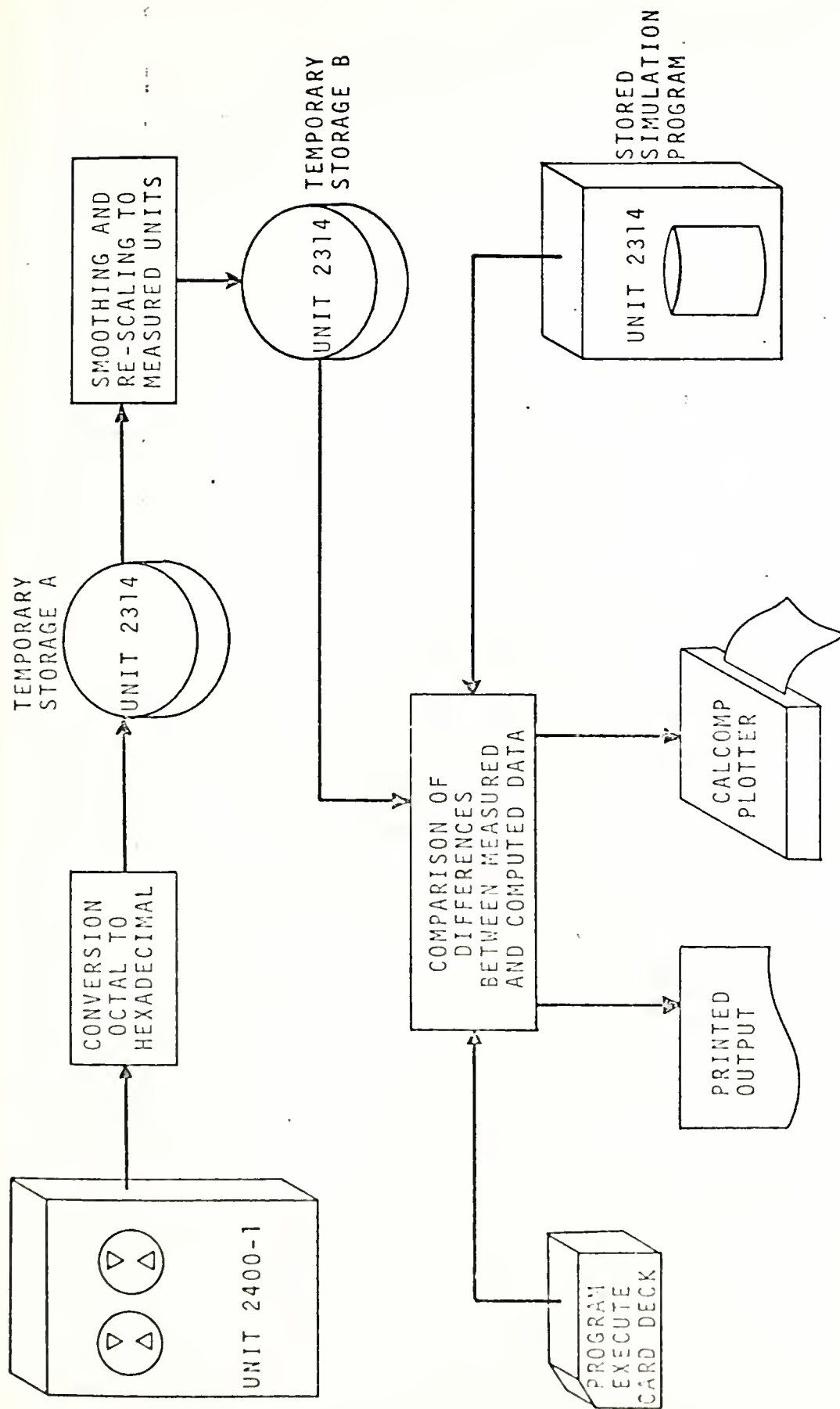


FIGURE 3. INFORMATION FLOW THROUGH IBM SYSTEM 360/67



high-frequency fluctuations in the digitally reproduced data which did not appear to be present on the Brush Recorder tapes.

The final phase in data processing was to recover the measured data into the units which correspond with the measurement, i.e. pounds of thrust, degrees of pitch angle, knots of velocity, etc. to facilitate direct comparison in the XR-3 simulation model. To accomplish the recovery of data it was necessary to read the converted data from the temporary storage disk, multiply each set of variables by the inverse of the appropriate scale factor used when recording the data on the testcraft, divide out the gain factor of 50 introduced in the A-to-D process, and store the result on a temporary disk for later access by the XR-3 simulation program.

The height measurement made on the XR-3 during data collection runs does not have an immediately available counterpart in the XR-3 program as indicated in Table 1. A very close approximation to draft can be obtained from the height measurement through suitable scaling, however. The calculation of draft in the XR-3 simulation program is made with reference to draft at the center of gravity of the craft. The height measurement is made at a sensor located 191" forward of the reference center of gravity and 6.375" down from the deck level of the test craft (see Figure 1). The measurement of the height of the sensor above the surface of the water will vary as the



craft pitches up and down at the bow. Since pitch angles are, for the normal operating range, less than five degrees, the small angle approximation may be made for the sine of pitch angle. The draft measurement is synthesized by solution of the following relationship:

$$\text{DRAFT} = \text{SH} + \text{Z} - \text{HT} + \text{D} \cdot \sin \theta$$

where DRAFT = Water height above keel at the center of gravity

SH = Height of sensor above CG = 7.145"

Z = Distance of CG above keel = 30.48"

HT = Measured height of sensor above water surface

D = Distance of height sensor forward of CG = 191"

D \* SIN  $\theta$  = Variation of measured height due to pitch angle.

A FORTRAN program was written to accomplish the process of re-scaling to measured units and to provide the close approximation to a draft measurement. A time index was also included in the program to facilitate plotting each variable versus time on a CALCOMP plotter. This feature proved to be valuable as a final step in the process because each variable could be closely examined in graphical form prior to accessing the data by the XR-3 simulation program. It was at this point in the procedure that some difficulties were encountered in early attempts at signal processing, as described in the following section.

#### D. FREQUENCY COMPONENTS ENCOUNTERED IN DATA

Examination of the CALCOMP plots of the digitally reproduced measurement data revealed significant small



amplitude, high frequency noise impressed on the measurement signal. The noisy signal was not immediately evident on the Brush Recorder tape, however on close inspection it was apparent that some noise was passing through the filters. Figures 4,5,6, and 7 are representative CALCOMP plots of processed measurement data of thrust, pitch angle, velocity and plenum pressure respectively. These graphs are included to show the effect of noise on the processed data.

The source of noise present in the measurement data has not been established and can only be rationalized to be a combination of several possible environmental factors. First of these is vibration aboard the XR-3 testcraft from the twin engine propulsion system and fan drive system. Second, the testcraft is rarely run in completely glass-calm water conditions at the test site. Surface disturbances are nearly always present due to numerous pleasure craft, wind-induced ripples on the lake, and occasionally, the wake of the testcraft itself. Such disturbances can have a pronounced effect on the motion of the XR-3. Finally, 60-cycle power supply interference can be assumed to be present due to the antenna effect of unshielded wiring both in the testcraft and in the NPS Computer Laboratory.

#### 1. Elimination of Unwanted High Frequencies

Recognizing that the noisy data rendered it all but unusable for any meaningful attempt at validation, methods were sought to eliminate the noise and to obtain a "clean"



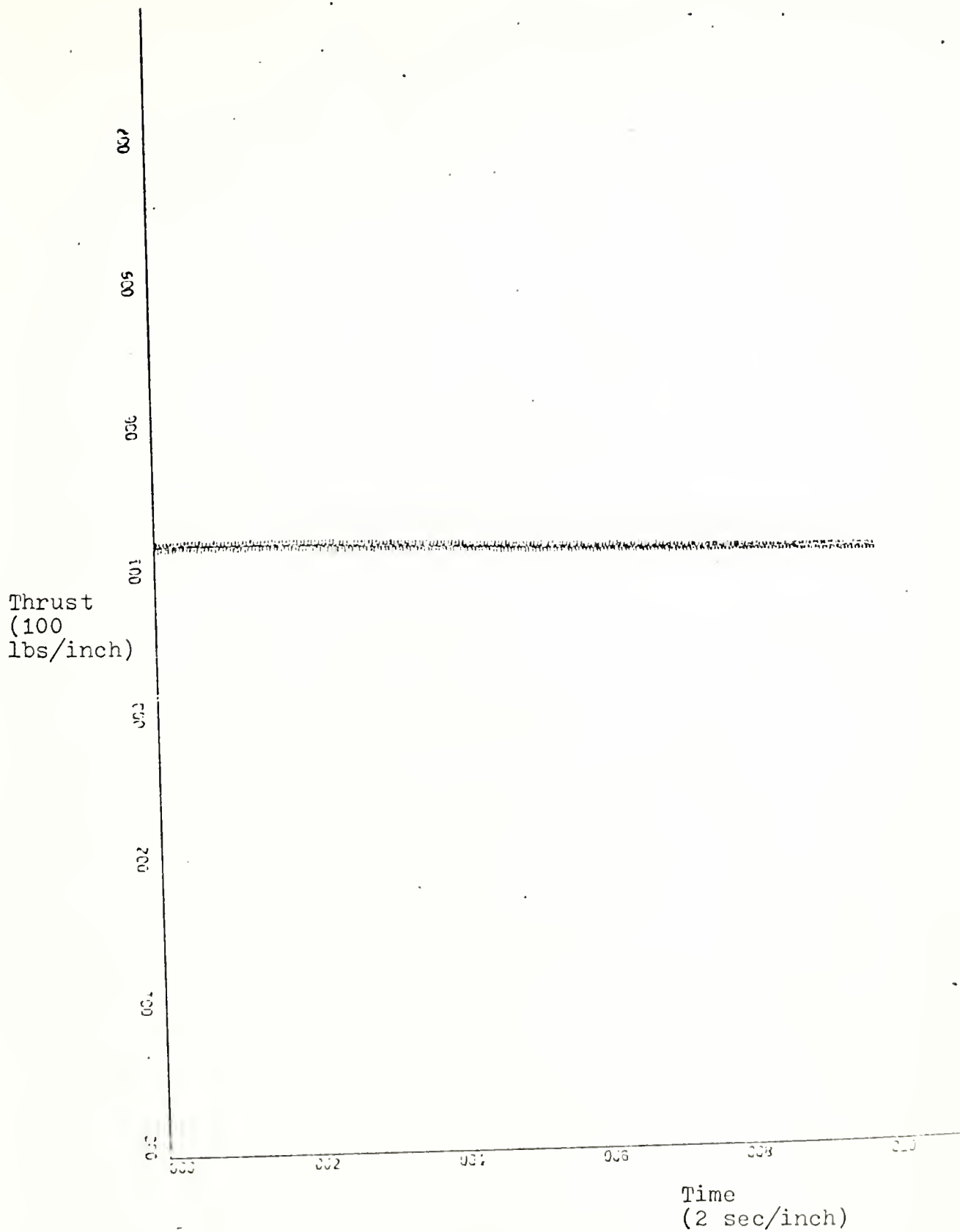


Figure 4. . Plot of Thrust Vs. Time



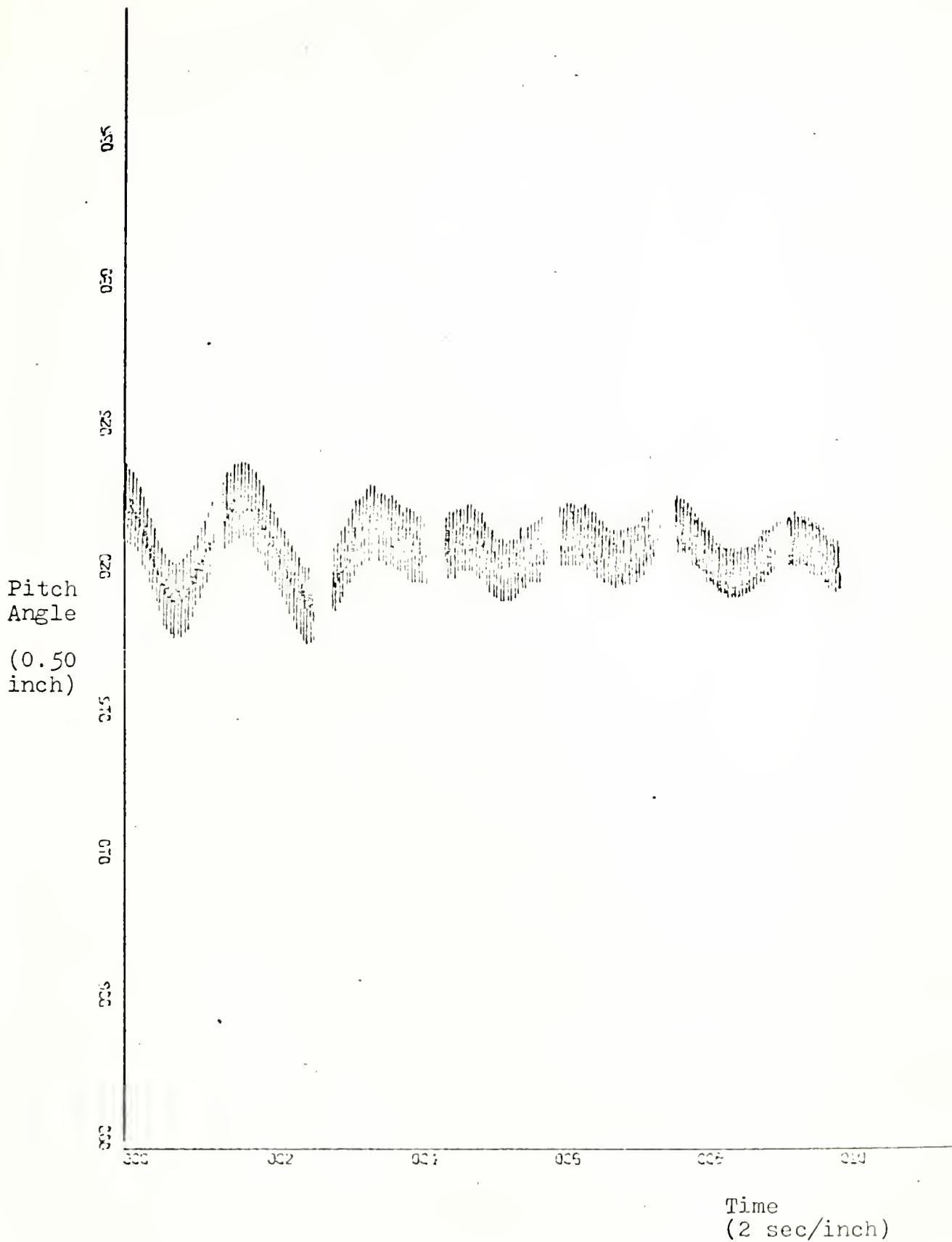


Figure 5. Plot of Pitch Angle Vs. Time



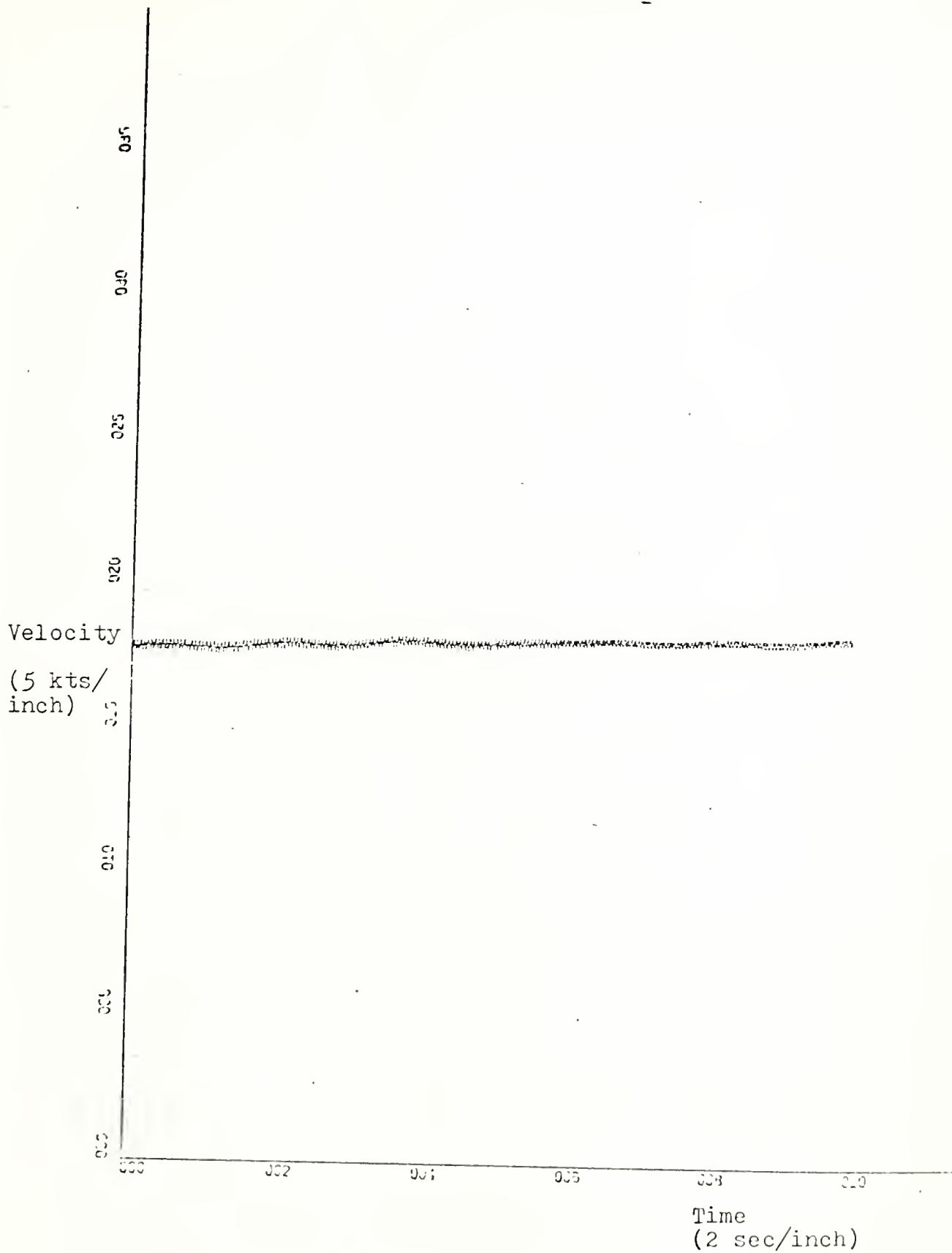


Figure 6. Plot of Velocity Vs. Time



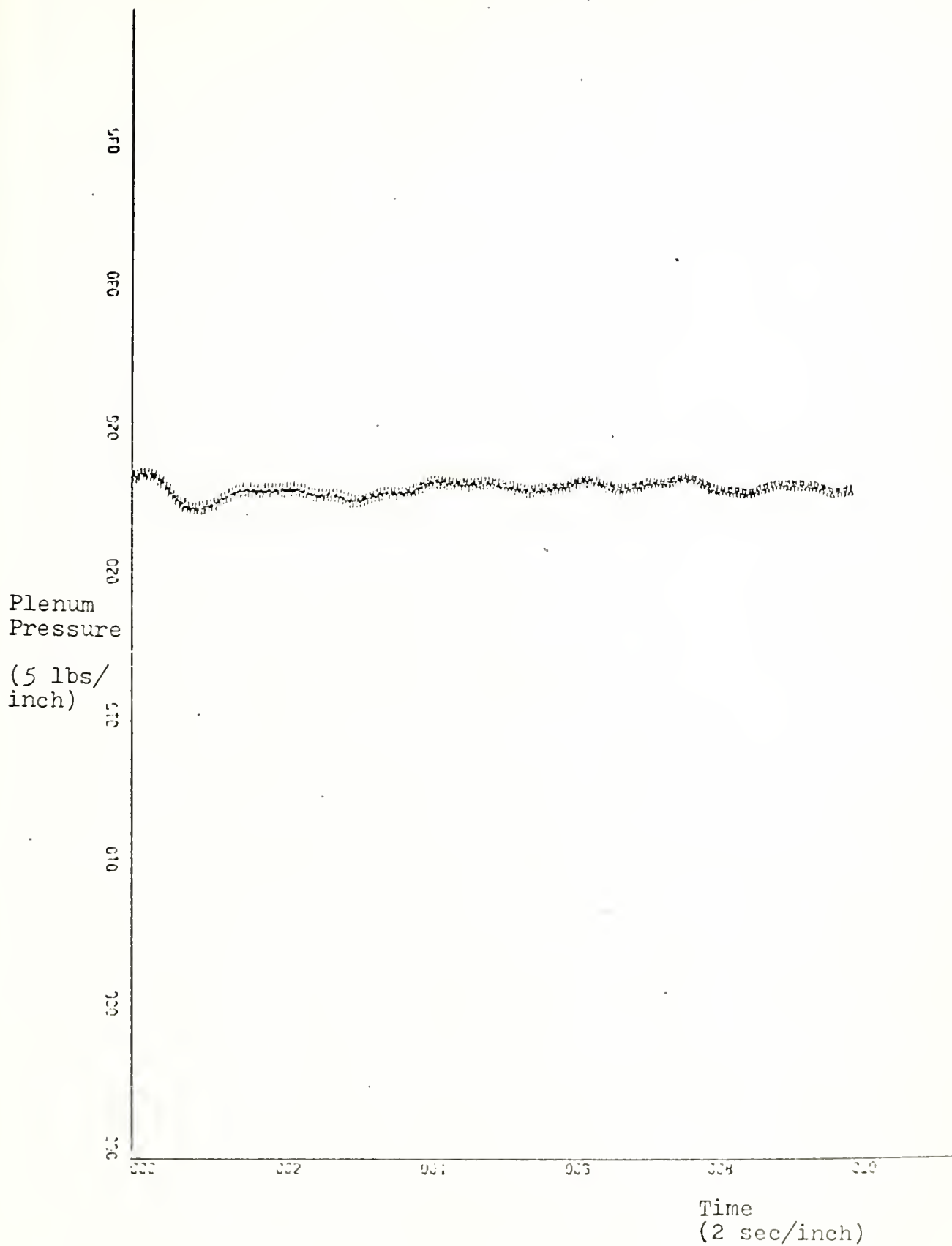


Figure 7. Plot of Plenum Pressure Vs. Time



signal and, at the same time, to preserve the validity of the actual measurement. The first effort was to filter at a lower frequency. The result was displeasing for, while the magnitude of the impressed noise was somewhat reduced, lower frequency oscillations which represented actual craft motions were nearly eliminated. The next possible solution was to employ two filters in cascade, thereby obtaining a low-pass filter with 48 db per octave attenuation above the cut off frequency. This procedure accomplished the main objective of removing virtually all the noise and passing only signals representative of the craft motions. The disadvantage of this method was that only three instead of six measurements were now possible because of the hardware limitations and synchronization became an insurmountable problem.

The third possibility of removing the noise from the measurement signal was to proceed on the assumption that the noise was gaussian and white and to employ a smoothing or time-averaging technique. The technique employed was to process the data as originally set forth and then, in the final scaling process on the digital computer, to obtain a moving time average. The algorithm implemented on the digital computer was to calculate the sum of the first ten points in the time history of a measured parameter, divide the sum by ten and call the resultant figure the first point in the time history. Next, a counter was incremented by five and the process was repeated to obtain



the next point. In this manner the data is reduced from 200 samples per second to 20 samples per second. The overlapping smoothing technique tends to preserve low frequencies. By comparison there were insignificant differences (less than two per cent) between this smoothing process and the aforementioned cascade filtering. The advantage realized was a more economical use of available equipment (filters) and a great savings in time required for data processing.

A listing of the program used for re-scaling the data to its original measurement form and including the smoothing routine is included as Appendix C. Figures 8, 9, 10 and 11 are CALCOMP plots of smoothed measurement data of thrust, pitch angle, velocity and plenum pressure respectively. By comparison with the measurement data plotted in Figures 4,5,6, and 7, it is evident that the moving time average smoothing technique has preserved the measurement information of value and has eliminated the impressed noise.



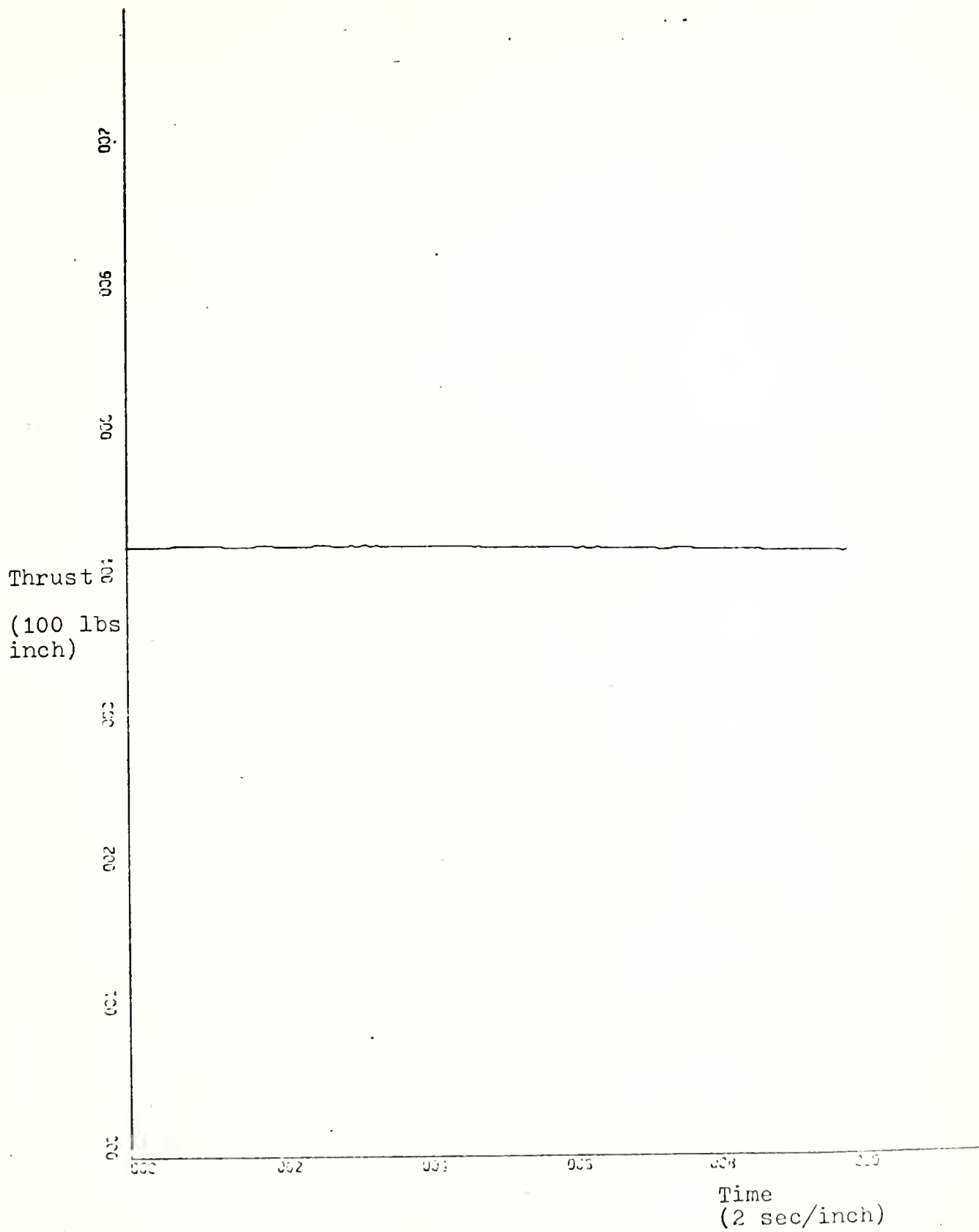


Figure 8. Plot of Thrust Vs. Time After Smoothing



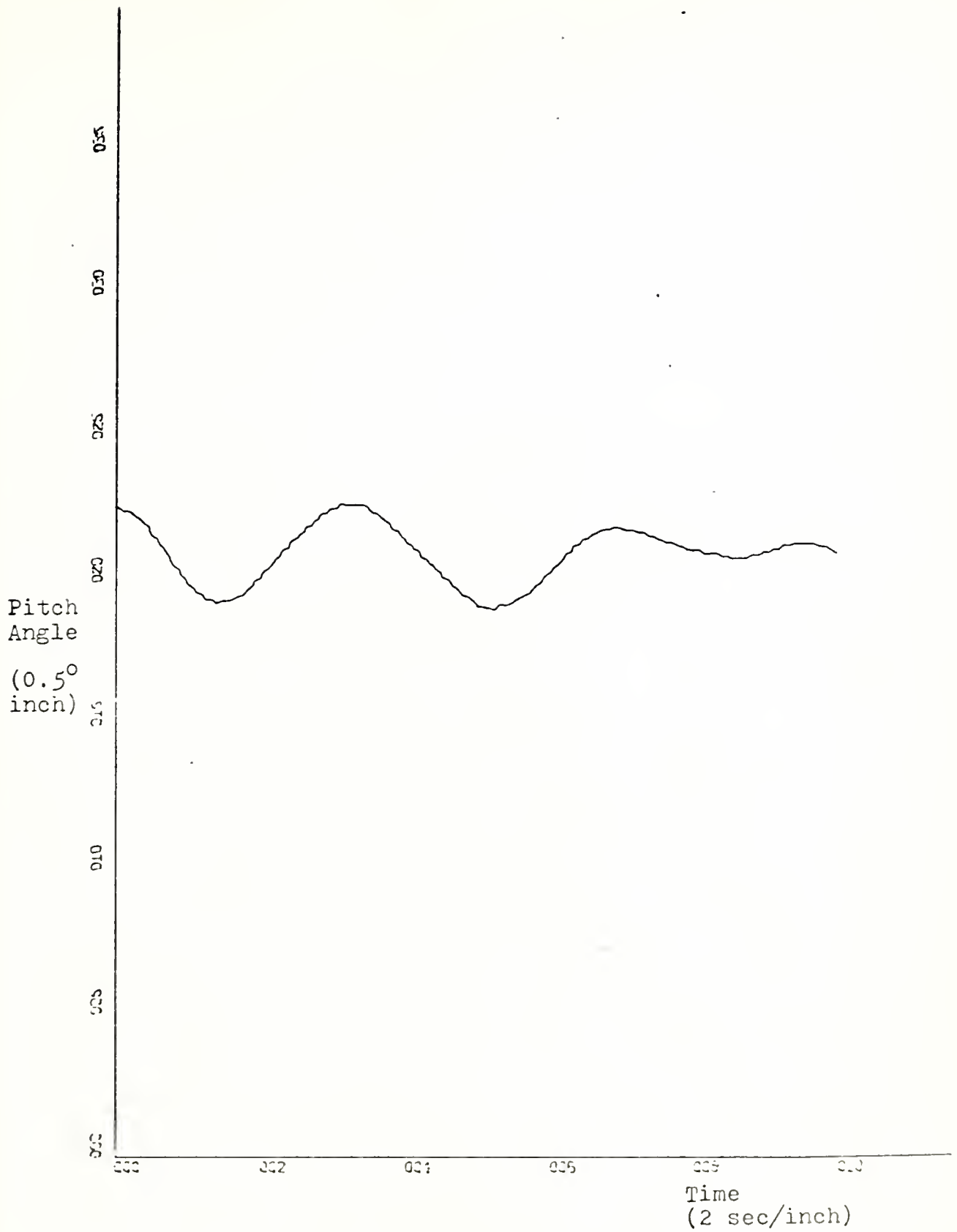


Figure 9. Plot of Pitch Angle Vs. Time After Smoothing



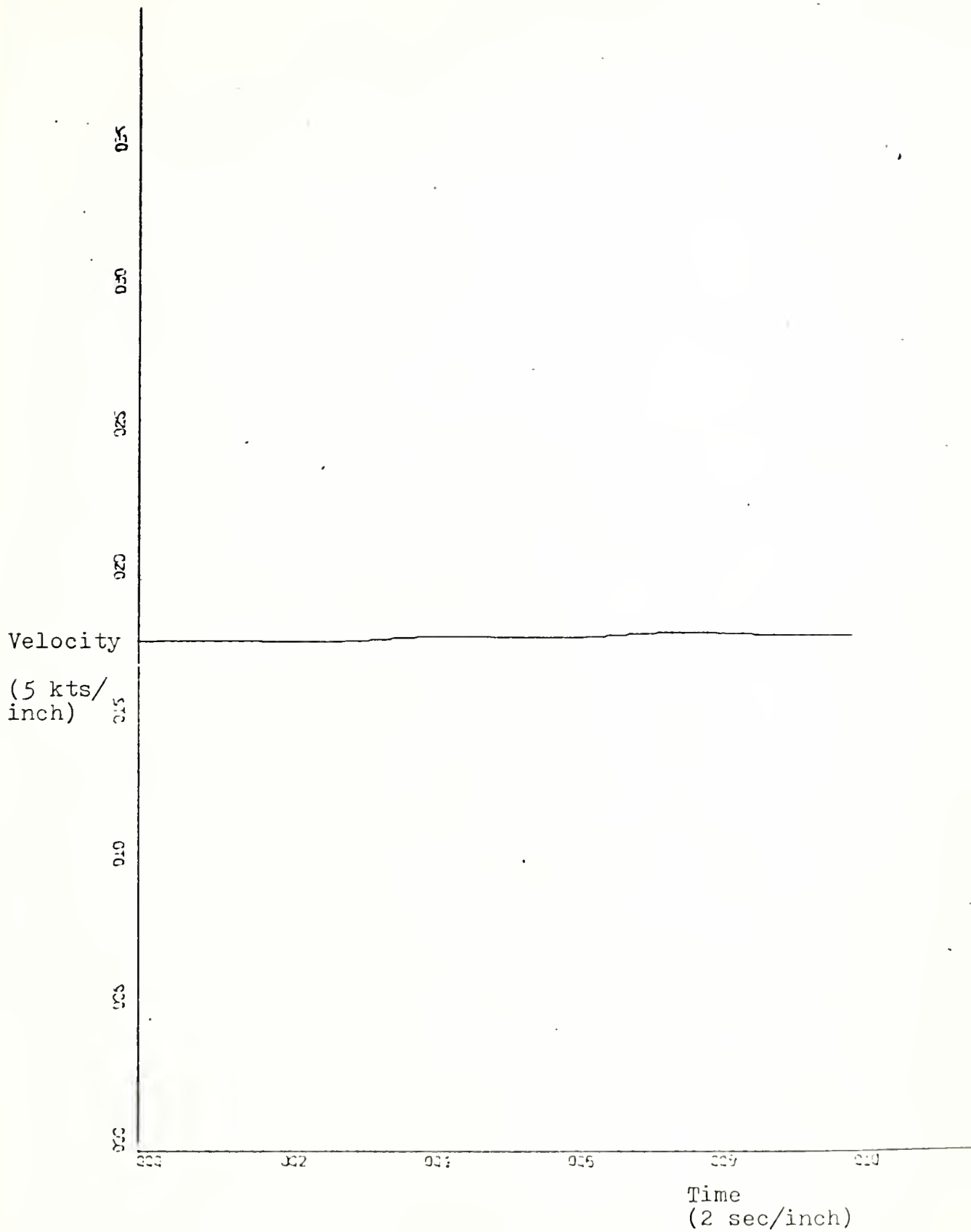


Figure 10. Plot of Velocity Vs. Time After Smoothing



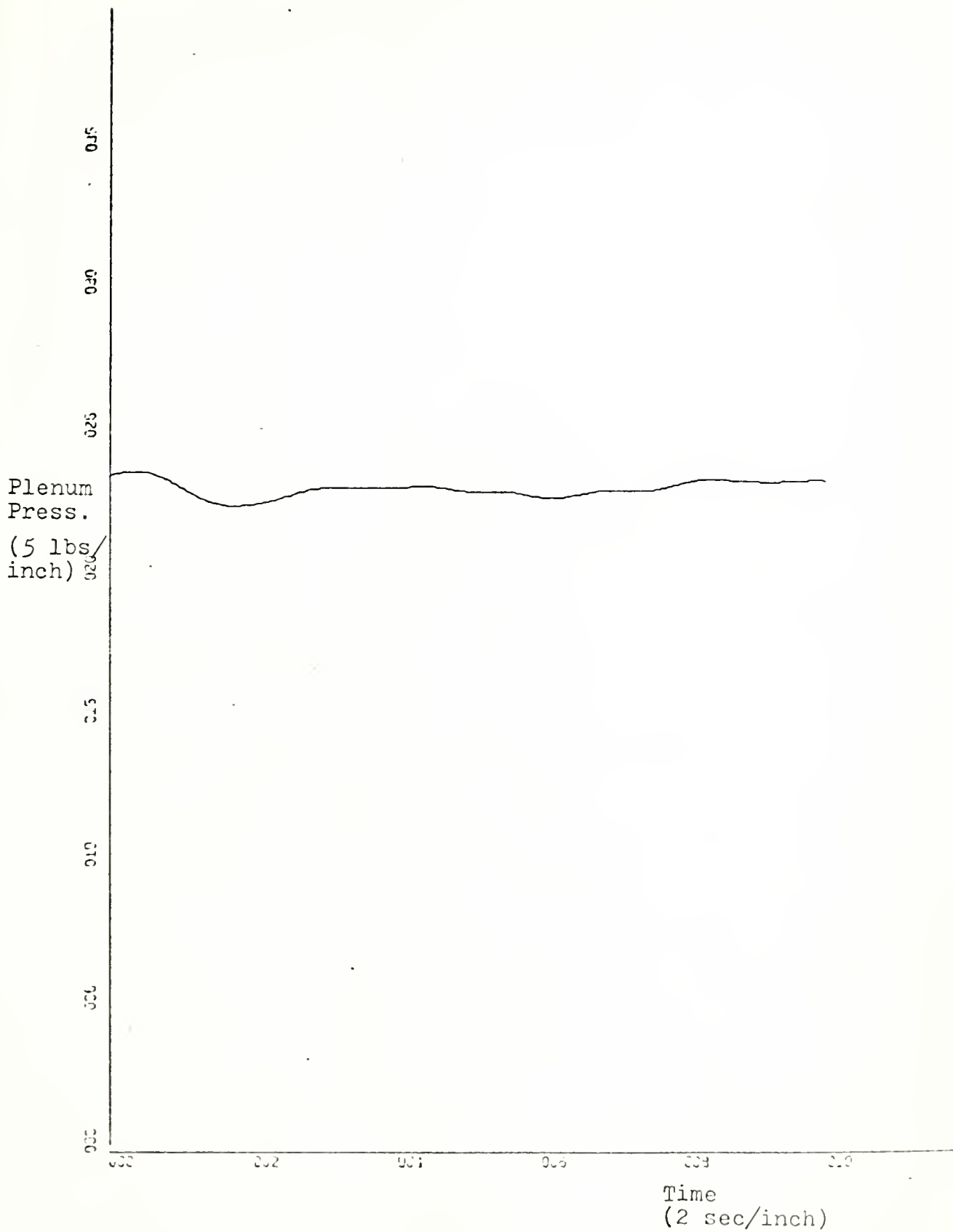


Figure 11. Plot of Plenum Pressure Vs. Time After Smoothing



#### IV. INTERFACE WITH XR-3 SIMULATION PROGRAM

##### A. LOGIC ADDITIONS TO SIMULATION PROGRAM

The XR-3 Loads and Motions simulation program was modified to the extent that, on execution of the program, the processed measurement data could be accessed if desired and on-line computation of differences could be made. The output from the program would then be a time history of the differences between computed and measured parameters. This entailed the addition of another option switch in the input data which is read by subroutine INCON. If the option switch is on or equal to one, subroutine INCON reads the measurement data into core from the disk where the data is stored. If the option switch is off or equal to zero, no reading of measurement data occurs.

It was decided to restrict validation or data comparison runs to ten seconds of simulation time because of core storage and computer time allocations. This decision set the size of the measurement data arrays at 200 elements. A COMMON block was added in subroutine INCON and RHS so that the measurement data could be available in subroutine RHS. As with other COMMON blocks, the feature to zero all elements of the added COMMON block was included in the main program. The following XR-3 test craft variables and the associated simulation names were selected for validation:



Total Thrust	THST
Velocity	VEL
Height	DRFT
Pitch Angle	THETAR
Roll Angle	DPHI
Plenum Pressure	PBAR
Yaw Angle	DEPSI
Rudder Angle	DELRS
Vertical Acceleration	ACCEL(3)
Yaw Rate	RDEG

The necessary logic was added in subroutine RHS such that the appropriate element with respect to time in the measurement array could be compared with the computed variable and a difference formed. The resultant differences were written into a temporary file for output by subroutine COLFIL after the simulation run reached the specified final time of ten seconds. Computation of differences was arranged such that positive values indicated that the computed parameter was greater than the measured parameter for any given sample time. The print interval for output purposes was set at one point every 0.05 seconds to correspond with the measurement data rate.

## B. METHOD OF THRUST INPUT AND OBSERVED DIFFERENCES

The first step in the validation process was to initialize the mathematical model at a particular operating point with the expected trim conditions of velocity, pitch



angle, draft, and plenum pressure. The feature exists in the simulation program to provide a thrust map of up to 25 points. Additional logic was included to select every fourth point in the 200 element array of measurement thrust to be applied to the mathematical model as an input variable and a ten second simulation proceeded to produce computed velocity. All other measurement parameters except velocity were ignored during initialization runs. The difference between computed velocity and measured velocity was taken as an output from the model. Following initialization of the model, another computer simulation was made using computed thrust as necessary to hold velocity constant. All measurement data for the run was read in and differences between computed and measured parameters were taken as output from the computer model.

For validation studies using measurement data with very nearly constant thrust applied on the testcraft, the foregoing procedure could be shortened by including only the last phase. Provided that the initial trim conditions were known for input to the computer model, no loss of accuracy resulted in the process of validation.

#### C. METHOD OF RUDDER AND THRUST INPUT TO THE MODEL

Similar to the thrust map provision is a provision for a rudder map input to the computer model. Up to 25 points may be included in a rudder map and the necessary logic was included in the program to select every fourth



point in the 200 element array of measured rudder angle for input to the mathematical model. The objective here was to apply the same inputs to the mathematical model as were used on the testcraft along with the initial trim conditions for each case. This method proved to be of little real value because a steering cable failure to the port propulsion engine on the testcraft rendered the rudder position measurement unreliable. To substitute for direct steering control on the port engine, the starboard engine was mechanically linked to the port engine by means of a long, rigid bar. Thus, the starboard engine controls the port engine in the rudder position and alignment of thrust vectors on the testcraft. Virtually all precision in rudder angle measurement is lost due to unavoidable play in the linkage and lack of direct steering control over both engines.

Validation studies involving turning maneuvers with the XR-3 testcraft and the mathematical model were carried out by matching yaw angles and yaw rates for a spectrum of operating conditions and by noting the differences between computed and measured rudder angles for each operating condition.



## V. PROGRAM SUBROUTINE MODIFICATIONS

### A. REPLACEMENT OF CENTER OF PRESSURE CURVE

Newman and Poole reported in Ref. 3 the existence of a pressure wave and the attendant gradual deformation of the surface of the water due to a moving pressure distribution with regard to CAB type hulls. NSRDC found that, in towing tank tests of CAB scale models, the craft tends to pivot in pitch motion about a point approximately 75-80% of the wetted length of the sidewall forward of the transom (Ref. 4). Based on these findings, it has been postulated that the center of volume within the plenum chamber moves aft with increasing speed.

Accordingly, the calculations made in the XR-3 simulation program to account for a shifting center of pressure were removed from subroutines RHS and WAVES. Computations were inserted in the program to account for the addition of an incremental wedge of volume to plenum volume which varies with craft speed. What follows is a description by subroutine of changes which were entered and the basis for the inclusion of the changes.

#### 1. Subroutine INCON

A previously unused space on the input data card number 00701 was used to read in the location of the pressure wave pivot point, measured in feet and tenths of feet forward of the transom. The statement  $XPWV = TEMP(3)$



was inserted in Block 07 in the INCON subroutine. A value of 17.2 ft. was used for XPWV in this study.

The relationship for wave drag produced by the movement of the pressure bubble over the water surface is, from Ref. 5:

$$X_{\text{bubble}} = - (P_b - P_a) C_F \frac{4W}{\rho g l} .$$

The same formula is mechanized in the simulation program as:

$$\text{FXPWAV} = -\text{PBBAR} * \text{CF} * \text{PWVCON}$$

where  $\text{CF} = 0.37 / ((U/\text{FNCON}) ** 1.5655981)$  and  $\text{PWVCON} = 4.0 * \text{WEIGHT} / (\text{RHO} * \text{G} * \text{XLBW})$ . The coefficient 0.37 and the exponent 1.5655981 are correct for the length to beam ratio of the XR-3 as determined from Ref. 3. The variable name WATSLP is given to the slope of the water surface inside the plenum and is calculated as:

$$\text{WATSLP} = \text{PBBAR} * \text{CF} * \text{PWVCON} / \text{WEIGHT}.$$

WATSLP represents the angle at the apex of the wedge-shaped increment of volume to be added to plenum volume. Since the ratio of  $\text{PBBAR} * \text{CF} * \text{PWVCON}$  ( i.e. bubble drag) to WEIGHT will always result in a small number for speeds above hump speed, the small angle approximation may be used without loss of accuracy. Therefore, the volume increment due to the water slope to be added to plenum volume is given by

$$0.5 * \text{WATSLP} * \text{XL} * \text{AB}$$

where XL is the length of the plenum chamber and AB is the area of the plenum at the water surface. The quantity  $0.5 * \text{WATSLP} * \text{XL}$  is then the vertical cross sectional area of the wedge-shaped volume increment.



Two other calculations were added in subroutine INCON for use in other subroutines during the simulation. The distance from XPWV from the forward extremity of the plenum is calculated as

$$XLXPWV = XLBW - XPWV$$

where XLBW represents the plenum length at the water surface. Also the distance between the craft center of gravity and XPWV is calculated as

$$XPWVXS = XPWV - XS$$

where XS is the longitudinal center of gravity measured in feet forward of the transom.

## 2. Subroutine BOWSL

In the computation for ELSKI, the wetted length of the bow seal, an incremental length is added to the wetted length of the seal. The increase is due to the water slope and is calculated simply as

$$XLXPWV * WATSLP$$

and added to the existing expression for ELSKI.

## 3. Subroutine STNSL

Similar to the wetted length correction in BOWSL, an incremental correction is computed and applied in subroutine STNSL. Here the correction is opposite in sign and is applied to the wetted length of the stern seal, ELSKI as

$$-XPWV * WATSLP.$$

## 4. Subroutine RHS

The water slope correction is computed in subroutine RHS as a continuous variable over the period of any given



simulation time. Recognizing that WATSLP is calculated as the ratio of bubble wave drag to total craft weight and that bubble wave drag varies with velocity and plenum pressure, WATSLP must be considered as a continuous variable. Accordingly, the following computation was introduced in RHS:

$$\text{WATSLP} = -\text{FXPWAV} / \text{WEIGHT}$$

The plenum volume is corrected for the water slope on each pass through subroutine RHS by the addition of a volume increment as in subroutine INCON:

$$+ .5 * \text{WATSLP} * \text{XL} * \text{AB.}$$

#### 5. Subroutine SIDEWL

The addition of a wedge-shaped volume to plenum volume required an alteration to the computation of the drafts along the sidewalls inside the plenum chamber. Displacement of water is calculated as

$$\text{PBHEAD} = \text{PBAR} / (\text{RHO} * \text{G})$$

where PBAR is the instantaneous plenum pressure. The immersion depth on the inside of each sidewall section is calculated in the relation

$$\text{DDIN} = \text{DD} - \text{WATSLP} * (\text{XPWVXS} - \text{XX}(, \text{K}))$$

where DD represents the uncorrected water level height above the keel along each sidewall section and XX(J,K) is the distance from the transom of the center of each of the eleven stations along the sidewall.

A revision of the method of computing sidewall gaps at any given station was also necessary. A logical IF



statement was included to test each value of DDIN after it was computed. If DDIN is less than zero another logical IF statement must be tested to determine if a gap exists between the bottom of the sidewall (keel) and the water surface. If DSW (J,K), or the actual sidewall immersion depth, is less than PBHEAD, then a gap for that sidewall section is computed as

$$\text{GAP (J,K)} = - \text{DDIN} * (1. - (\text{DSW(J,K)}) / \text{PBHEAD})$$

where the computed GAP for any given station is in units of feet.

Further background information of use in this study is contained in References 6-11.

#### B. THRUST VECTORS IN SUBROUTINE PROP

The propulsion system in the XR-3 consists of two forty horsepower outboard motors. The port screw has a right hand rotation and the starboard screw has a left hand rotation. Steering control is obtained by rotation of the motors in the horizontal plane. Thus, there is some rudder effect from the foil-shaped lower motor housings, however the predominant turning moment results from re-alignment of the propulsion thrust vectors when rudder angle is applied. In addition to the main thrust vector, directed in the line of craft motion for zero rudder angle, there exists a side thrust vector for each propeller. Since the propellers are counter-rotating, and due to the direction of rotation of each propeller, the side thrust vectors are



oppositely directed and, for zero rudder angle, are directed inboard.

The assumption is made that both port and starboard propulsion motors rotate together through the same rudder angle. It is also assumed that the magnitude of the main and side thrust vectors are independent of rudder angle.

The propeller thrust diagram shown in Figure 12 was used to verify and correct the force and moment equations for the XR-3 propulsion system. The figure displays the main thrust and side thrust vectors for both propellers positioned with right (positive) rudder angle  $\delta$ , positive pitch angle  $\theta$ , and negative (port side down) roll angle  $\phi$ . The thrust vectors act through the port and starboard propeller positions,  $X_P$ ,  $Y_P$ , and  $Z_P$  from the craft center of gravity in the Body Reference coordinate system.

The forces associated with the propeller alignment of Figure 1 are shown vectorially in Figure 13 in the Local Level coordinate system after having been corrected for pitch and roll angles. The assumption is made that pitch angle and roll angle are limited to small angles such that  $\sin\theta \approx \theta$  and  $\cos\theta \approx 1$ ,  $\sin\phi \approx \phi$  and  $\cos\phi \approx 1$ . The following force equations result:

$$T1X = THST1 * \cos \delta$$

$$T2X = THST2 * \cos \delta$$

$$ST1X = - STHST1 * \sin \delta$$

$$ST2X = STHST2 * \sin \delta$$

$$T1Y = THST1 * \sin \delta$$



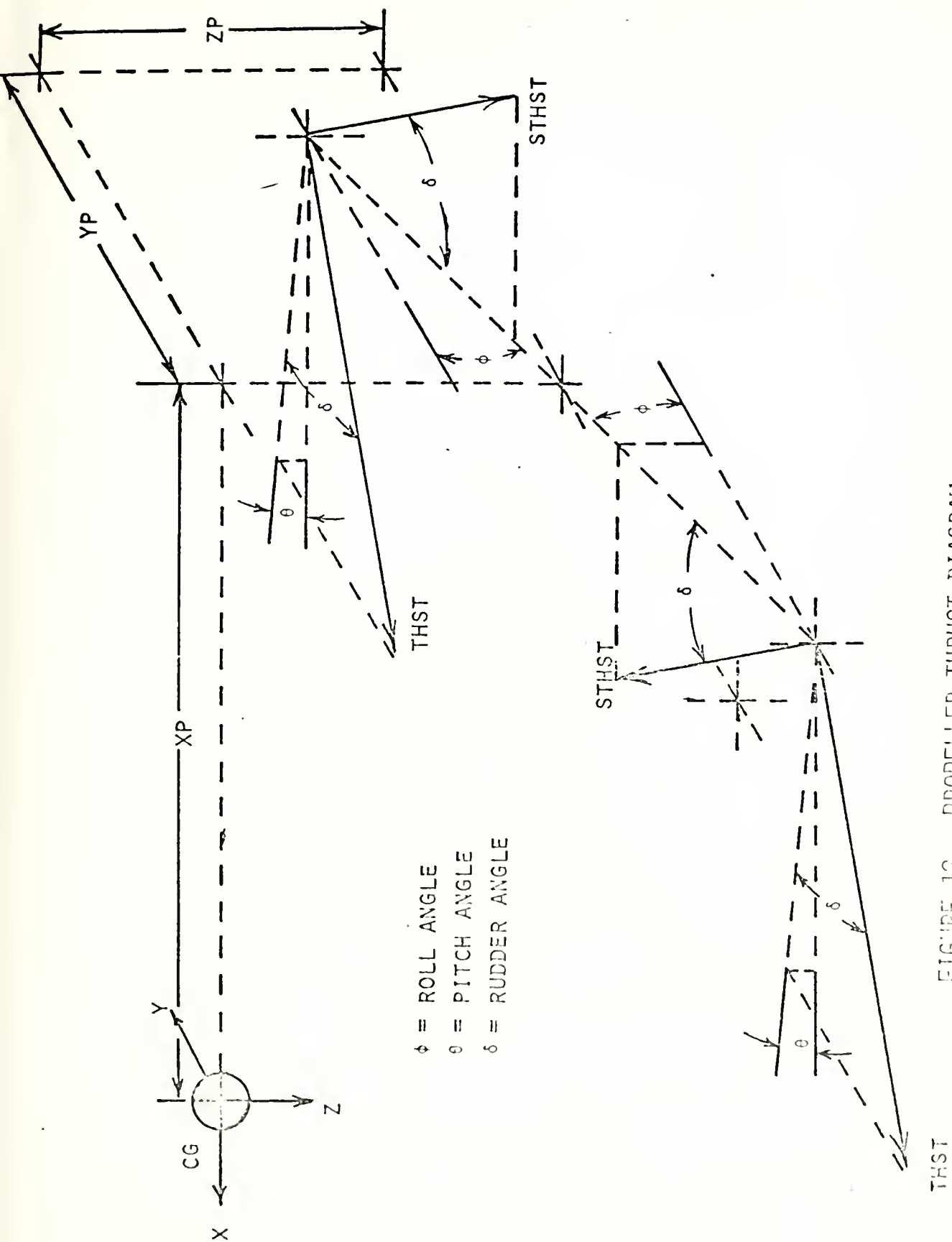


FIGURE 12. PROPELLER THRUST DIAGRAM



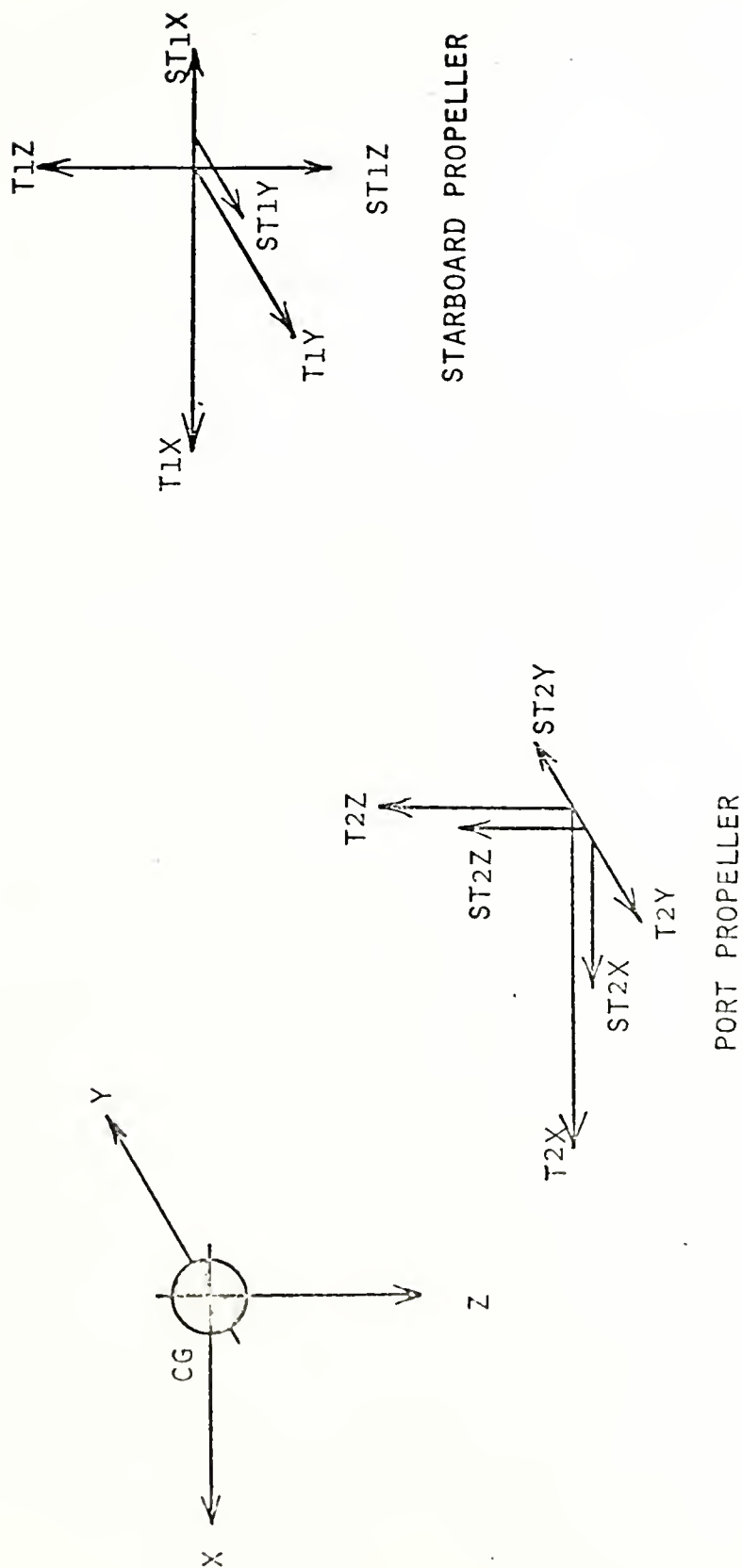


FIGURE 13. VECTOR RESOLUTION OF PROPELLER THRUST FORCES



$$T2Y = THST2 * \sin \delta$$

$$ST1Y = -STHST1 * \cos \delta$$

$$ST2Y = STHST2 * \cos \delta$$

$$T1Z = THST1 * \cos \delta * \theta$$

$$T2Z = THST2 * \cos \delta * \theta$$

$$ST1Z = STHST1 * \cos \delta * \phi$$

$$ST2Z = STHST2 * \cos \delta * \phi$$

Summing the forces in each of the three coordinate directions yields the following result:

$$FXS = T1X - ST1X$$

$$FXP = T2X + ST2X$$

$$FYS = -T1Y - ST1Y$$

$$FYP = T2Y + ST2Y$$

$$FZS = -T1Z + ST1Z$$

$$FZP = -T2Z - ST2Z$$

The total force equations are found by summation of the force equations for the port and starboard propulsion systems in each of the three coordinate directions as follows:

$$FX = FXP + FXS$$

$$FY = FYP + FYS$$

$$FZ = FZP + FZS$$

Corrections were made to the force calculations of subroutine PROP from Reference 1 on the basis of the foregoing discussion.



## VI. DISCUSSION AND EVALUATION OF RESULTS

### A. OBTAINING AGREEMENT AMONG VARIABLES

Computer simulation runs in the initial stages of this study revealed that plenum pressure was consistently approximately 2.5 psf higher than that recorded on the XR-3 testcraft. Among other variables, thrust on the testcraft was higher than the computer model indicated for any given speed and calculated draft was greater by approximately three inches than the computer model produced. The decision was made to first obtain agreement in plenum pressure between the mathematical model and the testcraft.

The bow seal leakage area input to the mathematical model was listed in Ref. 1 as one of the parameters not known to be exact. The estimate of leakage area was revised from 0.08 sq. ft. to 0.10 sq. ft. This slight alteration had the desired effect of reducing plenum pressure to agree with that measured on the XR-3 testcraft. An unexpected but welcome additional effect was nearly perfect agreement in thrust and draft. Aside from the alterations to the structure of the mathematical model there were no further changes made to the model during the course of the present study.

#### 1. Straight Runs Made with Different C.G. Positions

Validation runs were made interfacing data measured on the XR-3 testcraft with the computer model. The data



presented in Table III is a summary of average differences calculated between time histories of actual craft motions and simulated craft motions for the thrust, velocity, pitch angle, plenum pressure and draft variables. Also included is percentage differences for ease in qualitative comparison. It should be noted that percentage differences in pitch angle measurement appear to be quite large, however in most cases the difference is within the measurement accuracy limitation of  $\pm 0.5$  degree aboard the testcraft.

The total craft weight on the measurement runs listed in Table III was 6270 lbs. In addition to the pilot there was a passenger in the co-pilot position and 250 lbs. of water in plastic containers aboard used for changing the location of the center of gravity of the XR-3.

The data presented in Table IV is a summary of average time history differences with a fixed center of gravity on the XR-3. On the measurement runs listed in Table IV the total craft weight was 6050 lbs. Vertical acceleration was substituted for draft in this series of validation runs.

Figures 14, 15, 16, 17, and 18 are typical of the graphical output from the XR-3 simulation program arranged to display the time histories of differences between computed and measured variables for this study.

## 2. Runs Made with Turns

A series of eleven validation runs were made with various rudder angles at various speeds. A summary of the



TABLE III. SUMMARY OF DIFFERENCES IN STRAIGHT RUNS-A

Average Differences Between Mathematical Model and Measured Variables are Listed \*  
(Percentage Differences in Parentheses)

Run	Velocity	CG Location	Thrust	Velocity	Pitch	Plenum Press	Draft
1.	18.2 kts	10.15 ft	-9.0 (-1.96)	0.0 (0)	-0.65 (-32.5)	0.0 (0)	-0.6 (-4.9)
2.	18.9	10.27	28.0 (5.9)	0.0 (0)	-0.8 (-38.1)	0.01 (.05)	-2.1 (-15)
3.	16.6	10.03	-17.0	-0.1	-0.2	0.01	0.1
4.	14.3	10.03	(-3.9)	(-0.6)	(-10.2)	(.04)	(0.86)
			-38.0	-0.06	-0.4	0.14	1.2
5.	16.5	10.15	(-8.9)	(-0.42)	(-18.6)	(.63)	(11.3)
			-12.5	-0.1	-0.3	0.0	0.6
6.	17.1	10.19	(-3.0)	(-0.6)	(-14.6)	(0)	(5.4)
			-10.0	0.0	-0.3	0.0	0.6
7.	13.9	10.067	(-2.3)	(0)	(-12.0)	(0)	(5.4)
			3.5 (0.9)	0.0 (0)	-0.2 (-9.52)	0.01 (.04)	0.1 (.85)



TABLE III. (Continued)

Run	Velocity	CG Location	Thrust	Velocity	Pitch	Plenum Press	Draft
8.	22.0	10.03	32.0 (6.4)	0.05 (0.2)	0.0 (0)	-0.7 (-3.2)	-1.4 (-11.2)
9.	12.5	10.15	-8.7 (-2.3)	0.07 (.6)	0.2 (9.1)	0.01 (.4)	0.5 (4.3)
10.	22.4	10.03	38.0 (7.5)	0.0 (0)	0.16 (9.3)	0.0 (0)	-1.6 (-11.8)

\* NOTE: Negative sign indicates computed variable is smaller than measured variable.

Craft total weight was 6270 lbs. in all runs.



TABLE IV. SUMMARY OF DIFFERENCES IN STRAIGHT RUNS-B

Average Differences Between Mathematical Model and Measured Variables are Listed \*  
(Percentage Differences in Parentheses)

Run	Velocity	CG Location	Thrust	Velocity	Pitch	Plenum Press	Vert Accel
1.	20.6 kts	10.15	29.0 (5.6)	0.0 (0)	0.1 (5.3)	0.12 (4.5)	0.01 (2.1)
2.	15.2	10.15	-16.0 (-4.2)	-0.05 (-0.3)	-0.2 (-9.1)	0.02 (0.1)	0.008 (0.9)
3.	14.4	10.15	-11.0 (-3.5)	0.03 (0.2)	0.1 (6.35)	0.05 (0.22)	0.004 (0.45)
4.	18.7	10.15	21.0 (4.8)	0.01 (0.05)	-0.7 (-22.0)	0.01 (0.4)	0.01 (2.1)
5.	22.8	10.15	28.0 (6.4)	0.04 (0.17)	-0.3 (-12.0)	0.06 (0.3)	0.003 (0.4)

\* NOTE: Negative sign indicates computed variable is smaller than  
measured variable

Craft total weight was 6040 lbs. in all runs.



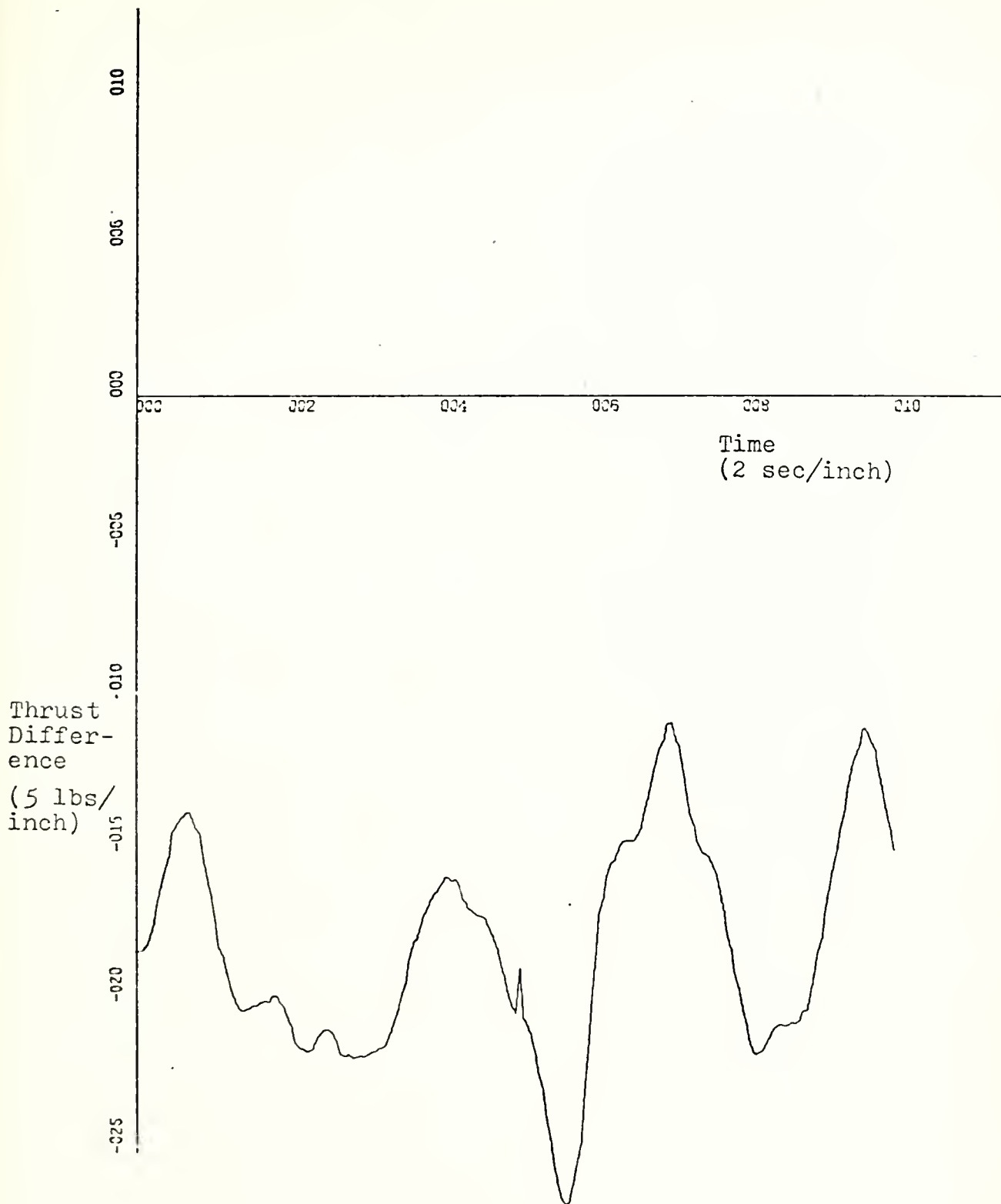


Figure 14. Plot of Thrust Difference Vs. Time



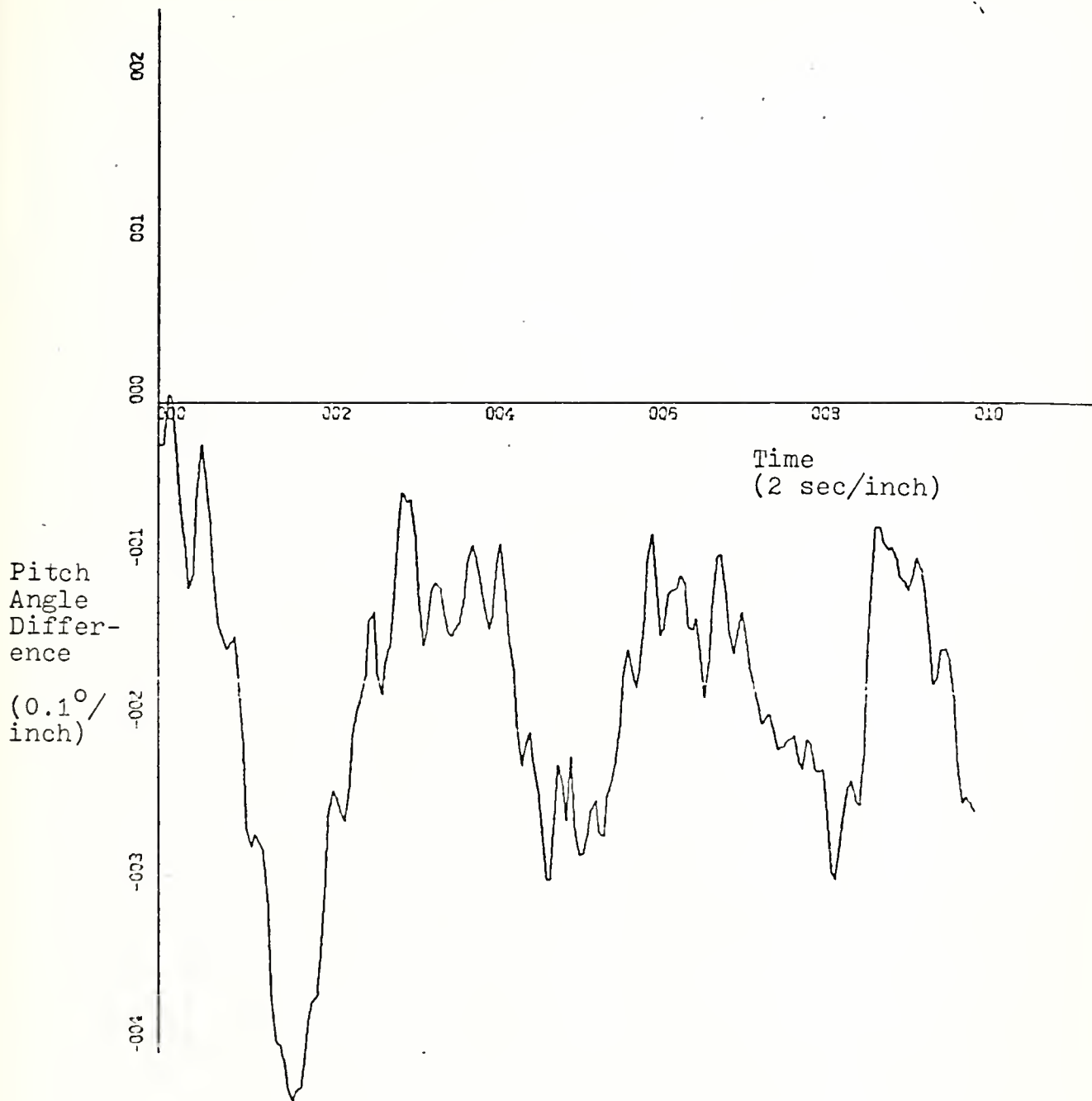


Figure 15. Plot of Pitch Angle Difference Vs. Time



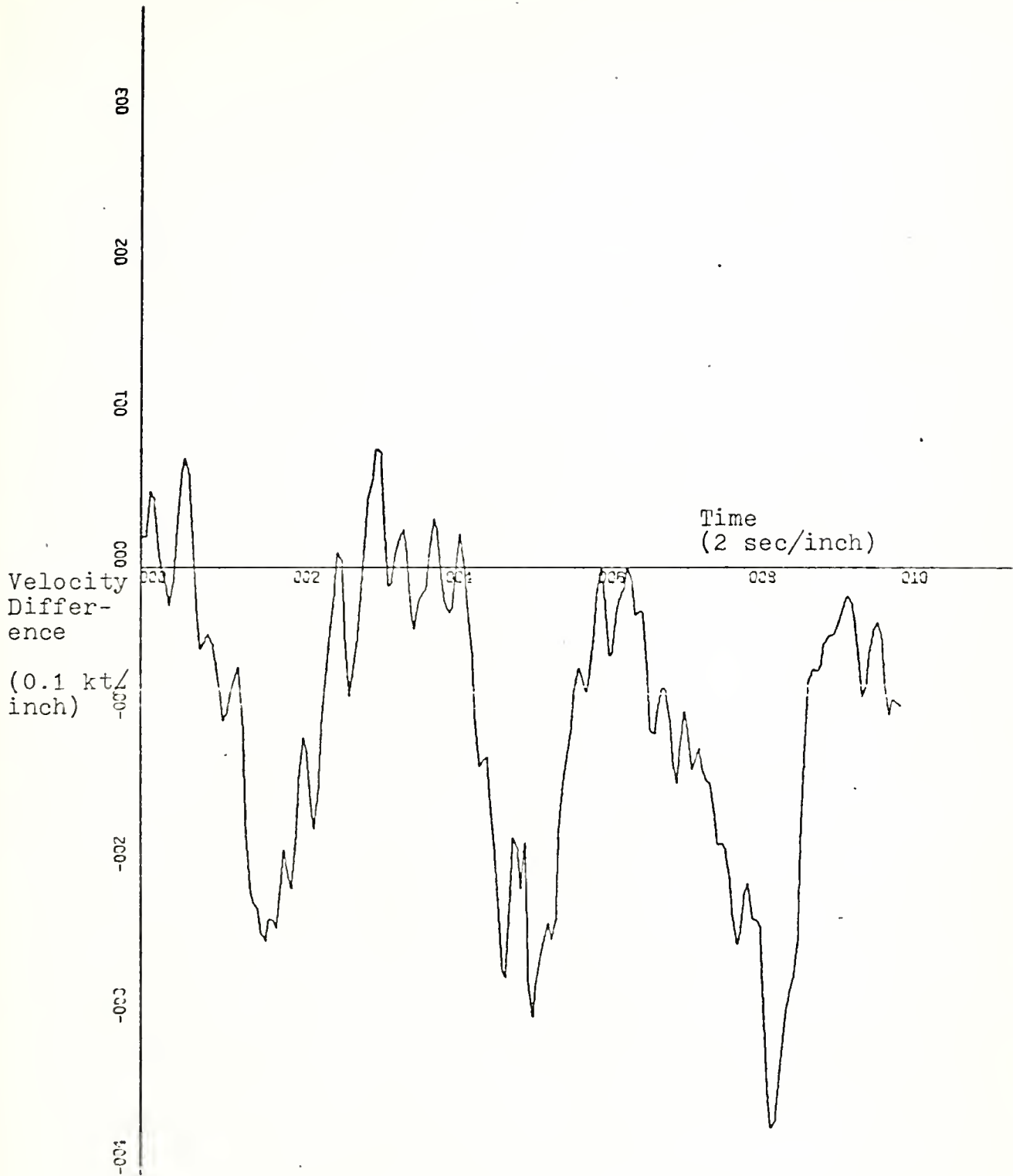


Figure 16. Plot of Velocity Difference Vs. Time



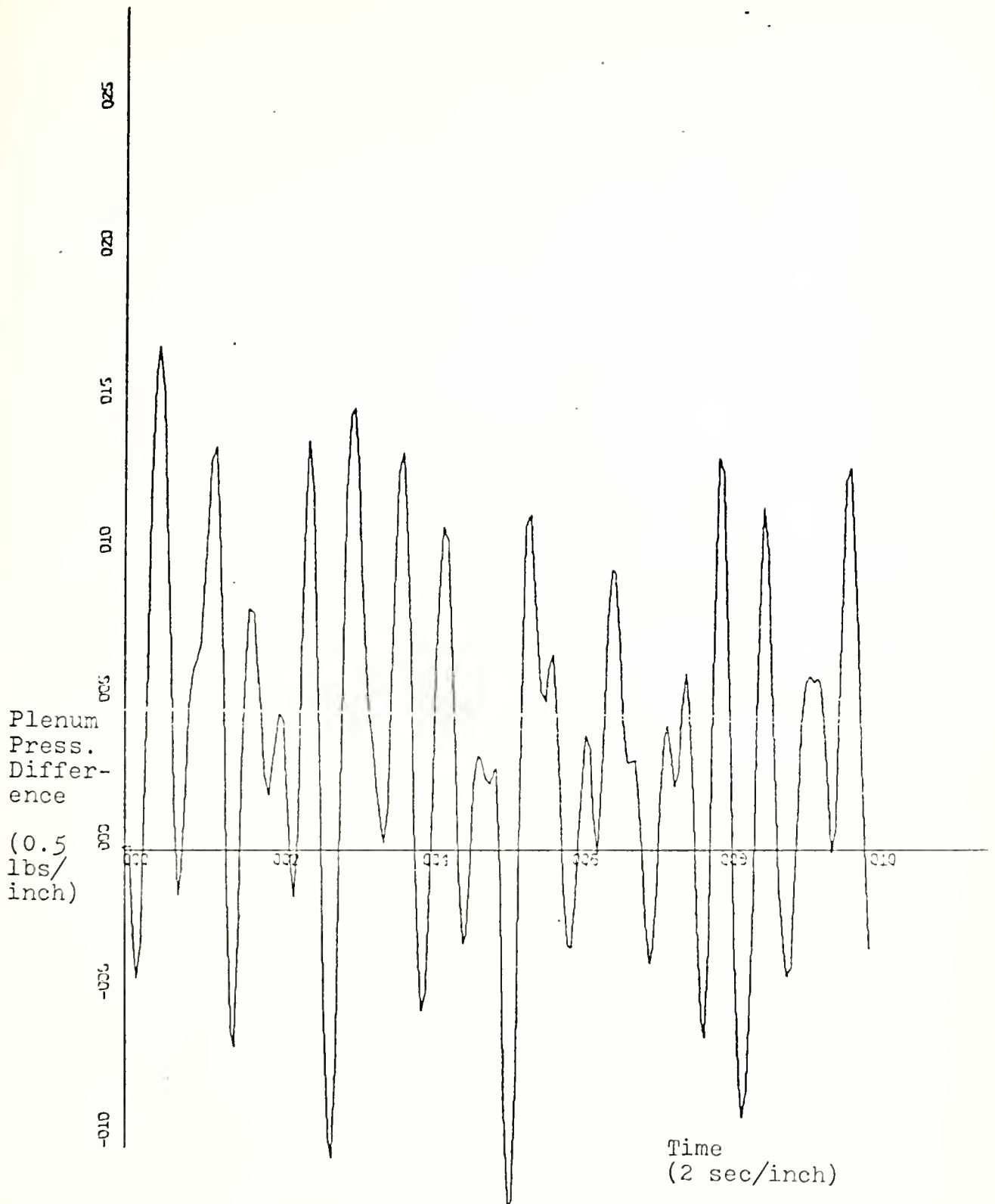


Figure 17. Plot of Plenum Pressure Difference Vs. Time



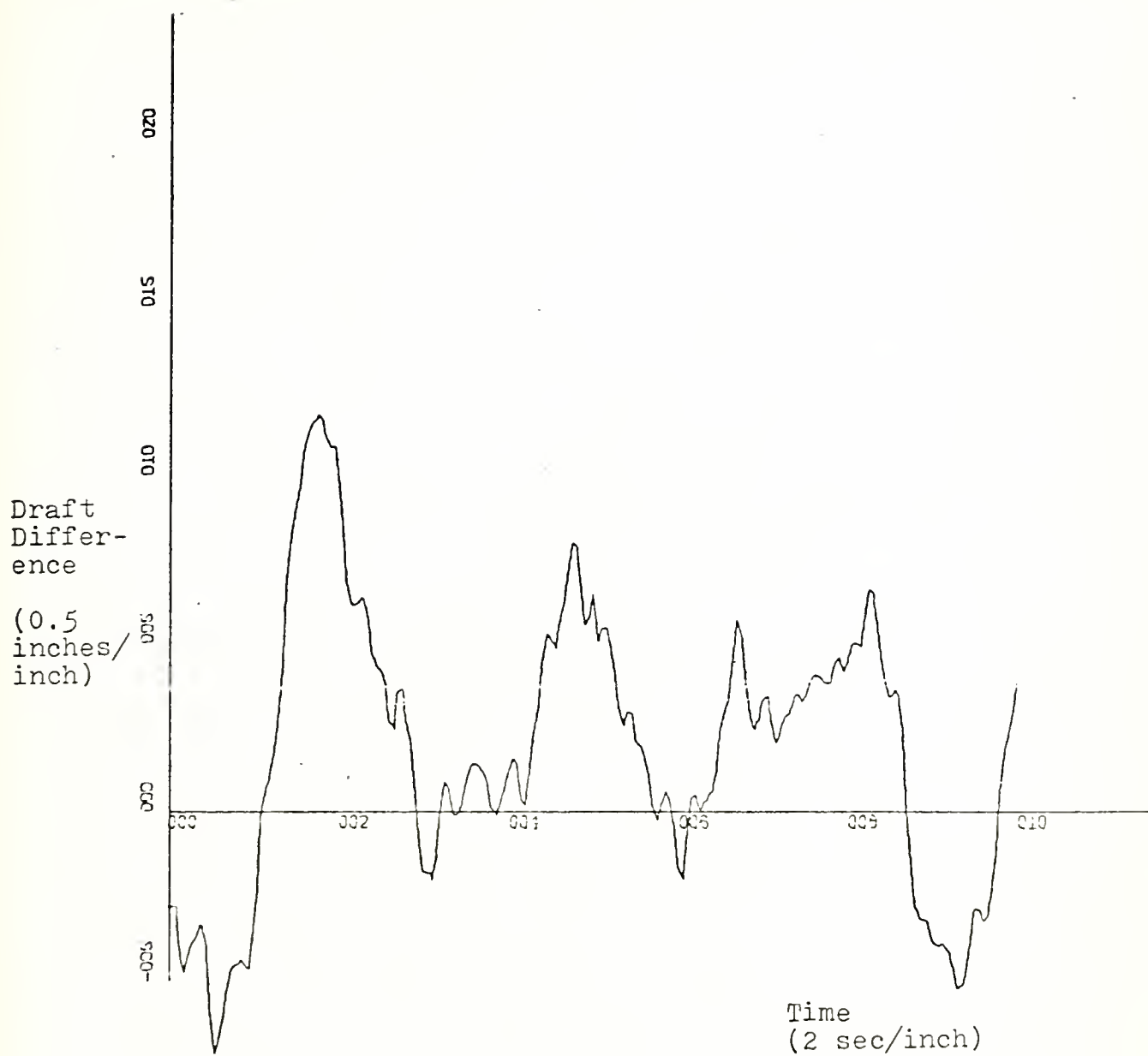


Figure 18. Plot of Draft Difference Vs. Time



average differences calculated between actual craft motions and simulated craft motions during the turning maneuvers for thrust, velocity, pitch angle, roll angle, yaw angle, yaw rate and rudder position variables is presented in Table V.

The relatively large differences in rudder angles in many runs is attributed to the lack of confidence in an accurate rudder position measurement. In the future when direct steering control of both propulsion motors is restored, it is recommended that confirmation be made of the results presented here with regard to rudder position and other variables in turning maneuvers.

Figures 19, 20, 21 and 22 are typical of the graphical output from the XR-3 simulation program which display the time histories of differences in roll angle, yaw angle, yaw rate, and rudder angle, respectively.

#### B. LIMITED TO CALM WATER CASES

It is recognized that much of the measurement data obtained at the XR-3 test site at Lake San Antonio, California contains small perturbations due to surface disturbances on the lake. No attempt has been made to measure the surface disturbances or their effect on the testcraft. Validation of the mathematical model in the presence of waves of any amplitude and wavelength is suggested as an area for further study.



TABLE V. SUMMARY OF DIFFERENCES IN TURNS

Average Differences Between Mathematical Model and Measured Parameters are Listed \*  
(Percentage Differences in Parentheses)

Run	Rudder Ang	Velocity	Thrust	Velocity	Pitch	Roll	Yaw	Yaw Rate	Rudder Ang
1.	L 4.5°	19.7 kts	8.5 (2.2)	0.0 (0)	-.36 (-13.4)	0.03 (6.5)	3.63 (22.7)	0.01 (7.0)	-3.0 (-40)
2.	L 3.0	24.7	12.0 (2.5)	0.0 (0)	-.3 (-13.4)	0.04 (8.0)	0.5 (4.7)	0.2 (21.7)	-3.0 (-50)
3.	L 3.0	13.7	-17 (-4.9)	-0.08 (-.3)	-.7 (-38.6)	0.03 (18.7)	-.15 (1.85)	0.0 (0)	-8.0 (-72)
4.	L 3.3	25.1	28.0 (5.8)	0.0 (0)	0.05 (2.2)	0.22 (38.6)	1.8 (15.2)	0.3 (29.1)	0.65 (16)
5.	L 5.4	16.3	-14.0 (-3.9)	0.0 (0)	0.09 (4.7)	0.1 (40)	-.73 (-6.2)	0.09 (6.4)	-1.3 (-23)
6.	L 5.8	21.5	-21.0 (-4.9)	0.06 (0.3)	0.29 (11.6)	0.23 (44)	1.1 (6.3)	0.05 (2.6)	1.4 (31)
7.	R 4.1	19.6	27.0 (6.8)	-0.06 (-0.3)	-0.38 (-20)	-0.1 (-25.6)	0.2 (1.4)	0.04 (3.1)	0.7 (14.6)



TABLE V. (Continued)

Run	Rudder Ang	Velocity	Thrust	Velocity	Pitch	Roll	Yaw	Yaw Rate	Rudder Ang
8.	R 3.8	19.6	28.0 (7.1)	-0.03 (-0.2)	-0.4 (-20.7)	-0.13 (-36)	0.96 (7.4)	0.05 (4.2)	0.44 (10.4)
9.	R 6.1	20.2	-18.0 (-4.5)	0.05 (0.2)	-0.21 (-10.5)	0.15 (31.2)	1.9 (9.2)	0.0 (1.8)	-2.5 (-29)
10.	R 3.9	18.1	16.0 (4.2)	0.0 (0)	0.06 (3.1)	0.1 (20)	0.62 (5.3)	0.03 (2.2)	-0.9 (-19)
11.	R 5.6	15.7	12.0 (5.1)	0.0 (0)	-0.04 (-2.6)	0.03 (19.4)	0.51 (6.1)	0.17 (9.8)	1.2 (17.6)

\* NOTE: Negative sign indicates computed variable is smaller than measured variable.

Craft total weight was 6040 lbs. in all runs.



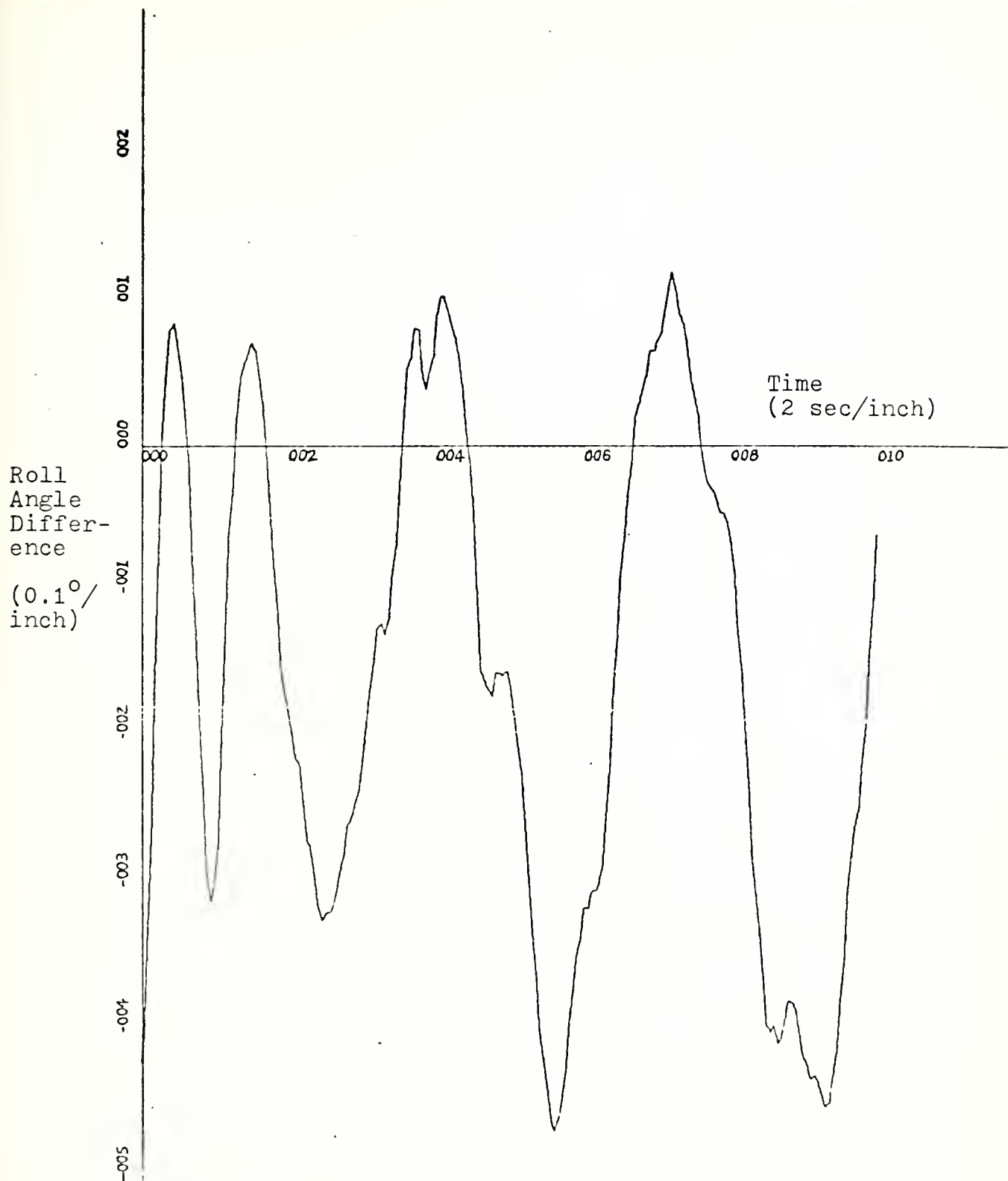


Figure 19. Plot of Roll Angle Difference Vs. Time





Figure 20. Plot of Yaw Angle Difference Vs. Time



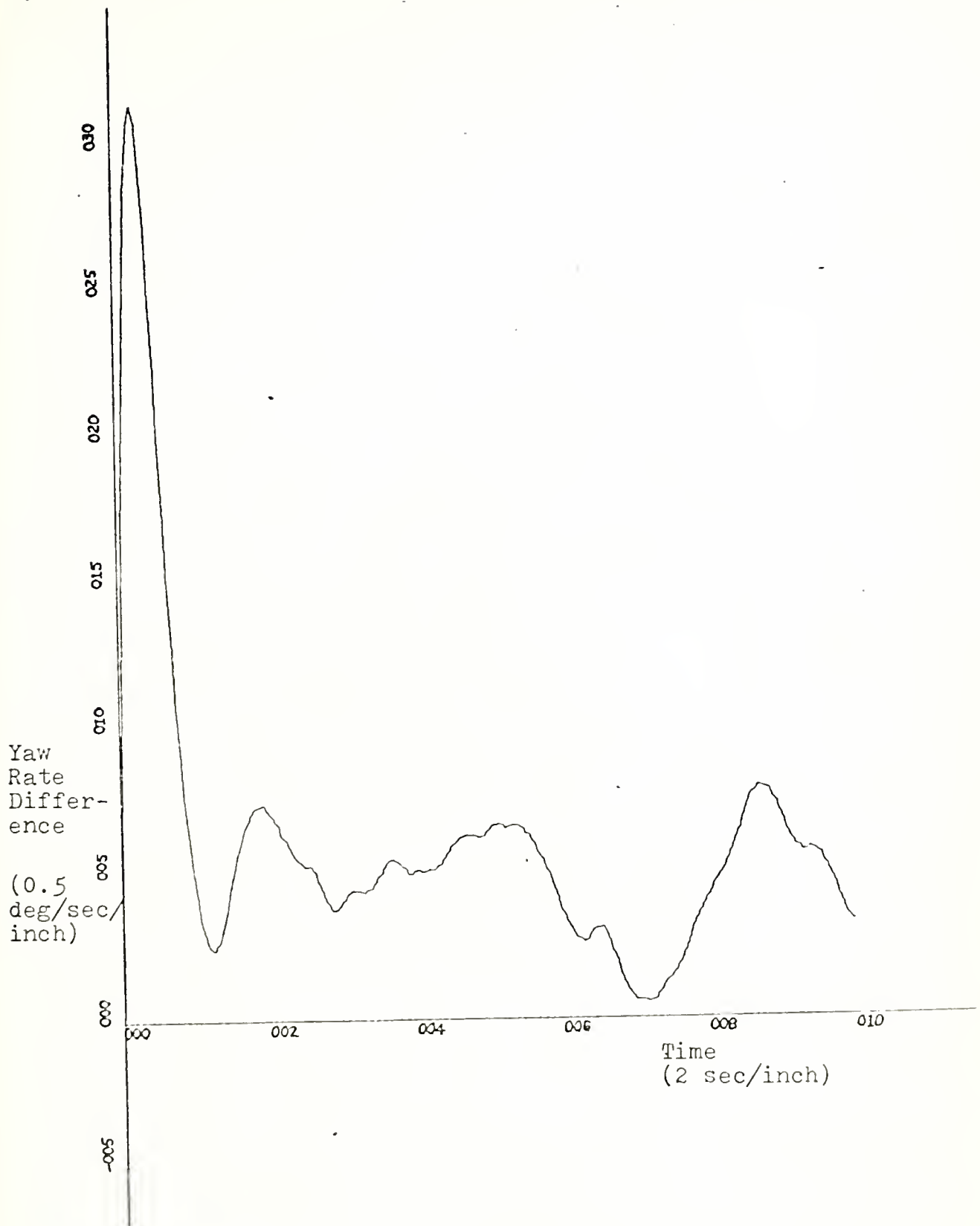


Figure 21. Plot of Yaw Rate Difference Vs. Time



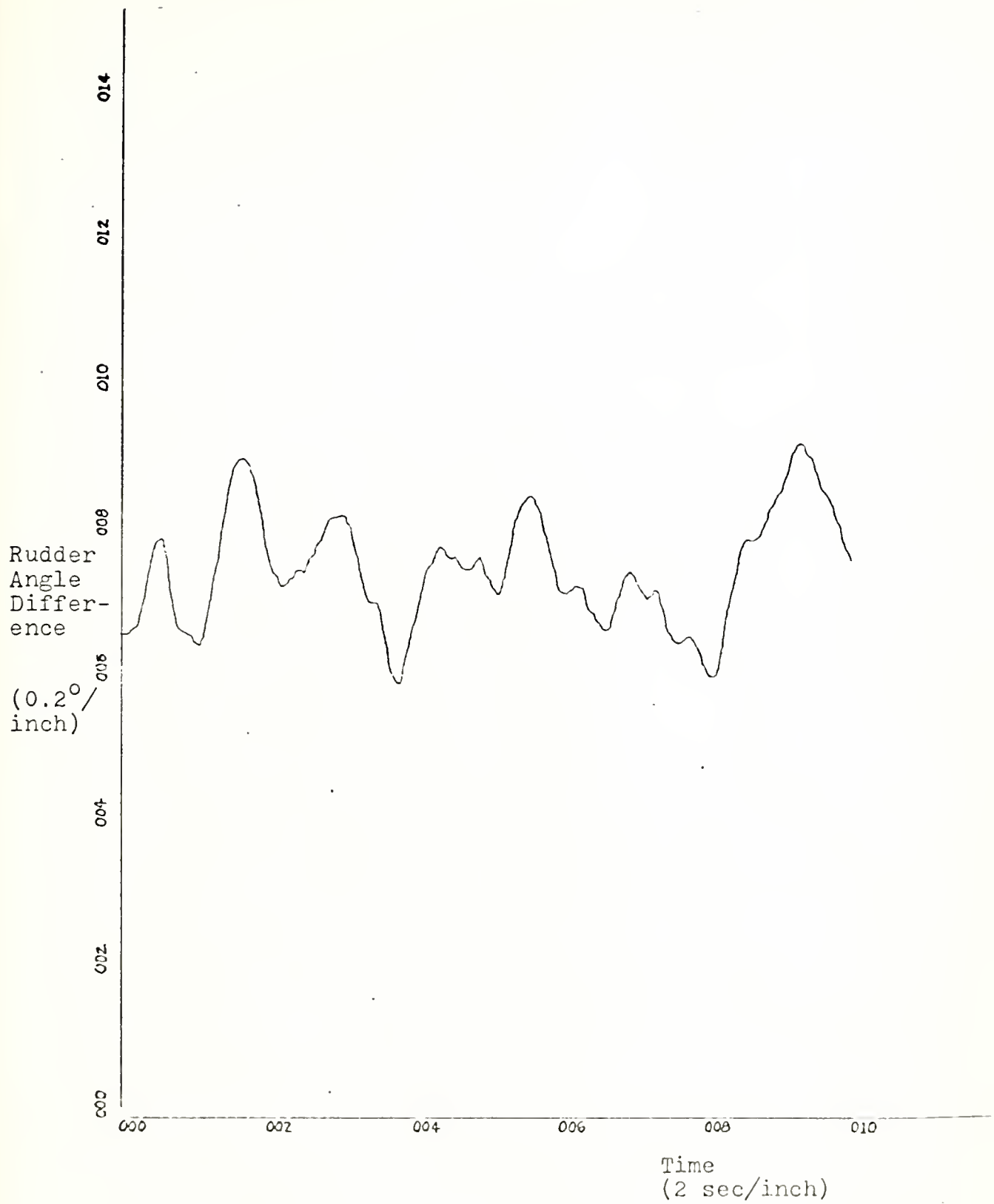


Figure 22. Plot of Rudder Angle Difference Vs. Time



A listing of the FORTRAN program for simulation of the XR-3 is included as Appendix D. A sample input data deck is also included.



## VII. CONCLUSIONS AND RECOMMENDATIONS

This study has shown that the nonlinear mathematical model with six degrees of freedom adequately describes the motions of the XR-3 in calm water conditions. The variables used in the validation included thrust, longitudinal velocity, pitch angle, plenum pressure, draft and vertical acceleration in straight runs. For validation of turning dynamics the variables included thrust, longitudinal velocity, pitch angle, roll angle, yaw angle, yaw rate and rudder angle. Differences that were found to exist between the computer model and the testcraft were less than 5% for the majority of the variables compared and those differences that exceeded 5% are considered acceptable, given the range of the measured variables and the accuracy of the sensors aboard the testcraft.

During the course of this study, it became apparent that the computer model exhibits a more oscillatory, or underdamped, response in pitch and roll motions than does the XR-3 testcraft. A concurrent study by LCDR. R.A. Finley, USN upon this aspect of the simulation with attention to the modelling of the bow seal and the lift fan system is reported in Reference 12.

The method of data processing set forth in this study to produce data in adequate form for interface with the mathematical model is recommended for use in future



validation efforts. A considerable amount of time and effort was spent in signal analysis and data processing to prepare the measured data in a form useful for comparison with the mathematical model variables. In order to eliminate the requirement for smoothing the re-scaled data, it is recommended that a study be made using a lower sampling rate for the A-to-D conversion to see if the high frequency noise can be eliminated from the digitally reproduced data. It is also recommended that a vibration study be conducted aboard the XR-3 in an attempt to determine if the source or sources of the high frequency noise is the result of internal ship vibration acting on the measurement transducers, gyros, and accelerometers. The current data acquisition system installed in the testcraft should be adequate for such a study.

A very fertile area for future study would be validation of the computer model in the presence of waves. Instrumentation exists to measure wave conditions at the XR-3 test site during measurement runs and the simulated waves could be input to the mathematical model. Direct comparison of craft behavior and simulation model calculations could then be obtained to produce an evaluation of the accuracy of the simulation in sea states.



# APPENDIX A

-----

## LISTING OF FORTRAN PROGRAM FOR ANALOG TO DIGITAL CONVERSION OF MEASUREMENT DATA

```

DIMENSION IBUF(4096,2),LOCB(-1,1),BADREC(100)
INTEGER RECNUM,BADREC
NAMELIST NREC, NSAMP, NCHAN, ITAPE,NDEL,NT
1 INPUT(101)
  NWORDS=NSAMP*NCHAN
  LOCB(-1)=LOCB(1,1)
  IF NREC.GT.1,LOCB(1)=LOCB(1,2)
  IF NREC.EQ.1,LOCB(1)=LOCB(-1)+NWORDS
  IND=2
  GO TO 15
2 NB=1
  RECNUM=0
  NEWBUF=LOCB(1)
  IF(IABS(IND).NE.2)GO TO 94
  CALL WRITCLOCK(0)
  CALL ADSTART(NCHAN,LOCB(-1),NEWBUF,NSAMP,RECNUM,11S)
  CALL MTRDY(ITAPE,LOCB(-1),LOCB(1),NWORDS,IND)
4 IF IND.EQ.1, GO TO 4
  GO TO(4,3,91,93)IND
3 IF NT.EQ.0,GO TO 7
  CALL MTRDY(ITAPE+1,LOCB(-1),LOCB(1),NWORDS,IND)
6 IF IND.EQ.1,GO TO 6
  GO TO(6,7,91,93)IABS(IND)
7 IF(TEST(1).GT.0)GO TO 7
  IND=2
  NBAD=0
  CALL STARTCLOCK
  CALL ENABLE
5 CCONTINUE
10 GO TO 5
11 NB=-NB
  NEWBUF=LOCB(NB)
  IF(TEST(1).GT.0.OR.RECNUM.GE.NREC)CALL DISABLE
  GO TO(90,12,91,92)IABS(IND)
12 CONTINUE
  IF(IND.GT.0)CALL MTOUT(NB)
  IF(IND.LT.0)CALL MTOUT1(NB)
  IF(TEST(1).LT.0.AND.RECNUM.LT.NREC)GO TO 5
  CALL STOPCLOCK
  CALL ADSTOP
  CALL PROCESS(IBUF,NSAMP,NCHAN+1,2S)
  OUTPUT( 6 )RECNUM
  IF NBAD.NE.0,WRITE( 6 ,106) (BADREC(I),I=1,NBAD)
106 FORMAT($ BAD RECORDS ARE,(/,I6))
15 OUTPUT(102)'OPTION=(11)'
  READ(101,100)NOPT
100 FORMAT(I1)
  GO TO(1,2,30,40,50,60,70)NOPT
30 OUTPUT(102)'EOF ON WHICH TAPE'
  READ(101,100)N
  IF N.EQ.0,GO TO 15
  ENDFILE(N)
  GO TO 15
40 OUTPUT(102)'REWIND WHICH TAPE'
  READ(101,100)N
  IF N.EQ.0,GO TO 15
  REWIND(N)
  GO TO 15
50 OUTPUT(102)'SKIP FILES=(14)'
  READ(101,101)NF
101 FORMAT(I4)
  OUTPUT(102)'ON WHICH TAPE'

```



```

      READ(101,100)N
      IF N.EQ.0,GO TO 15
      DO 55 I=1,NF
51     CALL BUFFERIN(N,1,IBUF(1,1),1,IN )
52     IF(IN .LT.2)GO TO 52
      IF(IN .NE.3)GO TO 51
55     CONTINUE
      OUTPUT(102)NF
      GO TO 15
60     OUTPUT(102)'NUMWORDS TO LIST=(14) '
      READ(101,101)NW
      OUTPUT(102)'FROM WHICH TAPE '
      READ(101,100)N
      IF N.EQ.0,GO TO 15
601    IN =1
      CALL BUFFERIN(N      ,1,IBUF(1,1),NWORDS,IN )
66     IF(IN .EQ.1)GO TO 66
62     GO TO(62,63,64,65)IN
63     WRITE(6,102)
102    FORMAT(1H1)
      DO 631 I=1,NW,NCHAN
104    WRITE(6,104)(IBUF(J,1),J=I,I+NCHAN-1)
631    FORMAT(12G10)
      CONTINUE
      IF (SENSE SWITCH 1)601,15
64     OUTPUT(102)'EOF READ '
      GO TO 15
65     OUTPUT(102)'READ ERR '
      GO TO 63
70     OUTPUT(102)'D/A FROM WHICH TAPE '
      READ(101,100)N
      IF N.EQ.0,GO TO 15
      OUTPUT(102)'TYPE * C/R TO CONTINUE '
      INPUT(101)
77     IN =1
      CALL BUFFERIN(N      ,1,IBUF,NWORDS,IN )
76     IF(IN .EQ.1)GO TO 76
71     GO TO(71,72,64,74)IN
72     DO 73 I=1,NWCROS
73     IBUF(I,1)=IBUF(I,1)/2*10
      DO 75 I=1,NWORDS,NCHAN
      DO 750 J=1,NCHAN
750    CALL DAC(J,IBUF(I+J-1,1))
      M=NDEL
      CALL DELAY
75     CONTINUE
      IF(SENSE SWITCH 1)77,15
74     OUTPUT(102)'READ ERROR '
      GO TO 72
90     CALL DISABLE
      CALL ADSTOP
      OUTPUT(102)'RATE ERR',RECNUM
      GO TO 15
92     IF NBAD.LT.100,NBAD=NBAD+1
      BADREC(NBAD)=RECNUM-1
      GO TO 12
91     CALL DISABLE
      CALL ADSTOP
      OUTPUT(102) - MT NOT READY -
      GO TO 15
93     CALL DISABLE
      CALL ADSTOP
      OUTPUT(102) - MT ERROR ON SPACING FROM LOAD POINT-
      GO TO 15
94     OUTPUT(102)'DELAY TIME BETWEEN RECORDS TOO SHORT '
      GO TO 15
      END

```



```
1  SUBROUTINE PROCESS(I,N,NC,IR)
    J=N*NC*9
    CALL DELAY
    IF TEST(1).LT.0,GO TO 1
    IF TEST(2).GT.0,RETURN IR
    RETURN
    END
```



# APPENDIX B

LISTING OF FORTRAN PROGRAM TO READ FROM  
SEVEN TRACK TAPE, CONVERT FROM OCTAL TO  
HEXADECIMAL, AND STORE RESULT ON DISK

```
//CONVERT EXEC FORICLG,REGION.GO=100K
//FORT.SYSIN DD *

DIMENSION IDAT(3072), DAT(3072)
FACTOR=100./(2**23)
REWIND 2
NRECL = 3072
J=0
10 READ(2,15,END=50,ERR=60) IDAT
15 FORMAT (16(192A4))
J=J+1
70 WRITE (6,70) J
FORMAT ('0',10X,'RECORD NO.=' ,I4)
CALL FORM(IDAT,NRECL)
DO 22 I=1,NRECL
22 DAT(I)=IDAT(I)*FACTOR
40 WRITE (6,40) (DAT(I),I=1,180)
FORMAT (1X,6F12.5)
WRITE (4) DAT
GO TO 10
60 WRITE(6,61) J
61 FORMAT ('0',5X,'READ ERROR RECORD NO.=' ,I3)
GO TO 10
50 WRITE (6,51) J
51 FORMAT ('0',5X,'END OF TAPE, RECORD NO.=' ,I3)
ENDFILE 4
RETURN
END

//GO.FT02F001 DD UNIT=2400-1,VOL=SER=BOLEY,LABEL=(9,NL,,IN),
// DISP=OLD,DCB=(DEN=1,RECFM=F,BLKSIZE=12288)
//GO.FT04F001 DD UNIT=2314,DSNAME=S0896.TAPESS,DISP=(NEW,KEEP),
// VOL=SER=DUFFY,
// LABEL=RETPD=120,SPACE=(TRK,(2,2),RLSE),
// DCB=(RECFM=VS,BLKSIZE=3504,LRECL=3000)
```



# APPENDIX C

LISTING OF FORTRAN PROGRAM TO READ FROM DISK,  
 RESCALE DATA TO MEASURED UNITS, PERFORM SMOOTHING,  
 AND STORE THE RESULT ON DISK

```

// EXEC FORTCLGP,REGION.GO=200K
//FORT.SYSIN DD *

INTEGER*4 ITB(12)/12*0/
REAL*4 RTB(28)/28*0.0/
EQUIVALENCE (ITITLE,RTB(5))
REAL*8 ITITLE(12)
DIMENSION TP(2000),TS(2000),HT(2000),PANG(2000),PB(2000),
1VK(2000),TTHST(200),PITCH(200),PBUB(200),SPD(200),DRFT(200),
2TIME(200)
110 READ (5,110) NPTS
    FORMAT (I4)
    M=500
    N=1
    DO 5 K=1,4
      READ (4) (TP(I),TS(I),HT(I),PANG(I),VK(I),PB(I),I=N,M)
      N=500+N
      M=500+M
5    CONTINUE
      CALL SMOOTH (TP)
      CALL SMOOTH (TS)
      CALL SMOOTH (HT)
      CALL SMOOTH (PANG)
      CALL SMOOTH (VK)
      CALL SMOOTH (PB)
      DO 10 J=1,200
        K=J
        TTHST(J)=(TP(K)+TS(K))*10.
        PITCH(J)=(PANG(K)-25.)*0.6
        PBUB(J)=PB(K)*1.2
        SPD(J)=VK(K)*0.8
        HT(J)=(100.-HT(K))*0.48
        DRFT(J)=48.0-HT(J)-3.19335*PITCH(J)
        TIME(J)=(J-1)*0.05
10    CONTINUE
        WRITE(6,165) (I,TTHST(I),DRFT(I),PITCH(I),SPD(I),PBUB(I),I=1,200)
  
```



```

165  FORMAT(/3X,I4,5F12.4)
      WRITE(8)(TTHST(I),DRFT(I),PITCH(I),SPD(I),PBUB(I),I=1,200)
100  READ (5,100) TITLE
      FORMAT (6A8)
      CALL DRAWP(NPTS,TIME,TTHST,ITB,RTB)
      READ (5,100) TITLE
      CALL DRAWP(NPTS,TIME,PITCH,ITB,RTB)
      READ (5,100) TITLE
      CALL DRAWP(NPTS,TIME,PBUB ,ITB,RTB)
      READ (5,100) TITLE
      CALL DRAWP(NPTS,TIME,SPD ,ITB,RTB)
      READ (5,100) TITLE
      CALL DRAWP(NPTS,TIME,DRFT ,ITB,RTB)
      STOP
      END

      SUBROUTINE SMOOTH (VBLE)
      DIMENSION VBLE(2000)
      SUM=0.0
      N=1
      M=10
      DO 210 I=1,200
      DO 205 K=N,M
      SUM=SUM+VBLE(K)
205  CONTINUE
      VBLE(I)=0.1*SUM
      N=N+5
      M=M+5
      SUM=0.0
210  CONTINUE
      RETURN
      END

      //GO,F104F001 DD DISP=SHR,DSN=S0896,TAPESS,UNIT=2314,VOL=SER=DUFFY,
      // LABEL=(, , IN),DCB=(RECFM=VS,BLKSIZE=3504,LRECL=3000)
      //F108F001 DD DSN=S0896-DA1A10,UNIT=2314,VOL=SER=MARY,DISP=(NEW,KEEP),
      // LABEL=RETPD=180,DCB=(RECFM=VS,LRECL=4004,BLKSIZE=7290),
      // SPACE=(TRK,(2,1))

```



# APPENDIX D -----

## LISTING OF FORTRAN XR-3 SIMULATION PROGRAM

```

100
99
101
105
102
104

INTEGER ON
COMMON /AIR/ PINF,RHOINF,GAM
COMMON /BMCO / IMM,IMNX,IMNY,IBMFIL,BTIME,IMT,XMI(10),YMI(7),IX,IY
COMMON /CONST/ PI,RAD,UO
COMMON /ENGINE/NPS,NPP,THSTS(25),THSTP(25),XP,YP,ZP,STHS,SIHP,
ATIP(25),TIS(25)
COMMON /EQNCO/ NEQS,TCL(20),JQQ
COMMON /FPROP/ FXP,FYP,FZP,FKP,FMP,FNP
COMMON / FROUDE / FN,FNCKIT
COMMON / PRIME/ STIME,ETIME,DELT,DELPNT,TPRINT
COMMON /PRINT/ON,IACCEL,IVEL,ITRAJ,ISIDLW,IBOWSL,ISTNSL,IWAVES,
-IRUD,IPROP,IAERUD,IRHS
COMMON /KOLL/ PHIMAX,TROLL
COMMON/RUDDER/ NPR,DELRUD(25),XR,YR,ZR,IRDS,TL,RSPAN,RAREA,RASPR,
ARCLB,RTC,RUDANG,TIR(25)
COMMON / VALOLD / YULD(20)
COMMON /VARBLE/ VAL(40)
COMMON /WAVE/ ETA(4,11),AW(10),OMEGA(10),DVOLW,NWAVE,BETA,
FXWAV,FYWAV,FZWAV,FKWAV,FMWAV,FNWAV
,ZBAR,PHIBAR,THEBAR,TC,COSBET,SINBET,PBBAR
EQUIVALENCE
1(VAL(5),P),(VAL(6),Q),(VAL(7),R),(VAL(8),PHI),(VAL(9),THETA),
2(VAL(10),Z),(VAL(11),BMASS),(VAL(21),X),(VAL(22),Y),(VAL(23),PSI),
3(VAL(24),PB)
DIMENSION DUMMY(20)
TC=1.0
ON=1
PI=4.*ATAN(1.)
RAD=180./PI
WRITE(6,100)
FORMAT(1H1//35X,22H LISTING OF INPUT DECK //)
READ(44,101,END=104) DUMMY
FORMAT(20A4)
WRITE(6,102) DUMMY
WRITE(5,101) DUMMY
FURMAT(5X,20A4)
GO TO 99
REWIND 5

```



```

11 CALL INCON(TIME)
   IF (IMM.EQ.3) GO TO 605
10 DO 10 J=1,20
   YOLD(J)=VAL(J+1)
   GO TO 2
1 CONTINUE
  TOLD=TIME
  PBBAR=PBBAR*(1.-DELT/TC)+DELT*(PB-PINF)/TC
  IF ( N WAVE .LE.0 ) GO TO 13
  ZBAR=(1.-DELT/TC)*ZBAR+DELT*Z/TC
  PHIBAR=(1.-DELT/TC)*PHIBAR+DELT*PHI/TC
  THEBAR=(1.-DELT/TC)*THEBAR+DELT*THETA/TC
  CALL WAVES(TIME)
13 CALL SIDEWL
   CALL PROP
   CALL RUDDER
   CALL AERCD
   CALL INTCRL(TIME)
   IF (TIME.GT.FTIME) GO TO 12
   IF ( FN.GT.FNCRIT) GO TO 14
   PRINT 505
   GO TO 12
14 DELOLD=TIME-TOLD
   PSI=PSI+DELOLD*R
   X=X+DELOLD*(U*COS(PSI)-V*SIN(PSI))
   Y=Y+DELOLD*(U*SIN(PSI)+V*COS(PSI))
15 IF (ABS(TIME-TPRINT) .LT. 1.E-6) GO TO 2
   GO TO 1
2 CONTINUE
  IF (ITRAJ .EQ. 0) GOTO 16
  DPHI=PHI*RAD
  DPSI=PSI*RAD
  DTHETA=THETA*RAD
  DP=P*RAD
  DQ=Q*RAD
  DR=R*RAD
  VEL=0.5925*U
  WRITE (6,500) TIME,VEL,V,W,DP,DQ,DR,Z,DPHI,DTHETA,X,Y,DPSI
  BETS=(-V/U)*RAD
  DELRS=RUDANG*RAD
  WRITE(6,501) BETS,DELRS,FXP
16 CONTINUE
   IMM1AG = (IMM+1)/2

```



```

IF (IMMTAG.EQ.1).AND. TIME.GE.BTIME-1.E-8 ) IMT = 1
TPRINT=TPRINT+DELPT
QN=1
GO TO 1

12 CALL COLFIL
IF (IMM.LT.1) GO TO 11
IF (IMM.NE.1) GO TO 605
END FILE IBMFIL
GO TO 11
605 CALL SAM
GO TO 11
500 FORMAT(/10X,13HTIME (SEC) = F6.2//10X,33HTRANSLATIONAL VELS (KTSMAIN1030
1)/(FT/SEC) /10X,2HU= F6.2,5X,2HV= F6.3//10X,31HROTATIMAIN1040
2ONAL VELOCITIES (DEG/SEC) /10X,2HP= F6.2,5X,2HQ= F6.2,5X,2HR= F6.2MAIN1050
3//10X,30HDISPLACEMENTS (FT AND DEGREES) /10X,2HZ= F7.3,5X,4HPhi=
4F6.2,3X,6HHETA= F6.2//10X,27HTRAJECTORY (FT AND DEGREES) /10X,
52HX= F8.2,4X,2HY= F8.2,4X,4HPSI= F8.2)
501 FORMAT(1H0,9X,23HSLIP ANGLE (DEG) = F8.2,10X,21HRUDDER ANGLEMAIN1080
1 (DEG) = F8.3,10X,15HTHRUST (LBS) = F12.1)
505 FORMAT(/10X,28HCRAFT SPEED BELOW HUMP SPEED )
END
BLOCK DATA
COMMON /AIR/ Z1(3)
COMMON /BMCO/ Z2(25)
COMMON /COLUMN / Z3(2)
COMMON /CONST/ Z4(3)
COMMON /CNTRL/ Z5(10)
COMMON /ENGINE/ Z6(107)
COMMON /EQNCO/ Z7(22)
COMMON /FAERO/ Z8(6)
COMMON /FAIR/ Z9(2)
COMMON /FANMAP/ Z10(262)
COMMON /FORBS/ Z11(7)
COMMON /FORSS/ Z12(8)
COMMON /FPRUP/ Z13(6)
COMMON /FROUDE/ Z14(2)
COMMON /FRUD/ Z15(6)
COMMON /GBOW/ Z16(1)
COMMON /GEOM/ Z17(138)
COMMON /GEOMBS/ Z18(62)
COMMON /GEOMSS/ Z19(62)
COMMON /GEU4SW/ Z20(11)
COMMON /KSWTCH/ Z21(1)
COMMON /LEAKER/ Z22(4)
COMMON /MASSES/ Z23(817)
COMMON /MATRIX/ Z24(36)
COMMON /MSIDW/ Z25(55)

```



COMMON /MWAVE/ Z26(12)  
COMMON /OPTION/ Z27(4)  
COMMON /PLENUM/ Z28(4)  
COMMON /PLVCQQ/ Z28A(4)  
COMMON /PRIME/ Z29(5)  
COMMON /PRINT/ Z30(12)  
COMMON /PWAVE/ Z31(2)  
COMMON /RISER/ Z32(1)  
COMMON /ROLL/ Z33(2)  
COMMON /RUDDR/ Z34(62)  
COMMON /SIDE/ Z35(22)  
COMMON /SOFTBS/ Z36(19)  
COMMON /SOFTSS/ Z37(19)  
COMMON /STABLE/ Z38(5)  
COMMON /STSLR/ Z39(2)  
COMMON /VALULD/ Z40(20)  
COMMON /VARIABLE/ Z41(40)  
COMMON /WAVE/ Z42(80)  
COMMON /WAVEF/ Z43(40)  
COMMON /SLOPE/ Z44(4)  
DATA Z1/3\*0.0/  
DATA Z2/25\*0.0/  
DATA Z3/2\*0.0/  
DATA Z4/3\*0.0/  
DATA Z5/10\*0.0/  
DATA Z6/107\*0.0/  
DATA Z7/21\*0.0/  
DATA Z8/6\*0.0/  
DATA Z9/2\*0.0/  
DATA Z10/262\*0.0/  
DATA Z11/7\*0.0/  
DATA Z12/8\*0.0/  
DATA Z13/6\*0.0/  
DATA Z14/2\*0.0/  
DATA Z15/6\*0.0/  
DATA Z16/0.0/  
DATA Z17/138\*0.0/  
DATA Z18/62\*0.0/  
DATA Z19/62\*0.0/  
DATA Z20/11\*0.0/  
DATA Z21/0.0/  
DATA Z22/4\*0.0/  
DATA Z23/817\*0.0/  
DATA Z24/36\*0.0/  
DATA Z25/55\*0.0/  
DATA Z26/12\*0.0/  
DATA Z27/4\*0.0/  
DATA Z28/4\*0.0/

MAIN1390  
MAIN1400  
MAIN1410  
MAIN1420  
MAIN1430  
MAIN1440  
MAIN1450  
MAIN1460  
MAIN1470  
MAIN1480  
MAIN1490  
MAIN1500  
MAIN1510  
MAIN1520  
MAIN1530  
MAIN1540  
MAIN1550  
MAIN1560  
MAIN1570  
MAIN1580  
MAIN1590  
MAIN1600  
MAIN1610  
MAIN1620  
MAIN1630  
MAIN1640  
MAIN1650  
MAIN1660  
MAIN1670  
MAIN1680  
MAIN1690  
MAIN1700  
MAIN1710  
MAIN1720  
MAIN1730  
MAIN1740  
MAIN1750  
MAIN1760  
MAIN1770  
MAIN1780  
MAIN1790  
MAIN1800  
MAIN1810  
MAIN1820  
MAIN1830  
MAIN1840  
MAIN1850  
MAIN1860



```

DATA Z28A/4*0.0/
DATA Z29/5*0.0/
DATA Z30/12*0.0/
DATA Z31/2*0.0/
DATA Z32/0.0/
DATA Z33/2*0.0/
DATA Z34/62*0.0/
DATA Z35/22*0.0/
DATA Z36/19*0.0/
DATA Z37/19*0.0/
DATA Z38/5*0.0/
DATA Z39/2*0.0/
DATA Z40/20*0.0/
DATA Z41/40*0.0/
DATA Z42/80*0.0/
DATA Z43/40*0.0/
DATA Z44/4*0.0/
END

```

```

MAIN1870
MAIN1880
MAIN1890
MAIN1900
MAIN1910
MAIN1920
MAIN1930
MAIN1940
MAIN1950
MAIN1960
MAIN1970
MAIN1980
MAIN1990
MAIN2000
MAIN2010
MAIN2020
MAIN2030
MAIN2040

```

```

SUBROUTINE AEROD
INTEGER ON
COMMON /FAERO/ FX,FY,FZ,FK,FM,FN
COMMON /FAIR/ RHOA,XLAERO
COMMON /PRINT/ON,IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,
-IRUD,IPROP,IAEROD,IRHS
COMMON /VARBLE/ VAL(40)

EQUIVALENCE
1(VAL(5),PI),(VAL(6),Q),(VAL(7),R),(VAL(8),PHI),(VAL(9),THETA),
2(VAL(10),Z),(VAL(11),BMASS),(VAL(21),X),(VAL(22),Y),(VAL(23),PSI),
3(VAL(24),PB)
QA=RHOA*U*U
QAL=QA*XLAERO
BETA=-V/U
BETASQ=BETA*BETA
FX=-(0.90*BETASQ+0.53*BETA)*QA
FY=(0.0*BETASQ+0.53*BETA)*QA
FZ=-(2.06*BETASQ+0.39)*QA
FK=-(0.5*BETASQ+0.0*BETA)*QAL
FM=(0.29*BETASQ+0.12)*QAL
FN=(0.0*BETASQ+0.07*BETA)*QAL

IF (IAEROD.NE.ON) RETURN
WRITE(6,100) FX,FY,FZ,FK,FM,FN
100 FORMAT(/1CX,23HAEROD FX,FY,FZ,FK,FM,FN/6E15.4)
RETURN
END

```

```

AER 0020
AER 0030
AER 0040
AER 0050
AER 0060
AER 0070
AER 0080
AER 0090
AER 0100
AER 0110
AER 0120
AER 0130
AER 0140
AER 0150
AER 0160
AER 0170
AER 0180
AER 0190
AER 0200
AER 0210
AER 0220
AER 0230
AER 0240
AER 0250
AER 0260
AER 0270
AER 0280
AER 0290

```



```

SUBROUTINE BOWSL
  INTEGER ON
  COMMON /AIR/ PINF, RHOINF, GAM
  COMMON /CONST/ PI, RAD, UO
  COMMON /FORBS/ FX, FY, FZ, FK, FM, FN, QL
  COMMON /GEOM/ WIDTH, XL, XX(4,11), YY(4,11), NSTA(4), AB, VOLNOM
  1, DELS(4,10), XCP, ZCP
  COMMON /GECNBS/DETABX(11), DETABT(11), ARM1B(10), ARM2B(10)
  1, DFBS(10), TSKIB(10)
  COMMON /LEAKER/ALEAK, BLEAK, CFSS, CFBS
  COMMON /MASSES/ AM, AIXX, AIYY, AIZZ, AIXZ, AIMAX, G, WEIGHT, RHO, NMASS,
  COMMON /IRUD, IPROP, IAEROD, IRHS
  COMMON /SLGPE/WATSLP, XPWV, XLX, PWV, XPBS, XBS, ZBS, DELYBS, DPBS, ELMAXB, YAVG
  COMMON /SUFTRS/XBF, PBS, SINBS, COSBS, X3S, Z3S
  18(10)
  COMMON /VARBLE/ VAL(40)
  COMMON /WAVE/ ETA(4,11), AW(10), OMEGA(10), DVOLW, NWAVE, BETA,
  1 FXWAV, FYWAV, FZWAV, FKWAV, FMWAV, FNWAV
  2 ZBAR, PHIBAR, THEBAR, TC, COSBET, SINBET, PBBAR
  DIMENSION GAP(11), ELSKI(11)
  DIMENSION WTAB(6), ZTAB(6)
  DATA NPTS, IBS/6, 0/
  DATA WTAB/0.0, 3.75, 5.42, 6.67, 7.5, 8.42/
  DATA ZTAB/3.75, 4.00, 4.42, 4.83, 5.25, 5.67/
  DATA ENU, UWSKI, CLSKI/1.28E-05, 0.0, 1.5708/
  EQUIVALENCE (VAL(1), TIME), (VAL(2), U), (VAL(3), V), (VAL(4), W),
  1 (VAL(5), P), (VAL(6), Q), (VAL(7), R), (VAL(8), PHI), (VAL(9), THETA),
  2 (VAL(10), Z), (VAL(11), BMASS), (VAL(21), X), (VAL(22), Y), (VAL(23), PSI),
  3 (VAL(24), PB)
  DO 5 J=1,11
    GAP(J)=0.0
    ELSKI(J)=0.0
  5 CCNTINUE
  ALBS=0.0
  FX=0.0
  FZ=0.0
  FK=0.0
  FM=0.0
  FN=0.0
  DELPBG=PBS-PB
  IF(DELPG.LT.0.0) DELPBG=0.0
  PPAK=PB-PINF
  DELP=PBAR
  IF(DELP.LT.0.0)DELP=0.0
  BWSL0010
  BWSL0020
  BWSL0030
  BWSL0040
  BWSL0050
  BWSL0060
  BWSL0070
  BWSL0080
  BWSL0090
  BWSL0100
  BWSL0110
  BWSL0120
  BWSL0130
  BWSL0140
  BWSL0150
  BWSL0160
  BWSL0170
  BWSL0180
  BWSL0190
  BWSL0200
  BWSL0210
  BWSL0220
  BWSL0230
  BWSL0240
  BWSL0250
  BWSL0260
  BWSL0270
  BWSL0280
  BWSL0290
  BWSL0300
  BWSL0310
  BWSL0320
  BWSL0330
  BWSL0340
  BWSL0350
  BWSL0360
  BWSL0370
  BWSL0380
  BWSL0390
  BWSL0400
  BWSL0410
  BWSL0420
  BWSL0430
  BWSL0440
  BWSL0450
  BWSL0460

```



```

SINDIF=SINBS-COSBS*THETA
COSDIF=COSBS+SINBS*THETA
X1=XBS+ZBS*THETA-XBF*SINDIF
Z1=-Z-ZBS+XBS*THETA-XBF*COSDIF
N=NSTA(3)
DO 10 K=1,N
  ELSKI(K)=(ETA(3,K)-DETABX(K)*(XX(3,K)-X1)-Z1)+YY(3,K)*PHI
  1+XLXPWV*WATSLP
  1 GAP(K)=-ELSKI(K)
  IF(GAP(K).LT.0.0) GAP(K)=0.0
  10 CONTINUE
  N=NSTA(3)-1
  DO 20 J=1,N
    ELSK1A=(ELSKI(J+1)+ELSKI(J))/2.0
    IF(ELSK1A.LE.0.0) GO TO 15
    IF(ELSK1A.GT.ELMAXB) ELSK1A=ELMAXB
    ARM1B(J)=XX(3,J)+ELSK1A/2.0
    ARM2B(J)=ZS-ELSK1A
    DFBS(J)=-DELP*ELSK1A*DELYBS
    ARG=0.5*RHO*U*ELSK1A*DELYBS
    RESK1=U*ELSK1A/ENU
    CDTSKI=0.427/(ALOG10(RESK1)-0.407)**2.64
    TSKIB(J)=-ARG*CDTSKI
    GO TO 18
  15 DFBS(J)=0.0
  18 TSKIB(J)=0.0
    CONTINUE
    FX=FX+TSKIB(J)
    FZ=FZ+DFBS(J)
    FK=FK+DFBS(J)*YAVGB(J)
    FM=FM-DFBS(J)*ARM1B(J)+TSKIB(J)*ARM2B(J)
    FN=FN-TSKIB(J)*YAVGB(J)
    ALBS=ALBS+(GAP(J)+GAP(J+1))*DELYBS/2.0
  20 CONTINUE
    ALBS=ALBS+BLEAK
    QL=CFBS*ALBS*SWRT(2.0*ABS(PBAR.)/RHOINF)*SIGN(1.0,PBAR)
    IF(1BOWSL.NE.ON) RETURN
    WRITE(6,100) GAP,ELSKI,FX,FY,FZ,FK,FM,FN
  100 FORMAT(/10X,8HBOV SEAL/26H GAP (FI.) (PORT TO STBU.) /11F10.5
    2K,FM,FN/6E15.4)
    2K,FM,FN/6E15.4)
    RETURN
  END

```

CFL 0020  
 CFL 0070  
 CFL 0080

SUBROUTINE COLFIL  
 COMMON/AXIS/NXYS(26)  
 COMMON/COLUMN/IVERT,ILATRL



```

COMMON /CURVE/NCURV(10)
COMMON/EQNCO/ NEQS,TOL(20), JQQ
COMMON/GRAF/NGRAF,NORW
COMMON /HEADG/TICRD(6)
COMMON/STEP/ STEP2
COMMON /SUM/ ISUM1(8), ISUM2(8)
REAL*8 TICRD
REAL LABEL
REAL LAB(4)
REAL*8 NAMES(52)
1SPLA, 'CEMENT', 'PITCH AN', 'GLE', 'WAVE HEI', 'GHT', 'Z DICFL
2ACCE, 'LERATION', 'C.G.ACCE', 'LERATION', 'PLENUM P', 'RESSURE', 'BOW CFL
3L ANG, 'LE WATER', 'TURN RAD', 'IUS', 'LAT ACCE', 'LERATION', 'SPECFL
4ED TH, 'RU CEMENT', 'Y DISPLA', 'CEMENT', 'AIR FLOW', 'IN', 'AIRCFL
51SPLA, 'CEMENT', 'NET FORC', 'E X DIR', 'WAVE FOR', 'CE X DIR', 'NETCFL
6 FLOW, 'OUT', 'NET FORC', 'E Z DIR', 'NET TORQ', 'UE X AXIS', 'NETCFL
7 FORC, 'E Y DIR', 'NET FORC', 'E Z DIR', 'NET TORQ', 'UE X AXIS', 'NETCFL
8 TORQ, 'UE Y AXIS', 'NET TORQ', 'UE Z AXIS', 'RUDDER A', 'NGLE', 'CFL
REAL*8 TITLE(12)
REAL*8 LINE2(2)
REAL*8 LINE2(2)/ 'PLOT IS ', ' VERSUS ' /
REAL*8 NAMEX(2), NAMEY(2), INAME(16)
EQUIVALENCE (TITLE(1),TICRD(1)),(TITLE(2),TICRD(2)),(TITLE(3),TI
TICRD(3)),(TITLE(4),TICRD(4)),(TITLE(5),TICRD(5)),(TITLE(6),TICRD(
26))
DIMENSION PVQQ(26),XOUT(900),YOUT(900),AFILE(8)
EQUIVALENCE (PVQQ(1),TIME),(PVQQ(2),ETA),(PVQQ(3),Z),(PVQQ(4),THETCFL
14),(PVQQ(5),PB),(PVQQ(6),BOWACC),(PVQQ(7),ACC),(PVQQ(8),FANPWR),(PCFL
2VQQ(9),PHI),(PVQQ(10),BETAS),(PVQQ(11),ACCLAT),(PVQQ(12),U),(PVQQ(13
313),TRADUS),(PVQQ(14),R),(PVQQ(15),X),(PVQQ(16),Y),(PVQQ(17),QIN),CFL
4(PVQQ(18),QOUT),(PVQQ(19),GFXX),(PVQQ(20),FXPWAV),(PVQQ(21),GF2),CFL
5(PVQQ(22),GF3),(PVQQ(23),GF4),(PVQQ(24),GF5),(PVQQ(25),GF6),CFL
6(PVQQ(26),DELS)
IF(JQQ.NE.2) GO TO 1
WRITE(6,777) STEP2
777 FORMAT(0,'4X, THIS RUN USED VARIABLE STEP SIZE',/, '0',4X, 'THE MINC
1 1 MIN STEPSIZE RECORDED DURING THE RUN WAS',2X,E30.5)
1 REWIND 1
TITLE(7)=LINE2(1)
TITLE(10)=LINE2(2)
IF(NGRAF.EQ.0) GO TO 11
J=1
NCF=NGRAF
INDEX=NGRAF*2
DO 19 I=1,INDEX,2
INDEX=NXYS(I)
INDY=NXYS(I+1)
IQ=0

```







```

INAME(J)=NAMES( IDEX-1)
INAME(J+1)=NAMES( IDEX)
J=J+2
33 CONTINUE
WRITE(6,300)( INAME(I), I=1,N)
300 FORMAT( '0',16A8)
GO TO 4
26 ENDFILE 2
REWIND 2
NGF=NGRAF
J=1
27 READ(2,END=38) IQ,NCUR,NGRAF,LABEL,(TITLE(K),K=1,12),(XOUT(L),YOUT(
1L),L=1,IQ)
IF((NGF.EQ. NGRAF).AND.(NCUR.EQ. J)) GO TO 29
GO TO 27
29 LABEL=LAB(J+1)
CALL DRAW(IQ,XOUT,YOUT,NCUR,0,LABEL,TITLE,0,0,0,0,8,8,0,0,LAST)
REWIND 2
J=J+1
IF(J.EQ.4) GO TO 38
GO TO 27
38 NGF=NGF-1
IF(NGF.EQ.0) GO TO 11
J=1
GO TO 27
4 READ(1,END=13)(PVQQ(I),I=1,26)
DO 35 I=1,NUM1
J=ISUM1(I)
35 AFIL(I)=PVQQ(J)
WRITE(6,400)(AFIL(I),I=1,NUM1)
400 FORMAT( '0',8(3X,F10.2,3X))
GO TO 4
13 REWIND 1
14 IF(ILATRL.NE.1) GO TO 17
WRITE(6,200)
200 FORMAT( '0',50X,'***SUMMARY TWO***',/, '0')
K=0
DO 32 I=1,8
IF( ISUM2(I).NE.0) K=K+1
32 CONTINUE
NUM2=K
IF(K.EQ.0) GO TO 16
N=K*2
J=1
DO 34 I=1,NUM2
IDEX= ISUM2(I)*2
INAME(J)=NAMES( IDEX-1)
INAME(J+1)=NAMES( IDEX)

```



```

34 J=J+2
   CONTINUE
23   WRITE(6,300)(I,NAME(I),I=1,N)
   READ(1,END=16)(PVQQ(I),I=1,26)
   DO 36 I=1,NUM2
     J=ISUM2(I)
36   AFILE(I)=PVQQ(J)
   WRITE(6,400)(AFILE(I),I=1,NUM2)
   GO TO 23
16 REWIND 1
17 RETURN
   END

```

```

CFL 1530
CFL 1540
CFL 1550
CFL 1560
CFL 1570
CFL 1580
CFL 1590
CFL 1600
CFL 1610
CFL 1620
CFL 1650
CFL 1640

```

C

```

SUBROUTINE DMINV (A,N,D)
DIMENSION A(6,6),PIVOT(6)
DIMENSION IPVOT(6),INDEX(6,2)
EQUIVALENCE (IROW,JROW),(ICOL,JCOL)
D=1.0
DO 17 J=1,N
  IPVOT(J)=0
17 CONTINUE
DO 135 I=1,N
  T=0.0
  DO 9 J=1,N
    IF(IPVOT(J)-1) 13,9,13
13  DO 23 K=1,N
      IF(IPVOT(K)-1) 43,23,81
43  IF (ABS(T)-ABS(A(J,K))) 83,23,23
83  IROW=J
      ICOL=K
      T=A(J,K)
23 CONTINUE
9  IPVOT(ICOL)=IPVOT(ICOL)+1
  IF(IROW-ICOL) 73,109,73
73  D=-D
  DO 12 L=1,N
    T=A(IROW,L)
    A(IROW,L)=A(ICOL,L)
    A(ICOL,L)=T
12 CONTINUE
  INDEX(I,1)=IROW
  INDEX(I,2)=ICOL
109 PIVOT(I)=A(ICOL,ICOL)
    D=D*PIVOT(I)
    A(ICOL,ICOL)=1.0

```

```

DMV 0010
DMV 0020
DMV 0030
DMV 0040
DMV 0050
DMV 0060
DMV 0070
DMV 0080
DMV 0090
DMV 0100
DMV 0110
DMV 0120
DMV 0130
DMV 0140
DMV 0150
DMV 0160
DMV 0170
DMV 0180
DMV 0190
DMV 0200
DMV 0210
DMV 0220
DMV 0230
DMV 0240
DMV 0250
DMV 0260
DMV 0270
DMV 0280
DMV 0290
DMV 0300
DMV 0310
DMV 0320
DMV 0330
DMV 0340

```



```

205 DO 205 L=1,N
      A(ICOL,L)=A(ICOL,L)/PIVOT(I)
      CONTINUE
      DO 134 LI=1,N
        IF(LI-ICOL) 21,134,21
        T=A(LI,ICOL)
        A(LI,ICOL)=0.0
        DO 89 L=1,N
          A(LI,L)=A(LI,L)-A(ICOL,L)*T
          CONTINUE
        CONTINUE
        CONTINUE
      DO 3 I=1,N
        L=N-I+1
        IF(INDEX(L,1)-INDEX(L,2)) 19,3,19
        JROW=INDEX(L,1)
        JCOL=INDEX(L,2)
        DO 549 K=1,N
          T=A(K,JROW)
          A(K,JROW)=A(K,JCOL)
          A(K,JCOL)=T
          CONTINUE
        CONTINUE
      RETURN
      END
549
3
81

```

C

```

SUBROUTINE FAN
  INTEGER ON
  COMMON /AIR/ PINF,RHOINF,GAM
  COMMON /FANMAP/QIN,QBFAN(25),QMFAN(25),QSFAN(25),ENBFAN,ENMFAN,
1  ENSFAN,BRPM,EMRPM,SRPM,NPTS8,NPTSM,NPTSS
2  ,PBFAN(25),PMFAN(25),PSFAN(25),TMEB(25),DELB(25),NB,TMES(25),
3  DELS(25),NS
  COMMON /PRINT/ON,IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,
- IRUD,IPROP,IAEROD,IRHS
  COMMON/SOFTBS/XBF,PBS,SINBS,COSBS,XBS,ZBS,DELYBS,DPBS,ELMAXB,YAVG
1B(10)
  COMMON /SOFTSS/ XLF,PSS,SINTH,COSTH,XSS,ZSS,DELYSS,DPSS
1  ,LLMAXS,YAVGS(10)
  COMMON /VARBLE/ VAL(40)
  DIMENSION QB(1),QM(1),QS(1),PBOW(1),PM(1),PS(1)
  EQUIVALENCE (VAL(1),TIME),(VAL(2),U),(VAL(3),V),
1  (VAL(4),W),
2  (VAL(5),P),(VAL(6),Q),(VAL(7),R),(VAL(8),PHI),(VAL(9),THETA),
3  (VAL(10),Z),(VAL(11),BMASS),(VAL(12),X),(VAL(21),Y),(VAL(23),PSI),
  (VAL(24),PB)
  EQUIVALENCE (VAL(18),FANPWR)
FAN 0010
FAN 0020
FAN 0030
FAN 0040
FAN 0050
FAN 0060
FAN 0070
FAN 0080
FAN 0090
FAN 0100
FAN 0110
FAN 0120
FAN 0130
FAN 0140
FAN 0150
FAN 0160
FAN 0170
FAN 0180
FAN 0190
FAN 0200
FAN 0210

```



```

EQUIVALENCE (QB,FAN(1),QB(1)),(QM,FAN(1),QM(1)),(QSFAN(1),QS(1)),
1 (PB,FAN(1),PBOW(1)),(PM,FAN(1),PM(1)),(PSFAN(1),PS(1)),
    BRAT=3000/BRPM
    EMRAT=3000/EMRPM
    SRAT=3000/SRPM
    TL=VAL(1)
    IF(NB.EQ.0.0) GO TO 5
    DPBS=FGI(TL,NB,TMEB,DELB,ILB)
    PBS=PB+DPBS
5   IF(NS.EQ.0.0) GO TO 6
    DPSS=FGI(TL,NS,TMES,DELS,ILS)
    PSS=PB+DPSS
6   CONTINUE
    PB1=PBS-PINF
    PB2=PB-PINF
    PB3=PSS-PINF
    PBARB=PB1*BRAT**2
    PBARM=PB2*EMRAT**2
    PBAKS=PB3*SRAT**2
    QBOW=ENBFAN*FGI(PBARB,NPTSB,PBOW,QB,IB)/BRAT
    QMAIN=ENMFAN*FGI(PBARM,NPTSM,PM,QM,IM)/EMRAT
    QSTN=ENSFAN*FGI(PBARS,NPTSS,PS,QS,IS)/SRAT
    QIN=QBOW+QMAIN+QSTN
    FANPWR=(QBOW*PB1+QMAIN*PB2+QSTN*PB3)/550.
    IF (IRHS.NE.ON) RETURN
    WRITE(6,100) QBOW,QMAIN,QSTN,PBARB,PBARM,PBARS
100  FORMAT(//4H FAN /32H Q - BOW,MAIN,STERN (CU FT /SEC) 3F12.1
1    /28H DELP - BOW,MAIN,STERN (PSF) 3F11.2)
    RETURN
END

```

FAN 0220  
 FAN 0230  
 FAN 0240  
 FAN 0250  
 FAN 0260  
 FAN 0270  
 FAN 0280  
 FAN 0290  
 FAN 0300  
 FAN 0310  
 FAN 0320  
 FAN 0330  
 FAN 0340  
 FAN 0350  
 FAN 0360  
 FAN 0370  
 FAN 0380  
 FAN 0390  
 FAN 0400  
 FAN 0410  
 FAN 0420  
 FAN 0430  
 FAN 0440  
 FAN 0450  
 FAN 0460  
 FAN 0470  
 FAN 0480  
 FAN 0490  
 FAN 0500  
 FAN 0510  
 FAN 0520  
 FAN 0530

C

```

FUNCTION FGI(X,N,XT,YT,IX)
DIMENSION XI(1),YT(1)
IF (IX.LT.1) IX=1
IF (IX.GT.N-1) IX=N-1
I=SIGN(1.0,X-XT(IX))
IF (IX.LT.1 .OR. IX.GE.N) GO TO 30
IF (XT(IX).GT.X .OR. X.GT.XT(IX+1)) GO TO 20
C=(X-XT(IX))/(XT(IX+1)-XT(IX))
GO TO 100
IX=IX+1
GO TO 10
C=IX/N
IX=IX-I

```

FGI 0010  
 FGI 0020  
 FGI 0030  
 FGI 0040  
 FGI 0050  
 FGI 0060  
 FGI 0070  
 FGI 0080  
 FGI 0090  
 FGI 0100  
 FGI 0110  
 FGI 0120  
 FGI 0130  
 FGI 0140



100	FG1=YT(IX)+C*(YT(IX+1)-YT(IX))	FG1 0150
	RETURN	FG1 0160
	END	FG1 0170
C		
	SUBROUTINE FORIT(FNT,N,M,A,B,IER)	FRT 0010
	DIMENSION A(1),B(1),FNT(1)	FRT 0020
	CHECK FOR PARAMETER ERRORS	FRT 0030
20	IER=0	FRT 0040
30	IF(M) 30,40,40	FRT 0050
	IER=2	FRT 0060
	RETURN	FRT 0070
40	IF(M-N) 60,60,50	FRT 0080
50	IER=1	FRT 0090
	RETURN	FRT 0100
		FRT 0110
		FRT 0120
		FRT 0130
C 60	COMPUTE AND PRESET CONSTANTS	FRT 0140
	CONTINUE	FRT 0150
	AN=N	FRT 0160
	COEF=2.0/(2.0*AN+1.0)	FRT 0170
	PI=4.*ATAN(1.)	FRT 0180
	CONST=PI*COEF	FRT 0190
	S1=SIN(CONST)	FRT 0200
	C1=COS(CONST)	FRT 0210
	C=1.0	FRT 0220
	S=0.0	FRT 0230
	J=1	FRT 0240
	FNTZ=FNT(1)	FRT 0250
70	U2=0.0	FRT 0260
	U1=C.0	FRT 0270
	I=2*N+1	FRT 0280
		FRT 0290
C 75	FORM FOURIER COEFFICIENTS RECURSIVELY	FRT 0300
	U0=FNT(1)+2.0*C*U1-U2	FRT 0310
	U2=U1	FRT 0320
	U1=U0	FRT 0330
	I=I-1	FRT 0340
	IF(I-1) 80,80,75	FRT 0350
80	A(J)=COEF*(FNTZ+ C*U1-U2)	FRT 0360
	B(J)=COEF*S*U1	FRT 0370
	IF(J-(M+1)) 90,100,100	FRT 0380
90	Q=C1*C-S1*S	FRT 0390
	S=C1*S+S1*C	FRT 0400
	C=Q	FRT 0410
	J=J+1	FRT 0420
		FRT 0430



FRT 0440  
FRT 0450  
FRT 0460  
FRT 0470  
FRT 0480

GO TO 70

100

A(1)=A(1)\*0.5  
RETURN  
END

```

SUBROUTINE INCON (TIME)
  REAL*8 TICRD
  INTEGER ON
  COMMON /AIR/ PINF,RHOINF,GAM
  COMMON /AXIS/NXYS(26)
  COMMON /BMCU/ IMM,IMNX,IMNY,IBMFIL,BTIME,IMT,XMI(10),YMI(7),IX,IY
  COMMON /COLUMN/ IVERT,ILATRL
  COMMON /CONST/ PI,RAD,UO
  COMMON /CNTRL/CNTW,CONIQ,CONTH,QMULT,LOUVER,ACONTZ,ACONTW,ZEQUIL
  1,THEQL,ACBASE
  COMMON /CURVE/NCURV(10)
  COMMON /ENGINE/NPS,NPP,THSTS(25),THSTP(25),XP,YP,ZP,STHS,STHP,
  ATIP(25),TIS(25)
  COMMON /EQNCO/ NEQS,TOL(20),JQQ
  COMMON /FAIR/ RHUA,XLAERO
  COMMON /FANMAP/QIN,QBFAN(25),QM,FAN(25),QSFAN(25),ENBFAN,ENMFAN,
  1 ENSFAN,BRPM,EMRPM,SKPM,NPTSB,NPTSM,NPTSS
  2 ,PSFAN(25),PMFAN(25),PSFAN(25),TMEB(25),DELB(25),NB,TMES(25),
  3 DETS(25),NS
  COMMON / FROUDE / FN,FNCRIT
  COMMON /GBOW/ XBOV
  COMMON /GEOM/ WIDTH,XL,XX(4,11),YY(4,11),NSTA(4),AB,VOLNOM
  1,DELS(4,10),XCP,ZCP
  COMMON /GEOMSW/ XAVG(10),DS
  COMMON /GRAF/NGRAF,NDRW
  COMMON /HEADG/TICRD(6)
  COMMON /PWAVE/ FNCON,PWVCON
  COMMON /LEAKER/ALFAK,BLEAK,CFSS,CFBS
  COMMON /MASSES/ AM,AIXX,AIYY,AIZZ,AIXZ,AIMAX,G,WEIGHT,RHO,NMASS,
  - AMI(20),XI(20),YI(20),ZI(20),XS,ZS,HRHO
  COMMON /MATRIX/ A(6,6)
  COMMON /OPTION/ I3DOF,ISRGE,ITRIM,NVALID
  COMMON /PLENUM/XLBW,XBBW,ABW,BUBHGT
  COMMON /PLVCQ/NVI,NVD,NLI,NLD
  COMMON /PRIME/ STIME,DELTIME,DELPT,DELPTNT,TPRINT
  COMMON /PRINT/ON,IACCEL,IVEL,ITRAJ,ISLOWL,IBOWSL,ISTNSL,IWAVES,
  - ITRUD,IPROP,IAEROD,IIRS
  COMMON /ROLL/ PHIMAX,TKOLL
  COMMON /RUDDR/ NPR,DELRUD(25),XR,YR,ZR,IRDS,TL,RSPAN,RAREA,RASPR,
  ARCLB,RTC,RUDANG,TIR(25)
  COMMON /RISER/ AMPTC

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INCN0010  
INCN0020  
INCN0030  
INCN0040  
INCN0050  
INCN0060  
INCN0070  
INCN0080  
INCN0090  
INCN0100  
INCN0110  
INCN0120  
INCN0130  
INCN0140  
INCN0150  
INCN0160  
INCN0170  
INCN0180  
INCN0190  
INCN0200  
INCN0210  
INCN0220  
INCN0230  
INCN0240  
INCN0250  
INCN0260  
INCN0270  
INCN0280  
INCN0290  
INCN0300  
INCN0310  
INCN0320  
INCN0330  
INCN0340  
INCN0350  
INCN0360  
INCN0370  
INCN0380  
INCN0390  
INCN0400  
INCN0410



```

COMMON /SLOPE/WATSLP,XPWV,XLXPWV,XPWVXS
CCMMCN/SOFTBS/XBF,PBS,SINBS,COSBS,XBS,ZBS,DELYBS,DPBS,ELMAXB,YAVG
18(10)
COMMON /SOFTSS/ XLF,PSS,SINTH,COSTH,XSS,ZSS,DELYSS,DPSS
1,ELMAXS,YAVGS(10)
COMMON /SIDE/FXSH,FYSW,FZSW,FKSW,FMSW,FNSW,ALSW,YSW,XLSW,CFSW,CDSW
1,VAREA,VCHORD,VSPAN,VANGLE,VCOS,VX,VY,VZ ,AVBMSW,DELX,VTC
COMMON /STABLE/ S(4),ISTAB
COMMON /STSLR/ CPHI,CPHID
COMMON /SUM/ ISUM1(3),ISUM2(8)
COMMON /VALOLD / YOLD(20)
COMMON /VARBLE/ VAL(40)
COMMON /WAVE/ ETA(4,11),AW(10),OMEGA(10),DVOLW,NWAVE,BETA,
FXWAV,FYWAV,FZWAV,FWWAV,FNWAV
ZBAR,PHIBAR,THEBAR,TC,COSBET,SINBET,PBBAR
COMMON /WAVEF/WAVLEN(10),OMEGAF(10),WAVSLP(10),ENCPER(10)
COMMON /WAVTAB/ NAL,DAL,SAL,NDS,SDS,NTH,DTH,STH,NBB,DBB,SBB,
AC1(20,5,7),AC2(20,5,7),AC3(20,5,7),AC4(20,5,7),
AC5(20,5,7),AC6(20,5,7),AC7(20,5,7),
AC8(20,5,7),AC9(20,5,7),AC10(20,5,7),
AS1(20,5,7),AS2(20,5,7),AS3(20,5,7),AS4(20,5,7),
AS5(20,5,7),AS6(20,5,7),AS7(20,5,7),
AS8(20,5,7),AS9(20,5,7),AS10(20,5,7),
BB(36),XREF,RX
1
2
3
4
5
6
7
DIMENSION ZZZ(14050)
EQUIVALENCE (ZZZ,NAL)
1(VAL(5),P),(VAL(6),Q),(VAL(7),R),(VAL(8),PHI),(VAL(9),W),
2(VAL(10),Z),(VAL(11),BMASS),(VAL(21),X),(VAL(22),Y),(VAL(23),PSI),
3(VAL(24),P8)
DIMENSION TEMP(7),XMO(10)
DIMENSION ITILC(20)
DATA BEAM,BETAD,DELO,DELPI,DLRDO,DSO,ISYS,RMAXO,RCNO,RRATO,RREVO,
1 THETO,THSSI,TPRIND,UO,VXO,VZO,XBSI,XCPO,XLTOI,XPO,XRO,XSSI,YPO,
2 ZPO,ZRO,ZSSI/ 6*0.0,0,20*0.0/
DO 9 I=1,8
ISUM1(I)=0
ISUM2(I)=0
9 PINF=2116.
RHOINF=.002578
GAM=1.4
GO TO 10
2200 READ(5,3000) NGRAF,NDRW
3000 FCPMAT(212)
5001 READ(5,3001) NXYS
FURMAT(2612)
READ(5,3002) TICRD
COMMON /SLOPE/WATSLP,XPWV,XLXPWV,XPWVXS
CCMMCN/SOFTBS/XBF,PBS,SINBS,COSBS,XBS,ZBS,DELYBS,DPBS,ELMAXB,YAVG
18(10)
COMMON /SOFTSS/ XLF,PSS,SINTH,COSTH,XSS,ZSS,DELYSS,DPSS
1,ELMAXS,YAVGS(10)
COMMON /SIDE/FXSH,FYSW,FZSW,FKSW,FMSW,FNSW,ALSW,YSW,XLSW,CFSW,CDSW
1,VAREA,VCHORD,VSPAN,VANGLE,VCOS,VX,VY,VZ ,AVBMSW,DELX,VTC
COMMON /STABLE/ S(4),ISTAB
COMMON /STSLR/ CPHI,CPHID
COMMON /SUM/ ISUM1(3),ISUM2(8)
COMMON /VALOLD / YOLD(20)
COMMON /VARBLE/ VAL(40)
COMMON /WAVE/ ETA(4,11),AW(10),OMEGA(10),DVOLW,NWAVE,BETA,
FXWAV,FYWAV,FZWAV,FWWAV,FNWAV
ZBAR,PHIBAR,THEBAR,TC,COSBET,SINBET,PBBAR
COMMON /WAVEF/WAVLEN(10),OMEGAF(10),WAVSLP(10),ENCPER(10)
COMMON /WAVTAB/ NAL,DAL,SAL,NDS,SDS,NTH,DTH,STH,NBB,DBB,SBB,
AC1(20,5,7),AC2(20,5,7),AC3(20,5,7),AC4(20,5,7),
AC5(20,5,7),AC6(20,5,7),AC7(20,5,7),
AC8(20,5,7),AC9(20,5,7),AC10(20,5,7),
AS1(20,5,7),AS2(20,5,7),AS3(20,5,7),AS4(20,5,7),
AS5(20,5,7),AS6(20,5,7),AS7(20,5,7),
AS8(20,5,7),AS9(20,5,7),AS10(20,5,7),
BB(36),XREF,RX
1
2
3
4
5
6
7
DIMENSION ZZZ(14050)
EQUIVALENCE (ZZZ,NAL)
1(VAL(5),P),(VAL(6),Q),(VAL(7),R),(VAL(8),PHI),(VAL(9),W),
2(VAL(10),Z),(VAL(11),BMASS),(VAL(21),X),(VAL(22),Y),(VAL(23),PSI),
3(VAL(24),P8)
DIMENSION TEMP(7),XMO(10)
DIMENSION ITILC(20)
DATA BEAM,BETAD,DELO,DELPI,DLRDO,DSO,ISYS,RMAXO,RCNO,RRATO,RREVO,
1 THETO,THSSI,TPRIND,UO,VXO,VZO,XBSI,XCPO,XLTOI,XPO,XRO,XSSI,YPO,
2 ZPO,ZRO,ZSSI/ 6*0.0,0,20*0.0/
DO 9 I=1,8
ISUM1(I)=0
ISUM2(I)=0
9 PINF=2116.
RHOINF=.002578
GAM=1.4
GO TO 10
2200 READ(5,3000) NGRAF,NDRW
3000 FCPMAT(212)
5001 READ(5,3001) NXYS
FURMAT(2612)
READ(5,3002) TICRD

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3002 FORMAT(6A8)
10 READ(5,99) ISYSL,IOPT,(TEMP(1),I=1,7)
   IF( ISYSL .EQ. ISYS .AND. ISYSL.EQ. 13) GOTO 70
   ISYS=ISYSL
   IF((ISYS.LE.0).OR.(ISYS.GT.22)) GO TO 70
   GO TO(100,200,300,400,500,600,700,800,900,1000,1100,1200,1300,
11400,1500,1600,1700,1800,1900,2000,2100,2200),ISYS

C      PROGRAM CONTROL PARAMETERS
100 CONTINUE
   GO TO (101,102,103,104,105),IOPT
101 CONTINUE
   STIME=TEMP(1)
   FTIME=TEMP(2)
   DELO=TEMP(3)
   DELPNT=TEMP(4)
   TPRINO=TEMP(5)
   IF (TPRINO.LT.STIME+DELPNT) TPRINO = STIME+DELPNT
   IF (DELO.GT.DELPNT) DELO=DELPNT
   IF (DELO.EQ.0.0) GO TO 140
   GO TO 10
2000 READ(5,3003) NCURV
3003 FORMAT(10I1)
   GO TO 10
2100 READ(5,2210) ISUM1
2210 READ(5,2210) ISUM2
      FORMAT(8I2)
   GO TO 10
102 READ(5,191) IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,IRUD,
1 IPROP,IAEROD,IRHS
   GO TO 10
103 READ(5,175) NEQS,JQQ,(TOL(J),J=1,NEQS)
   GO TO 10
104 READ(5,191) IVERT,ILATRL,NVD,NVI,NLD,NLI
   GO TO 10
105 CONTINUE
   I3DOCF=TEMP(1)
   I3RGE=TEMP(2)
   ITRIM=TEMP(3)
   GO TO 10
140 WRITE(6,195)
      STOP

C      MASS DISTRIBUTION
200 G=32.17
   RHQ=1.09
   H*HQ=RHQ/2.
   GC TO (210,220,230), IOPT

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```

INCN0900
INCN0910
INCN0920
INCN0930
INCN0940
INCN0950
INCN0960
INCN0970
INCN0980
INCN0990
INCN1000
INCN1010
INCN1020
INCN1030
INCN1040
INCN1050
INCN1060
INCN1070
INCN1080
INCN1090
INCN1100
INCN1110
INCN1120
INCN1130
INCN1140
INCN1150
INCN1160
INCN1170
INCN1180
INCN1190
INCN1200
INCN1210
INCN1220
INCN1230
INCN1240
INCN1250
INCN1260
INCN1270
INCN1280
INCN1290
INCN1300
INCN1310
INCN1320
INCN1330
INCN1340
INCN1350
INCN1360
INCN1370

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```

210 IMM = 0
    WEIGHT = TEMP(1)
    AM = WEIGHT/G
    XS = TEMP(2)
    ZS = TEMP(3)
    AIXX = TEMP(4)
    AIYY = TEMP(5)
    AIZZ = TEMP(6)
    AIXZ = TEMP(7)
    INERTIA MATRIX OPERATIONS
C 212 DO 211 I=1,6
    DO 211 N=1,6
211 A(I,N) = 0.0
    DO 213 N=1,3
213 A(N,N)=AM
    A(4,4)=AIXX
    A(5,5)=AIYY
    A(6,6)=AIZZ
    A(4,6)=-AIXZ
    A(6,4)=-AIXZ
    AIMAX=AMAX1(AM,AIXX,AIYY,AIZZ,ABS(AIXZ))
    DO 214 I=1,6
    DO 214 J=1,6
214 A(I,J)=A(I,J)/AIMAX
    CALL DMINV(A,6,D)
    DO 215 I=1,6
    DO 215 J=1,6
215 A(I,J)=A(I,J)/AIMAX
    IF(D.NE.0.0) GO TO 10
    WRITE(6,216)
    STOP
C      WEIGHT DISTRIBUTION - ASSUME TRANSVERSE (PORT/STBD) SYMMETRY
C      READ X INPUT DIST. FWD. OF (SIDEWALL) TRANSOM
C      Y INPUT DIST. TO STARBOARD
C 220 I = 1
    Z INPUT DIST. UP FROM KEEL-LINE
222 READ(5,192) AMI(I),XI(I),YI(I),ZI(I)
    IF (AMI(I).LT.0.0) GO TO 224
    I = I+1
    IF (I.GT.201) GO TO 70
    GO TO 222
224 NMASS = I-1
    SUM = 0.0
    SUX = 0.0
    SUL = 0.0
    DO 225 I=1,NMASS
    AMI(I) = AMI(I)/G
    SUM = SUM+AMI(I)

```



```

225  SUX = SUX+AMI(I)*XI(I)
      AMZ = SUM*2.0
      WEIGHT = AM*G
      ZS = SUX/SUM
      XS = SUX/SUM
      SUM = 0.0
      SUX = 0.0
      SUY = 0.0
      SUZ = 0.0
      DU 226 I=1,NMASS
        XI(I) = XI(I)-XS
        ZI(I) = -ZI(I)+ZS
        AMK = AMI(I)*2.0
        SUX = SUX+AMK*XI(I)*XI(I)
        SUY = SUX+AMK*YI(I)*YI(I)
        SUZ = SUX+AMK*ZI(I)*ZI(I)
226  AIXX = SUX+SUZ
      AIYY = SUX+SUZ
      AIZZ = SUX+SUY
      AIXZ = SUM
      GO TO 212
230  GO TO 10

C 300  XX AND YY TABLES
      CONTINUE
      NSTA(1) = TEMP(1)
      NSTA(2) = TEMP(2)
      NSTA(3) = TEMP(3)
      NSTA(4) = TEMP(4)
      XLTOT=TEMP(5)
      GO TO 10

C 400  SIDEWALL (INCLUDING APPENDAGES)
      CONTINUE
      GO TO (401,402),IOPT
401  YSW=TEMP(1)
      XLSW=TEMP(2)
      CFSW=TEMP(3)
      CDSW=TEMP(4)
      AVBMSW=TEMP(5)
      READ (10) ZZZ
      REWIND 10
      GO TO 10
C 402  BLOCK 4 OPTION 2 REMOVED.
      CONTINUE
      GO TO 10

```

NO APENDAGES

INCN1860  
 INCN1870  
 INCN1880  
 INCN1890  
 INCN1900  
 INCN1910  
 INCN1920  
 INCN1930  
 INCN1940  
 INCN1950  
 INCN1960  
 INCN1970  
 INCN1980  
 INCN1990  
 INCN2000  
 INCN2010  
 INCN2020  
 INCN2030  
 INCN2040  
 INCN2050  
 INCN2060  
 INCN2070  
 INCN2080  
 INCN2090  
 INCN2100  
 INCN2110  
 INCN2120  
 INCN2130  
 INCN2140  
 INCN2150  
 INCN2160  
 INCN2170  
 INCN2180  
 INCN2190  
 INCN2200  
 INCN2210  
 INCN2220  
 INCN2230  
 INCN2240  
 INCN2250  
 INCN2260  
 INCN2270  
 INCN2280  
 INCN2290  
 INCN2300  
 INCN2310  
 INCN2320  
 INCN2330



```

C 500
STERNSEAL
CONTINUE
XSSI=TEMP(1)
ZSSI=TEMP(2)
ALEAK=TEMP(3)
CFSS=TEMP(4)
THSSI=TEMP(5)
DPSS=TEMP(6)
XLF=TEMP(7)
SINH=SIN(THSSI/RAD)
COSH=COS(THSSI/RAD)
ELMAXS=XLF*COSH
GO TO 10
INCN2340
INCN2350
INCN2360
INCN2370
INCN2380
INCN2390
INCN2400
INCN2410
INCN2420
INCN2430
INCN2440
INCN2450
INCN2460
INCN2470
INCN2480
INCN2490
INCN2500
INCN2510
INCN2520
INCN2530
INCN2540
INCN2550
INCN2560
INCN2570
INCN2580
INCN2590
INCN2600
INCN2610
INCN2620
INCN2630
INCN2640
INCN2650
INCN2660
INCN2670
INCN2680
INCN2690
INCN2700
INCN2710
INCN2720
INCN2730
INCN2740
INCN2750
INCN2760
INCN2770
INCN2780
INCN2790
INCN2800
INCN2810

C 600
BOWSEAL
CONTINUE
XBSSI=TEMP(1)
CPBS=TEMP(2)
DPBS=TEMP(3)
ZBSSI=TEMP(4)
THBSSI=TEMP(5)
XSF=TEMP(6)
BLEAK=TEMP(7)
SINBS=SIN(THBSSI/RAD)
COSBS=COS(THBSSI/RAD)
ELMAXB=XBF*COSBS
GO TO 10

C 700
PLENUM
CONTINUE
GO TO (705,710),IOPT
705
CONTINUE
XLBW=TEMP(1)
XBEW=TEMP(2)
XPWV=TEMP(3)
WIDTH=TEMP(4)
XL=TEMP(5)
XCPU=TEMP(6)
BUBHGT=TEMP(7)
XLXPHV=XLBW-XPWV
XPWVXS=XPWV-XS
ABW=XBOW*XLBW
A3=WIDTH*XL
VCLNUM=(ABW+AB)*BUBHGT/2.
GO TO 10
710
CONTINUE
FNCRI=TEMP(1)

```



```

      GO TO 10
C
800  PROPULSION
      CONTINUE
      GO TO (805,810),IOPT
805  CONTINUE
      XPO=TEMP(1)
      YPU=TEMP(2)
      ZPO=TEMP(3)
      GO TO 10
C BLOCK 8 OPTION 2 REMOVED. ENGINE OUT INPUT IN BLOCK 16
810  CONTINUE
      GOTO 10
C
900  RUDDER
      CONTINUE
      GU TO (905,910,915),IOPT
905  XRU = TEMP(1)
      YR = TEMP(2)
      ZR = TEMP(3)
      RSPAN=TEMP(4)
      RASPR=TEMP(5)
      RAREA=TEMP(6)
      RCLB=2.*PI*RASPR/(RASPR+3.)
      RTC=TEMP(7)
      GO TO 10
C
910  NOT USED
      CONTINUE
      GO TO 10
915  CONTINUE
      GOTO 10
C
1000 AERODYNAMICS
      CONTINUE
      XLAERO=TEMP(1)
      BEAM=TEMP(2)
      RHQA=.5*RHOINF*XLAERO*BEAM
      GOTO 10
C
1100 WAVES
      CONTINUE
      IKAWSN=IOPT
      NWAVE=TEMP(1)
      IF(NWAVE.EQ. 0) GOTO 10
      IF(NWAVE.GT. 10) GOTO 70
      BETAD=TEMP(2)
      BETAD=BETAD/RAD
      COSBET=COS(BETA)

```

```

INCN2820
INCN2830
INCN2840
INCN2850
INCN2860
INCN2870
INCN2880
INCN2890
INCN2900
INCN2910
INCN2920
INCN2930
INCN2940
INCN2950
INCN2960
INCN2970
INCN2980
INCN2990
INCN3000
INCN3010
INCN3020
INCN3030
INCN3040
INCN3050
INCN3060
INCN3070
INCN3080
INCN3090
INCN3100
INCN3110
INCN3120
INCN3130
INCN3140
INCN3150
INCN3160
INCN3170
INCN3180
INCN3190
INCN3200
INCN3210
INCN3220
INCN3230
INCN3240
INCN3250
INCN3260
INCN3270
INCN3280
INCN3290

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```

1104 SINBET=SIN(BETA)
1105 TC=1.0
1106 GOTO ( 1104,1106) ,IWAVSW
1107 DO 1105 I=1,NWAVE
READ(5,1190) GMEGA(I),AW(I)
GOTO 10
1106 DO 1107 I=1,NWAVE
1107 READ (5,1190) WAVLEN(I) ,AW(I)
GOTO 10

C INITIAL CONDITIONS
1200 CONTINUE
UD = TEMP(1)
THETO = TEMP(2)
DSO = TEMP(3)
DELP1=TEMP(4)
GO TO 10

1300 CONTINUE
INPUT COMPLETED. 1) PRINT ALL INPUT
WRITE(6,2004) ITILC
WRITE(6,2001) STIME,FTIME,DELO,TPRINO,DELPNT
WRITE(6,2002) IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,IRUD,
1 IPROP,IAERUD,IRHS
WRITE(6,2021) I3DOF,ISRGE,ITRIM,NVALID
WRITE(6,2003) NEQS, (TOL(J),J=1,NEQS)
WRITE(6,219) WEIGHT,XS,ZS,AIXX,AIYY,AIZZ,AIXZ
WRITE(6,217)A,AIMAX
WRITE(6,2018) NSIA
WRITE(6,490) YSW,XLSW,CFSW,CDSW,VANGLE,VSPAN,VCHORD,VXO,VY,VZO,
1 AVBMSW,VTC
WRITE(6,491) NAL,DAL,SAL,NDS,DDS,SDS,NTH,DTH,SIH,NBB,DBB,SBB
IF (IMM-GT.0) WRITE(6,1549) (XMD(J),J=1,IMNX)
WRITE(6,1519) IMM,IMNX,IMNY,IBMFI,BTIME,IMT
IF (IM1-GT.0) WRITE(6,1559) (YMI(J),J=1,IMNY)
WRITE(6,2010) XLBW,XBBW
WRITE(6,2011) XL,WIDTH,XCPO,VOLNDM,BUBHGT
WRITE(6,2020) DELPI
WRITE(6,2009) FNCRIT,XLTOT
WRITE(6,2028) ENBFAN,BRPM,ENMFAN,EMRPM,ENSFAN,SRPM
WRITE(6,2013) XRO,YR,ZRO,RCNO,RMAXO,RRATO,RREVO,DLRDO
1 ,KSPAN,RASPR,RAREA,KCLB,RTC
WRITE(6,2012) XPO,YPO,ZPO
WRITE(6,2027) XLAERO,BEAM
WRITE(6,2026) XBSI,CFBS,DPBS,ELMAXB
WRITE(6,2025) XSSI,ZSSI,ALAEAK,CFSS,THSSI,DPSS,XLF
WRITE(6,2017) UD,THETO,DSO
INCN3300
INCN3310
INCN3320
INCN3330
INCN3340
INCN3350
INCN3360
INCN3370
INCN3380
INCN3390
INCN3400
INCN3410
INCN3420
INCN3430
INCN3440
INCN3450
INCN3460
INCN3470
INCN3480
INCN3490
INCN3500
INCN3510
INCN3520
INCN3530
INCN3540
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INCN3570
INCN3580
INCN3590
INCN3600
INCN3610
INCN3620
INCN3630
INCN3640
INCN3650
INCN3660
INCN3670
INCN3680
INCN3690
INCN3700
INCN3710
INCN3720
INCN3730
INCN3740
INCN3750
INCN3760
INCN3770

```



AND 2) INITIALIZE VARIABLES FOR CALCS.

INC3780  
INC3790  
INC3800  
INC3810  
INC3820  
INC3830  
INC3840  
INC3850  
INC3860  
INC3870  
INC3880  
INC3890  
INC3900  
INC3910  
INC3920  
INC3930  
INC3940  
INC3950  
INC3960  
INC3970  
INC3980  
INC3990  
INC4000  
INC4010  
INC4020  
INC4030  
INC4040  
INC4050  
INC4060  
INC4070  
INC4080  
INC4090  
INC4100  
INC4110  
INC4120  
INC4130  
INC4140  
INC4150  
INC4160  
INC4170  
INC4180  
INC4190  
INC4200  
INC4210  
INC4220  
INC4230  
INC4240  
INC4250

```

C
  1302 DO 1302 I=1,40
        VAL(I) = 0.0
        U = UD*1.6878
        XSS = -(XS-XSSI)
        ZSS = ZS-ZSSI
        THETA = THETO/RAD
        THEQL = THEQA
        DS = DSO/12.
        Z = -ZS+DS
        ZEQUIL = Z
        PHIMAX = 0.
        TRULL = 0.
        IRDS = 0
        TL = 0.0
C      WAVE PARAMETERS TABLE
        IF(NWAVE .EQ.0) GOTO 1321
        AMPTC = 1.30287
        GOTO(1310,1315), I,WAVSW
  1310 DO 1311 I=1,NWAVE
        WAVLEN(I) = 2.*PI*G/(OMEGA(I)*OMEGA(I))
  1311 GOTO 1317
  1315 DO 1316 I=1,NWAVE
        OMEGA(I) = Sqrt(2.*PI*G/WAVLEN(I))
  1317 CONTINUE
C      CALCULATE INITIAL FREQUENCIES OF ENCOUNTER
        DO 1318 I=1,NWAVE
        WAVSLP(I) = 360.0*AW(I)/WAVLEN(I)
        OMEGAE(I) = 2.*PI*(Sqrt(G*WAVLEN(I)/(2.*PI))-U*COSBET)/WAVLEN(I)
        ENCPER(I) = 2.0*PI/OMEGAE(I)
        CONTINUE
  1318 WRITE (6,1191) NWAVE,BETAD,(OMEGA(I),OMEGAE(I),WAVLEN(I),AW(I),
        1 WAVSLP(I),ENCPER(I),I=1,NWAVE)
        GOTO 1322
  1321 WRITE (6,1192)
  1322 CONTINUE
        DO 1303 I=1,4
        DO 1303 N=1,11
        ETA(I,N) = 0.0
  1303 DVOLW = 0.0
        FXWAV = 0.0
        FYWAV = 0.0
        FZWAV = 0.0
        FXWAV = 0.0
        FWAV = 0.0
        ZBAR = Z

```



INCN4260  
 INCN4270  
 INCN4280  
 INCN4290  
 INCN4300  
 INCN4310  
 INCN4320  
 INCN4330  
 INCN4340  
 INCN4350  
 INCN4360  
 INCN4370  
 INCN4380  
 INCN4390  
 INCN4400  
 INCN4410  
 INCN4420  
 INCN4430  
 INCN4440  
 INCN4450  
 INCN4460  
 INCN4470  
 INCN4480  
 INCN4490  
 INCN4500  
 INCN4510  
 INCN4520  
 INCN4530  
 INCN4540  
 INCN4550  
 INCN4560  
 INCN4570  
 INCN4580  
 INCN4590  
 INCN4600  
 INCN4610  
 INCN4620  
 INCN4630  
 INCN4640  
 INCN4650  
 INCN4660  
 INCN4670  
 INCN4680  
 INCN4690  
 INCN4700  
 INCN4710  
 INCN4720  
 INCN4730

```

PHIBAR=PHI
THEBAR=THETA
TIME=TIME
DELT = DELO
TPRINT=TPRIND-DELPNT
PWVGN=4.*WEIGHT/(RHO*G*XLBW)
FNCON=SQRT(XLBW*G)
VX=VXO-XS
VZ = ZS-VZO
XP=XPO-XS
XR = XRO-XS
YP=YPO
ZP=ZS-ZPO
ZR = ZS-ZRO
IF (IMM.EQ. 0) GO TO 1305
DO 1304 J=1,IMNX
  1304 XMI(J) = XMO(J) - XS
  1305 CONTINUE
  XCP = XCP0-XS
  ZCP = ZS-BUBHGT
  XBS=XBSI-XS
  N=NSTA(3)
  ZBS=ZS-ZBSI
  DO 1364 J=1,N
    DELYBS=XBBW/(N-1)
    XX(3,J)=XBS-XSSI
    YY(3,J)=-0.5*XBBW+(J-1)*DELYBS
  1364 CONTINUE
    N=N-1
    DO 1367 J=1,N
      YAVGB(J)=(YY(3,J+1)+YY(3,J))/2.
    1367 CONTINUE
      N=NSTA(4)
      DELYSS=XBBW/(N-1)
      DO 1365 J=1,N
        XX(4,J)=-XS
        YY(4,J)=-.5*XBBW+(J-1)*DELYSS
      1365 CONTINUE
        N=N-1
        DO 1368 J=1,N
          YAVGS(J)=(YY(4,J+1)+YY(4,J))/2.
        1368 CONTINUE
          XBOW=XLTOT-XS
          N=NSTA(1)
          DELX=XBSI/(N-1)
          DO 1309 J=1,2
            1309 I=1,N
            XX(J,I)=(I-1)*DELX-XS
  
```



```

1309 YY(J,I) = YSW*(2*J-3)
      WRITE(6,1306) ((XX(J,N),N=1,11),(YY(J,N),N=1,11),J=1,4)
1366 FORMAT(/17H XX AND YY ARRAYS /14H PORT SIDEWALL /2(11F10.2/),
1 15H STBD. SIDEWALL /2(11F10.2/),9H BOW SEAL /2(11F10.2/),
2 11H STERN SEAL /2(11F10.2/))
      N=NSTA(1)-1
      DO 1308 I=1,N
1308   XAVG(I)=DELX*(2*I-1)/2.-XS
      CALL WAVES(TIME)

C INITIALIZE BUBBLE PRESSURE, ABSOLUTE (PSF)
PB=PINF+DELPI
PBBAR=DELPI
PBAR=DELPI
PSS=PB+DPSS
PBS=PB+DPBS
AB=ABW-(ABW-AB)*(ZS+Z/BUBHGT)
CF=.37/(U/FNCON)**1.5655981)
WATSLP=PBBAR*CF*PWVCON/WEIGHT
VOL=VOLNOM-.5*(AB+ABW)*(Z+ZS)-DVOLW
1+.5*WATSLP*XL*AS
BMASS=(PB/PINF)**(1./GAM)*VOL*RHOINF
WRITE(6,2023)
RETURN

C RUN TERMINATOR
1400 WRITE(6,98)
      STOP

C BENDING MOMENT
1500 GO TO (1510,1520,1530,1540), IGPT
1510 IMM = TEMP(1)
      IF (IMM.GT.3) GO TO 70
      IMNX = TEMP(2)
      IF (IMNX.GT.10) GO TO 70
      INNY = TEMP(3)
      IF (INNY.GT.7) GO TO 70
      IBMFIL = TEMP(4)
      BTIME = TEMP(5)
      IF (IMM.EQ.3) IMT = TEMP(6)
      GO TO 10
1520 DO 1521 J=1,7
1521   XMO(J) = TEMP(J)
      IF (IMNX.LE.7) GO TO 10
      READ 1522, (XMO(J),J=8,IMNX)
      GO TO 10
1530 DO 1531 J=1,INNY
1531   YHI(J) = TEMP(J)

```

```

INCN4740
INCN4750
INCN4760
INCN4770
INCN4780
INCN4790
INCN4800
INCN4810
INCN4820
INCN4830
INCN4840
INCN4850
INCN4860
INCN4870
INCN4880
INCN4890
INCN4900
INCN4910
INCN4920
INCN4930
INCN4940
INCN4950
INCN4960
INCN4970
INCN4980
INCN4990
INCN5000
INCN5010
INCN5020
INCN5030
INCN5040
INCN5050
INCN5060
INCN5070
INCN5080
INCN5090
INCN5100
INCN5110
INCN5120
INCN5130
INCN5140
INCN5150
INCN5160
INCN5170
INCN5180
INCN5190
INCN5200
INCN5210

```



GO TO 10	INCN5220
1540 CONTINUE	INCN5230
GO TO 10	INCN5240
1600 CONTINUE	INCN5250
GO TO(1605,1610,1615),IOPT	INCN5260
1605 CONTINUE	INCN5270
C VALUES INPUT FOR STBD SCREW	INCN5280
THST1=TEMP(1)	INCN5290
NPS=TEMP(2)	INCN5300
SHS=TEMP(3)	INCN5310
IF(NPS.EQ.0.0) GO TO 1609	INCN5320
READ(5,1950)(TIS(J),J=1,NPS)	INCN5330
READ(5,1950)(THSTS(J),J=1,NPS)	INCN5340
GO TO 10	INCN5350
1609 THST1=THST1	INCN5360
1610 CONTINUE	INCN5370
C VALUES INPUT FOR PORT SCREW	INCN5380
THST2=TEMP(1)	INCN5390
NPP=TEMP(2)	INCN5400
SHP=TEMP(3)	INCN5410
IF(NPP.EQ.0.0) GO TO 1614	INCN5420
READ(5,1950)(TIP(J),J=1,NPP)	INCN5430
READ(5,1950)(THSTP(J),J=1,NPP)	INCN5440
GO TO 10	INCN5450
1614 THST2=THST2	INCN5460
1615 CONTINUE	INCN5470
C VALUES INPUT FOR RUDDER	INCN5480
DELR=TEMP(1)	INCN5490
NPR=TEMP(2)	INCN5500
IF(NPR.EQ.0.0) GO TO 1616	INCN5510
READ(5,1950)(TIR(J),J=1,NPR)	INCN5520
READ(5,1950)(DELRUD(J),J=1,NPR)	INCN5530
GO TO 10	INCN5540
1616 DELRUD(1)=DELR	INCN5550
GO TO 10	INCN5560
1700 GO TO (1705,1710),IOPT	INCN5570
1705 NB=TEMP(1)	INCN5580
READ(5,1950)(TMEB(I),I=1,NB)	INCN5590
READ(5,1950)(DELB(I),I=1,NB)	INCN5600
GO TO 10	INCN5610
1710 NS=TEMP(1)	INCN5620
READ(5,1950)(TMES(I),I=1,NS)	INCN5630
READ(5,1950)(DETS(I),I=1,NS)	INCN5640
GOTO 10	INCN5650
C TITLE CARD (ALL 80 COLUMNS )	INCN5660
	INCN5670
	INCN5680
	INCN5690



1800	READ (5,2022)	TITLC	INC�5700
	GO TO 10		INC�5710
C	FAN MAPS		INC�5720
1900	CONTINUE		INC�5730
1905	GO TO (1905,1910,1915),IOPT		INC�5740
	CONTINUE		INC�5750
	ENBFAN=TEMP(1)		INC�5760
	BRPM=TEMP(2)		INC�5770
	NPTSB=TEMP(3)		INC�5780
	READIN=TEMP(4)		INC�5790
	IF (READIN.EQ. 0.0) GO TO 10		INC�5800
	READ (5,1950) (PBFAN(J),J=1,NPTSB)		INC�5810
	READ (5,1950) (QBFAN(J),J=1,NPTSB)		INC�5820
	GO TO 10		INC�5830
1910	CONTINUE		INC�5840
	ENMFAN=TEMP(1)		INC�5850
	EMKPM=TEMP(2)		INC�5860
	NPTSM=TEMP(3)		INC�5870
	READIN=TEMP(4)		INC�5880
	IF (READIN.EQ. 0.0) GO TO 10		INC�5890
	READ (5,1950) (PMFAN(J),J=1,NPTSM)		INC�5900
	READ (5,1950) (QMFAN(J),J=1,NPTSM)		INC�5910
	GO TO 10		INC�5920
1915	CONTINUE		INC�5930
	ENSFAN=TEMP(1)		INC�5940
	SRPM=TEMP(2)		INC�5950
	NPTSS=TEMP(3)		INC�5960
	READIN=TEMP(4)		INC�5970
	IF (READIN.EQ. 0.0) GO TO 10		INC�5980
	READ (5,1950) (PSFAN(J),J=1,NPTSS)		INC�5990
	READ (5,1950) (QSFAN(J),J=1,NPTSS)		INC�6000
	GO TO 10		INC�6010
1950	FORMAT(8F10.0)		INC�6020
C	ERROR IN INPUT		INC�6030
70	CONTINUE		INC�6040
	WRITE (6,79) ISYS		INC�6050
	STOP		INC�6060
79	FORMAT(34H INPUT ERROR - - STOP - - ISYS=,I3)		INC�6070
98	FORMAT(1H1,20(/),50X,19H COMPLETED ALL RUNS )		INC�6080
99	FORMAT(13,12,7F10.0)		INC�6090
191	FORMAT(16I5)		INC�6100
192	FORMAT(5F10.0)		INC�6110
195	FORMAT(//10X,65HERROR IN INPUT ---- DELT AND/OR DELPNT EQUALS ZERO		INC�6120
	1 ---- JOB ABORTED )		INC�6130
175	FORMAT(2I2/(8F10.0))		INC�6140
216	FORMAT(//10X,82HERROR IN INPUT ---- INPUT INERTIA ELEMENTS LEAD TO		INC�6150
	1 ZERO DETERMINANT --- JOB ABORTED )		INC�6160
			INC�6170



```

217 FORMAT(22H INERTIA MATRIX, A1MAX 6E15.4/((22X,6E15.4))
219 FORMAT(30H WEIGHT, C.G., INERTIA MOMENTS 7F12.3)
305 FCRMAT ( 11F7.0 )
490 FORMAT(15H SIDEWALL INPUT 12(F8.3,1X))
491 FORMAT(20H SIDEWALL TABLE PARAMETERS 4(I4,F7.3,F7.3))
1190 FORMAT(2F10.0)
1191 FORMAT(12HNO OF WAVES I2,I0H BETA(DEG)F5.0/15H OMEGA(RAD/SEC)
15X,10H OMEGAE(RAD/SEC) 5X,16H WAVE LFNGTH(FT) 5X,14H AMPLITUDE(FT)
- 5X,16H MAX SLOPE (DEG)5X,13HPERIOD,E(SEC)/(F8.4,12X,F8.4,4F20.3))
1192 FORMAT(11HOCALM WATER)
1519 FORMAT(32HOMOMENT CALC. CONTROL PARAMETERS 4I5, F8.3, I5 )
1522 FORMAT ( 5X,7F10.0)
1549 FORMAT(22H MOMENT CALCS. AT X OF 11F10.3)
1559 FORMAT(22H MOMENT CALCS. AT Y OF 11F10.3)
2004 FORMAT(33HISES MOTIONS AND LOADS PROGRAM - 20A4,/ )
2001 FORMAT(23H START AND FINISH TIMES 2F10.2/
- 22H INITIAL TIME INTERVAL F12.4/
- 18H START PRINTING AT F8.2,17H IN INCREMENTS OF F8.2)
2002 FORMAT(24H INTERMEDIATE PRINT IAGS 16I5)
2003 FCRMAT(39H NO. OF STATE EQUATIONS, AND TOLERANCES I5/(10X,10E12.2))
2009 FORMAT(23HOCRITICAL FROUDE NUMBER F15.4,5X,19H TOTAL CRAFT LENGTH
1 F15.4)
2010 FORMAT(34HOPLENUM, LENGTH AND WIDTH AT WATER 2F12.4)
2011 FURMAT(34H PLENUM, LENGTH AND WIDTH AT HULL 2F12.4/
- 35H PLENUM, CENTER OF PRESSURE AT HULL F12.4/
- 23H PLENUM, NOMINAL VOLUME F12.1,10X, 6HHEIGHT F12.4)
2012 FCRMAT(33H PROPUSSION, X, Y, Z COORDINATES 3F12.4/)
2013 FORMAT(28HORUDDER, X, Y, Z COORDINATES 3F12.4/
- 41H RUDDER, ON, MAX, RATE, REVERSE, INITIAL 5F12.4/
33H RUDDER, SPAN,ASPECT,AREA,CLB,T/C 5F12.4)
2017 FORMAT(39HINITIAL CONDITIONS: VELOCITY (KNOTS) = F7.2, 5X,
13HPITCH (DEG) = F8.3,5X,12HDRAFT (IN) = F8.2)
2018 FURMAT( 49H NUMBER OF STATIONS, SIDEWALLS (P+S), SEALS (B+S) ,4I5)
2020 FCRMAT( 38H PLENUM, INITIAL PRESSURE, GAGE (PSF) F8.2)
2021 FURMAT(79H PROGRAM OPTION SWITCH SETTINGS (LATERAL PLANE,CONSTANT
- SPEED, TRIM, VALIDATION) 4I5)
2022 FCRMAT (20A4)
2023 FCRMAT ( 1H1 )
2025 FCRMAT( 16H STERNSEAL INPUT 7F12.4 )
2029 FCRMAT( 16H BOWSEAL INPUT 7F12.4 )
2026 FURMAT( 19H0AERODYNAMICS INPUT 7F12.4)
2027 FCRMAT( 33H0FANS, NO. + RPM, BOW,MAIN,STERN 3(F10.0,F10.1))
2028 END

```

```

SUBROUTINE INTGRL (TIME)
INTEGER ON
COMMON /BMCO / IMM,IMNX,IMNY,IBMFIL,BTIME,IMT,XMI(10),YMI(7),IX,IYINT 0040
INT 0020
INT 0030

```



```

COMMON /EQNCO/ NEQS,TOL(20),JQQ
COMMON /KSWITCH/ ITHRST
COMMON /MASSES/ AM,AIXX,AIYY,AIZZ,AIXZ,AIMAX,G,WEIGHT,RHO,NMASS,
- AMI(20),XI(20),YI(20),ZI(20),XS,ZS,HRHO
COMMON /PRIME/ STIME,FTIME,DELT,DELPNT,IPRINT
COMMON /PRINT/ON,IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,
- IRUD,IPROP,IAEKOD,IRHS
COMMON /STABLE/ S(4),ISTAB
COMMON /STEP/ STEP2
COMMON /VALOLD / YOLD(20)
COMMON /VARELE/ VAL(40)
COMMON /VARELE/ VAL(1),X,(VAL(2),Y(1))
EQUIVALENCE (VAL(1),X),(VAL(2),Y(1))
DIMENSION Y(20),ERROR(20)
REAL K1(20),K2(20),K3(20),K4(20),K5(20)
DATA IPASS/0/
STEP2=1.0

```

```
STEP2=1.0  
PB=VAL(24)  
BMASS=Y(10)  
IF((TIME+DELT).LE.TPRINT) GO TO 12
```

DEL=DELTA  
DEL=TPRINT-TIME

PLEASE PRINT NAME

```
DO Z=1,NEQS  
  Y(J)=YOLD(J)
```

ITHRST=I

CALL K13(K1)  
I THRST=2

IF (IACCEL.NE. ON) GO TO 14

WRITE (6,101) ACCLAT ; DELT

ON-2  
H=DELT/3.

DO 3 J=1, NEQS

```
CALL RHS(K2)
```

$$Y(J) = YCD(J) + .5 * H * (K1(J) + K2(J))$$

1730x5+3111=11355.5\*DEL

$$Y(J) = YCLD(J) + .375 * H * (K1(J) + 3. * K3(J))$$
$$X = \text{TIME} + \text{COST}$$



```

6      DC 6 J=1,NEQS
      Y(J)=YOLD(J)+.5*H*(3.*K1(J)-9.*K3(J)+12.*K4(J))
      CALL RHS(K5)
      IF (JQQ.EQ.1) GO TO 7
      DO 7 J=1,NEQS
      ERROR(J)=(K1(J)-4.5*K3(J)+4.*K4(J)-.5*K5(J))*H/5.0
      IF (ABS(ERROR(J)).GT.TOL(J)) GO TO 11
7      CONTINUE
      DO 105 J=1,NEQS
      Y(J)=YOLD(J)+.5*H*(K1(J)+4.*K4(J)+K5(J))
      YOLD(J)=Y(J)
      TIME=TIME+DELT
      IF (IPASS.EQ.1) GO TO 8
      IF (JQQ.EQ.1) GO TO 10
      DO 75 J=1,NEQS
      IF (ABS(ERROR(J)).GT.TOL(J)/16.) GO TO 9
75      CONTINUE
      DELT=2.*DELT
      IF (DELT.GT.DELPNT) DELT=DELPNT
10      RETURN
9      STEP2=DELT
      GO TO 10
8      DELT=DEL
      IPASS=0
      GO TO 10
11      DELT=DELT/2.
      IF (DELT.LT: 1.E-6) GO TO 25
      IF (JQQ.EQ.2) GO TO 26
      WRITE (6,666) TIME,DELT,J,ERROR(J),TOL(J)
27      IPASS=0
      GO TO 15
26      STEP1=DELT*2.0
      IF (STEP1.LT.STEP2) STEP2=STEP1
      GO TO 27
25      WRITE (6,150)
      WRITE (6,100) TIME,DELT,(K1(J),J=1,NEQS),VAL
      STOP
100      FORMAT(/10X,23HINTGRL TIME,DELT,K1,VAL /2E15.4/2(5E15.4/),5(8E15.4/))
101      FORMAT(1H0,9X,33HTOTAL LATERAL ACCELERATION (G) = F12.4,
112X,5HD1 = E15.4)
150      FORMAT(1H1,10X,44HDELTA TIME LESS THAN 1.0E-6 - - JOB STOPS )
666      FORMAT(/10X,5HINT-J 2E30.5,15,2E20.5)
      END

```

```

INT 0520
INT 0530
INT 0540
INT 0550
INT 0560
INT 0570
INT 0580
INT 0590
INT 0600
INT 0610
INT 0620
INT 0630
INT 0640
INT 0650
INT 0660
INT 0670
INT 0680
INT 0690
INT 0700
INT 0710
INT 0720
INT 0730
INT 0740
INT 0750
INT 0760
INT 0770
INT 0780
INT 0790
INT 0800
INT 0810
INT 0820
INT 0830
INT 0840
INT 0850
INT 0860
INT 0870
INT 0880
INT 0890
INT 0900
INT 0910
INT 0920
INT 0930
INT 0940
INT 0950

```



```

SUBROUTINE PROP
  INTEGER ON
  COMMON /CONST/ PI,RAD,UO
  COMMON /FPROP/ FX,FY,FZ,EK,FM,FN
  COMMON /ENGINE/NPS,NPP,THSTS(25),THSTP(25),XP,YP,ZP,STHS,STHP,
  ATIP(25),TIS(25)
  COMMON /PRFINT/ON,IACCEL,IVEL,ITRAJ,ISIDL,IBOWSL,ISTNSL,IWAVES,
  -IRUD,IPROP,IAERUD,IRHS
  COMMON /RUDDR/ NPR,DELRUD(25),XR,YR,ZR,IRDS,TL,RSPAN,RAREA,RASPR,
  ARCLB,RTC,RUDANG,TIR(25)
  COMMON /VARIABLE/ VAL(40)
  EQUIVALENCE (VAL(1),TIME), (VAL(2),U), (VAL(3),V), (VAL(4),W),
  1(VAL(5),P), (VAL(6),Q), (VAL(7),R), (VAL(8),PHI), (VAL(9),THETA),
  2(VAL(10),Z), (VAL(11),BMASS), (VAL(21),X), (VAL(22),Y), (VAL(23),PSI),
  3(VAL(24),PB)
  DIMENSION THS(1),THP(1),TS(1),TP(1),RUD(1),TR(1)
  EQUIVALENCE (THSTS(1),THS(1)),(THSTP(1),THP(1)),(TIS(1),TS(1)),(TIP(1),TP(1)),(TIR(1),TIR(1)),(DELRUD(1),RUD(1))
  FX = 0.0
  FY = 0.0
  FZ = 0.0
  EK = 0.0
  FM = 0.0
  FN = 0.0
  TL=TIME
  IF(NPR.EQ.0.0) GO TO 5
  RUDANG=FG1(TL,NPR,TR,RUD,IR)
  RUDANG=RUDANG/RAD
  C CALCULATE THRUSTS AND MOMENTS INDIVIDUALLY
  GU TO 6
  5 RUDANG=DELRUD(1)
  RUDANG=RUDANG/RAD
  6 CU=COS(RUDANG)
  SD=SIN(RUDANG)
  IF(NPS.EQ.0.0) GO TO 2
  THSS=FG1(TL,NPS,TS,THS,IS)
  GC TO 4
  2 THSS=THSTS(1)
  4 IF(NPP.EQ.0.0) GO TO 3
  THSP=FG1(TL,NPP,TP,THP,IP)
  GU TO 1
  3 THSP=THSTP(1)
  1 THSTS=THS*THSS
  STHSTP=STHP*THSP
  FXS=THSS*CD-STHSTS*SD
  FXP=THSP*CD+STHSTP*SD
  FYS=-STHSTS*CD-THSS*SD
  FYP=STHSTP*CD+SD*THSP

```



```

FZS=-THSS*THETA*CD+STHSIS*SD*PHI
FZP=-THSP*THETA*CD-STHSTP*SD*PHI
FX=FXP+FXS
FY=FYP+FYS
FZ=FZP+FZS
FKP=-FZP*YP-FYP*ZP
FKS=FZS*YP-FYS*ZP
FK=FKS+FKP
FMS=FZS*(-XP)+FXS*ZP
FMP=FZP*(-XP)+FYP*ZP
FM=FMS+FMP
FNS=-FXS*YP-FYS*(-XP)
FNP=FXP*YP-FYP*(-XP)
FN=FNS+FNP
IF (IPKOP.NE.ON) RETURN
      WRITE(6,123)
123 FORMAT(/10X,22HPROP FX,FY,FZ,FK,FM,FN /6E15.4)
RETURN
END
PROP0490
PROP0500
PROP0510
PROP0520
PROP0530
PROP0540
PROP0550
PROP0560
PROP0570
PROP0580
PROP0590
PROP0600
PROP0610
PROP0620
PROP0630
PROP0640
PROP0650
PROP0660
PROP0670
PROP0680

```

```

SUBROUTINE RHS(VALUE)
INTEGER QN
COMMON /AIR/ PINF,RHOINF,GAM
COMMON /RMCQ/ IMM,IMNX,IMNY,IBMFIL,BTIME,IMT,XMI(10),YMI(7),IX,IY
COMMON /COLUMN/ IVERT,ILATRL
COMMON /CONST/ PI,RAD,UO
COMMON /CNTRL/CONTW,CONTH,CMULT,LOUVER,ACONTZ,ACONTW,ZEQUIL
1,THEQL,ACBASE
COMMON /ENGINE/NPS,NPP,THSIS(25),THSTP(25),XP,YP,ZP,STHS,STHP,
ATIP(25),TIS(25)
COMMON /FANMAP/QIN,QBFAN(25),QMFAN(25),QSFAN(25),ENBFAN,ENMFAN,
1,ESFAN,BRPM,NRPM,SRFM,NPTSB,NPTSM,NPTSS
2,PBFAN(25),PMFAN(25),PSFAN(25),TMEB(25),DELB(25),NB,TMES(25),
3,DEIS(25),NS
COMMON /FAERO/ FXAED,FYAED,FZAED,FKAED,FMAED,FNAED
COMMON /FORBS/FXBS,FYBS,FZBS,FKBS,FMBS,FNBS,QLBS
COMMON /FORSS/FXSS,FYSS,FZSS,FKSS,FMSS,FNSS,QLSS,FMS
COMMON /FPROP/ FXP,FYP,FZP,FKP,FMP,FNP
COMMON /FRUDE/ FN,FNCRIT
COMMON /FRUD/ FRUD,FYRUD,FZRUD,FKRUD,FMRUD,FNRUD
COMMON /GROW/ XBOW
COMMON /GEUH/ WIDTH,XL,XX(4,11),YY(4,11),NSTA(4),AB,VOLNOM
1,DELS(4,10),XCPO,ZCP
COMMON /GEOMBS/DETABX(11),DETABT(11),ARM1B(10),ARM2B(10)
1,DEBS(10),TSKIB(10)
COMMON /GEOTSS/DETADX(11),DETADT(11),ARM1S(10),DFSS(10),TSKIS(10)
RHS 0010
RHS 0020
RHS 0030
RHS 0040
RHS 0050
RHS 0060
RHS 0070
RHS 0080
RHS 0090
RHS 0100
RHS 0110
RHS 0120
RHS 0130
RHS 0140
RHS 0150
RHS 0160
RHS 0170
RHS 0180
RHS 0190
RHS 0200
RHS 0210
RHS 0220
RHS 0230
RHS 0240
RHS 0250
RHS 0260

```



```

1,ARM2S(10)
COMMON /KSWTCH/ ITHRST
COMMON /MASSES/ AM,AIXX,AIYY,AIZZ,AIXZ,AIMAX,G,WEIGHT,RHO,NMASS,
- AMI(201),XI(201),YI(201),ZI(201),XS,ZS,HRHO
COMMON /MATRIX/ A(6,6)
COMMON /MSIDW/ DF(2,10),DSWAV(2,10),FXH(2),FYH(2),FZH(2),FMH(2),
- FNH(2),VFY(2),VFZ(2),FXV
COMMON /MWAVE/ FXW(2),FYW(2),FZW(2),FKW(2),FMW(2),FNW(2)
COMMON /OPTION/ I3DDF,ISRGE,IIRIM,NVALID
COMMON /PLENUM/XL8W,XB8W,ABW,BUBHGT
COMMON /PRIME/ STIME,FTIME,DELT,DELPNT,TPRINT
COMMON /PRINT/ON,IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,
- IRUP,IPROP,IAERGD,IRHS
COMMON /PWAVE/ ENCON,PWVCON
COMMON/RUDDR/ NPR,DELRUD(25),XR,YR,ZR,IRDS,TL,RSPAN,RAREA,RASPR,
- ARCLB,RTG,RUDANG,TIR(25)
COMMON /SIDE/FXSW,FYSW,FZSW,FKSW,FNSW,ALSW,YSW,XLSW,CFSW,CDSW,RHS
1,VAREA /VCHORD,VSPAN,VANGLE,VCOS,VX,VY,VZ /AVBMSW,DELX,VTC
COMMON /SLOPE/WATSLP,XPHV,XLXPWV,XPHVXS
COMMON/ SOFTBS/XCF,PBS,SINBS,COSBS,XBS,ZBS,DELYBS,DPBS,ELMAXB,YAVG
1B(10)
COMMON /SOFTSS/ XLF,PSS,SINTH,COSTH,XSS,ZSS,DELYSS,DPSS
1,ELMAXS,YAVGS(10)
COMMON /VALOLD / YOLD(20)
COMMON /VARBLE/ VAL(40)
COMMON /WAVE/ ETA(4,11),AW(10),OMEGA(10),DVOLW,NWAVE,BETA,
- FXWAV,FYWAV,FZWAV,FKWAV,FMWAV,FNWAV
1 2,ZBAR,PHIBAR,THEBAR,TC,COSBET,SINBET,PBBAR
EQUIVALENCE (VAL(1),TIME),(VAL(2),J),(VAL(3),V),(VAL(4),W),
1(VAL(5),P),(VAL(6),Q),(VAL(7),R),(VAL(8),PHI),(VAL(9),THETA),
2(VAL(10),Z),(VAL(11),BMASS),(VAL(21),X),(VAL(22),Y),(VAL(23),PSI),
3(VAL(24),PB)
EQUIVALENCE (VAL(18),FANPWR)
DATA NOTIN /O/
DIMENSION ACCEL(3),ANGACL(3)
DIMENSION GF(6),VALUE(20)
DO 5 J=1,20
VALUE(J)=0.0
5 CALCULATION OF BUBBLE WAVE MAKING DRAG
FN=U/ENCON
CF=.37/(FN*.15655981)
FXPWAV=-PWVCON*PBBAR*CF
WATSLP=-FXPWAV/WEIGHT
AB=AB4-(ABW-(XL*WIDTH))*(ZS+Z)/BUBHGT
VCL=VOLNUM-.5*(AB+ABW)*(Z+ZS)-DVOLW
1+.5*WATSLP*XL*AB
P3=PI*NF*(BMASS/(VOL*RHOINF))**GAM
PBS=PB+DPBS
RHS 0270
RHS 0280
RHS 0290
RHS 0300
RHS 0310
RHS 0320
RHS 0330
RHS 0340
RHS 0350
RHS 0360
RHS 0370
RHS 0380
RHS 0390
RHS 0400
RHS 0410
RHS 0420
RHS 0430
RHS 0440
RHS 0450
RHS 0460
RHS 0470
RHS 0480
RHS 0490
RHS 0500
RHS 0510
RHS 0520
RHS 0530
RHS 0540
RHS 0550
RHS 0560
RHS 0570
RHS 0580
RHS 0590
RHS 0600
RHS 0610
RHS 0620
RHS 0630
RHS 0640
RHS 0650
RHS 0660
RHS 0670
RHS 0680
RHS 0690
RHS 0700
RHS 0710
RHS 0720
RHS 0730
RHS 0740

```



```

PSS=PB+DPSS
PBAR=PB-PINF
ABPB=PBAR*AB
FLOW=SQRT(2.*ABS(PBAR)/RHOINF)*SIGN(1.,PBAR)
QLSW=CFSW*ALSW*FLOW
CALL BOWSL
CALL STNSL

GF(1)=FXBS+FXSS+FXSW+FXRUD+FXP+FXWAV+FXAED
IF (1/THKST.NE.1/THK) GO TO 11
THSTS(1)=THSTS(1)-GF(1)/2.
THSTP(1)=THSTP(1)-GF(1)/2.
THST=THSTS(1)+THSTP(1)
GF(1)=0.0
11 CONTINUE
GF(2)=-R*U*AM+FYBS+FYSS+FYSW+FYRUD+FYP+FYWAV+FYAED
GF(3)=WEIGHT-ABPB +FZBS+FZSS+FZSW+FZRUD+FZP+FZWAV+FZAED
GF(4)=FXBS+FKSS+FKSW+FKRUD+FKP+FKWAV+FKAED +ABPB*PHI*(-Z)
XCP=XCPU
GF(5)=FMBSS+FMSW+FMKUD+FMP+FMWAV+FMAED +ABPB*(XCP-THETA*Z)
+FXPWAV*ZS
FMBUB=ABPB*(XCP-THETA*Z)
FMVAV=FXPWAV*ZS
GF(6)=FMBSS+FMSW+FMKUD+FNP+FMWAV+FNAED
IF (1/3DOF.NE.1) GO TO 100
GF(3)=0.0
GF(5)=0.0
100 CONTINUE
DO 1 I=1,6
VALUE(I)=0.0
DO 1 J=1,6
VALUE(I)=VALUE(I)+A(I,J)*GF(J)
1 CONTINUE
VALUE(7)=P
VALUE(8)=Q
VALUE(9)=W
IF (1/3DOF.EQ.1) GO TO 325
BUBPLE PRESSURE EQUATION
QOUT=QLBS+QLSS+QLSW
CALL FAN
QCNTRL=0.0
VALUE(10)=RHOINF*(QIN-QOUT-QCNTRL)
GO TO 236
325 CONTINUE
VALUE(10)=0.0
236 CONTINUE
WRITE DATA FILE FOR MOMENT AND SHEAR CALCS., IF REQUIRED
IF (1/3DOF.NE.1) GO TO 111

```



```

NBS = NSTA(3)-1
NSS = NSTA(4)-1
NSSL = NSS/2+1

- - -
- - -
- - -
X , FNBS, FNSS , (TSKIS(I),DFSS(I),I=NSSL,NSS)
Y , (TSKIB(I),DFBS(I),ARMIB(I),ARM2B(I),I=1,NBS)

111 CONTINUE
C CONSTANT LONGITUDINAL VELOCITY ( U )
IF (ISRGE .EQ.1) VALUE(1)=0.0
IF (ON.NE.1) RETURN
DO 2 I=1,3
ACCEL(I)=VALUE(I)/G
ANGACL(I)=VALUE(I+3)*RAD
2 CONTINUE
BXACC=ACCEL(3)-XBOW*VALUE(5)/G
STRACC=ACCEL(3)+XS*VALUE(5)/G
IF (IVERT.NE.ON) GO TO 10
ZD=Z+ZS
THETAR=THETA*RAD
10 IF (ILATRL.NE.ON) GO TO 15
DEPSI=PSI*RAD
RDEG=R*RAD
BETAS=-V/U*RAD
ACCLAT=(VALUE(2)+U*R)/G
DPHI=PHI*RAD
DRFT=12.0*ZD
VEL = 0.59249*U
DELR=KUDANG*RAD
IF (P.EQ.0.0) GO TO 115
TRADUS=U/R
GO TO 20
115 TRADUS=1.E3
20 WRITE(1) TIME, VAL(16), DRFT, THETAR, PBAR, BOWACC, ACCEL(3), FANPWR, DPHI,
1 DEPSI, ACCLAT, VEL, TRADUS, RDEG, X, Y, GIN, QOUT, GF(1), FXPWAV, GF(2), GF(3)
2 GF(4), GF(5), GF(6), DELRS
15 IF (IRHS .NE. ON) RETURN
WRITE(6,77) FMB3, FMSS, FMWAV, FMP, FMWAV, FMAED, FMBUB, FWAVZ
77 FORMAT(0,6X,5HFMB3=,E16.6,2X,5HFMBSS=,E16.6,2X,5HFMSW=,
A=16.6,/,0,6X,5HFMBUB=,E16.6,2X,6HFMBU=,E16.6,2X,6HFMBU=,E16.6,
B/,0,6X,6HFMAED=,E16.6,2X,6HFMBUB=,E16.6,2X,6HFMAVZ=,E16.6)
WRITE(6,401) FXPWAV
401 FORMAT(0,6X,7HFXPWAV=,E16.6)
WRITE(6,200) PBAR, FANPWR, QIN, QLBS, QL SW, QLSS
WRITE(6,215) Ad, VUL

```



```

WRITE(6,213) VALUE,VAL
WRITE(6,150) GF,ACCEL,ANGACL
WRITE(6,175) BOWACC,STNACC
200 FORMAT(/10X,3HRHS
120H GAGE PRESS. (PSF) = F7.2,5X,21HFAN POWER REQD (HP) = F8.2,
25X,27HFAN FLOW RATE (CU FT/SEC) = F9.2,
3//31H LEAKAGE FLOW RATES (CU FT/SEC) //11H BOW SEAL = F9.2,
411H SIDEWALL = F9.2,13H STERN SEAL = F9.2)
215 FORMAT(/13H PLENUM AREA= F9.2,10X,14HPLENUM VOLUME= F10.2)
213 FORMAT(/12H VALUE ARRAY 2(/10E13.4)/10H VAL ARRAY 4(/10E13.4))
150 FORMAT(/10X,24HTOTAL FORCES AND MOMENTS 6E12.4/10X,24HACCELERATIONRHS
-5 G,DEG/SEC2 6E12.4)
175 FORMAT(/10X,16HBOU ACCEL. (G) = E12.4,21H STERN ACCEL. (G) = E12RHS
-.4)
RETURN
END

```

```

SUBROUTINE RUDDER
INTEGER ON
COMMON /CONST/ PI,RAD,UO
COMMON /FRUD/ FX,FY,FZ,FK,FM,FN
COMMON /MASSES/ AM,AIXX,AIYY,AIZZ,AIXZ,AIMAX,G,WEIGHT,RHO,NMASS,
- AMI(201),XI(201),YI(201),ZI(201),XS,ZS,HRHO
COMMON /PRTINT/ON,IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,
- IRUD,IPROP,IAEROD,IRHS
COMMON/RUDDR/ NPR,DELRUD(25),XR,YR,ZR,IRDS,TL,RSPAN,KAREA,RASPR,
ARCCLB,RTC,RUDANG,TIR(25)
COMMON /VARBLE/ VAL(40)

EQUIVALENCE (VAL(1),TIME),(VAL(2),U),(VAL(3),V),(VAL(4),W),
1(VAL(5),P),(VAL(6),Q),(VAL(7),R),(VAL(8),PHI),(VAL(9),THETA),
2(VAL(10),Z),(VAL(11),BMASS),(VAL(21),X),(VAL(22),Y),(VAL(23),PSI),
3(VAL(24),PB)
EQUIVALENCE (DELRUD(1),RUD(1)),(TIR(1),TR(1))
DIMENSION RUD(1),TR(1)
EQUIVALENCE (VAL(18),FANPWR)
DATA ENU /1.28E-5/

C CALCULATE PROGRAMMED RUDDER DEFLECTION
IF(NPR.EQ.0.0) GO TO 5
GO TO 6
5 RUDANG=DELRUD(1)
RUDANG=RUDANG/RAD
GO TO 7
6 RUDANG=FG1(TL,NPR,TR,RUD,IR)
RUDANG=RUDANG/RAD

```



```

C      SIDE FORCE ON RUDDER
7      DSR=L+ZS-XR*THETA
      ENDFAC=(1.+DSR/(DSR+RSPAN))
      VH=V+XR*K-ZR*P
      QQ=HRHQ*U*U*RAREA
      EFFANG=RUDANG-ENDFAC*VH/U
      FY=2.*QQ*ENDFAC*RCLB*EFFANG
      DRAG FORCE UN RUDDER
      REY=U*(RAREA/RSPAN)/ENU
      CFR=.42/(ALOG10(REY)-.407)**2*.64
      PI3=PI/8.
      CD=2.*CFR+PI8*RTC*(1.+G*RSPAN/(U*U))+RCLB*EFFANG*EFFANG
      EX=-2.*CD*KAREA*HNHO*U*U
      FZ=0.
      FK=-ZR*FY
      FN=FX*ZR
      FN=X*FY
      IF (IRUD.NE.ON) RETURN
      WRITE(6,123)
123    FURMAT(/10X,24HRUDDER FX,FY,FZ,FK,FM,FN /6E15.4)
      RETURN
      END

```

```

RUD 0320
RUD 0330
RUD 0340
RUD 0350
RUD 0360
RUD 0370
RUD 0380
RUD 0400
RUD 0410
RUD 0420
RUD 0430
RUD 0440
RUD 0450
RUD 0470
RUD 0480
RUD 0490
RUD 0500
RUD 0510
RUD 0520
RUD 0530
RUD 0540
RUD 0550
RUD 0560

```

```

SUBROUTINE SAM
WRITE(6,10)
10  FORMAT(1H1,'YOU HAVE CALLED A DUMMY SAM SUBROUTINE.'/
110X,'CHANGE TO BHISES TO USE THE SAM SUBROUTINE.')
```

```

SAM 0020
SAM 0030
SAM 0040
SAM 0050
SAM 0060
SAM 0070

```

```

C      FUNCTION T1(X)
10     IF(ABS(X)-.1) 10,10,20
      T1=X*(1.-X*X/10.0)/3.
      RETURN
20     T1=(SIN(X)-X*COS(X))/(X*X)
      RETURN
      END

```

```

T1 0010
T1 0020
T1 0030
T1 0040
T1 0050
T1 0060
T1 0070
T1 0080

```

```

C      FUNCTION T2(X)
10     IF(ABS(X)-.1) 10,10,20
      T2=1.-X*X/6.
      RETURN

```

```

T2 0010
T2 0020
T2 0030
T2 0040
T2 0050

```



```

T2=SIN(X)/X
RETURN
END
T2      0060
T2      0070
T2      0080

```

```

SUBROUTINE SIDEWL
INTEGER UN
COMMON /AIR/ PINF,RHOINF,GAM
COMMON /BMCO / IMM,IMNX,IMNY,IBMFIL,BTIME,IMT,XMI(10),YMI(7),IX,IY
COMMON /CONST/ PI,RAD,UO
COMMON /GEOM/ WIDTH,XL,XX(4,11),YY(4,11),NSTA(4),AB,VOLNCM
1,DELS(4,10),XCP,ZCP
COMMON /GEOMSW/ XAVG(10),DS
COMMON /KSWTCH/ ITHRST
COMMON /MASSES/ AM,AIXX,AIYY,AIZZ,AIMAX,G,WEIGHT,RHO,NMASS,
- AMI(201),XI(201),YI(201),ZI(201),XS,ZS,HRHO
1,FNH(2),VFY(2),VFZ(2),FXV
COMMON /MSIDW/ DF(2,10),DSWAV(2,10),FXH(2),FZH(2),FMH(2),
COMMON /PLENUM/ XLBW,XBBW,ABW,BUBHGT
COMMON /PRIME/ STIME,ETIME,DELT,DELPNT,TPRINT
COMMON /PRINT/ ON,IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,
- IRUD,IPROP,IALEROD,IKHS
COMMON /SIDE/FX,FY,FZ,FK,FM,FN,ALSW,YSW,XLSW,CFSW,CDSW
1,VAREA,VCHORD,VSPAN,VANGLE,VCOG,VX,VY,VZ,AVBMSW,DELX,VIC
COMMON /SLOPE/WATSLP,XPWV,XLXPWV,XPWVXS
COMMON /VIBBLE/ VAL(40)
COMMON /WAVE/ ETA(4,11),AW(10),GMEGA(10),DVQLW,NWAVE,BETA,
FXWAV,FYWAV,FZWAV,FKWAV,FMWAV,FNWAV
1,ZBAR,PHIBAR,THEBAR,TC,COSBET,SINBET
COMMON /WAVTAB/ NAL,DAL,SAL,NDS,DDS,STH,NBB,DBB,SBB,
AC1(20,5,7),AC2(20,5,7),AC3(20,5,7),AC4(20,5,7),
AC5(20,5,7),AC6(20,5,7),AC7(20,5,7),
AC0(20,5,7),AC00(20,5,7),AC8(20,5,7),
AS1(20,5,7),AS2(20,5,7),AS3(20,5,7),AS4(20,5,7),
AS5(20,5,7),AS6(20,5,7),AS7(20,5,7),
AS0(20,5,7),AS00(20,5,7),AS8(20,5,7)
1,BB(36),XREF,KX
EQUIVALENCE
1,(VAL(5),P),(VAL(6),Q),(VAL(7),R),(VAL(8),PHI),(VAL(9),THETA),
2,(VAL(10),Z),(VAL(11),BMASS),(VAL(21),X),(VAL(22),Y),(VAL(23),PSI),
3,(VAL(24),PB)
DIMENSION GAP(2,11),DSW(2,11)
DATA ENU /1.28E-5/
PBHEAD=PBAR/(RHO*G)
GAP OR WETTED DRAFT CALCULATION
DO 10 J=1,2
N=I,STA(J)
SDWL0010
SDWL0020
SDWL0030
SDWL0040
SDWL0050
SDWL0060
SDWL0070
SDWL0080
SDWL0090
SDWL0100
SDWL0110
SDWL0120
SDWL0130
SDWL0140
SDWL0150
SDWL0160
SDWL0170
SDWL0180
SDWL0190
SDWL0200
SDWL0210
SDWL0220
SDWL0230
SDWL0240
SDWL0250
SDWL0260
SDWL0270
SDWL0280
SDWL0290
SDWL0300
SDWL0310
SDWL0320
SDWL0330
SDWL0340
SDWL0350
SDWL0360
SDWL0370
SDWL0380
SDWL0390
SDWL0400
SDWL0410
SDWL0420
SDWL0430

```



```

DD 10 K=1,N
DD=ZS+Z+YY(J,K)*PHI-XX(1,K)*THETA+ETA(J,K)
DDIN=DD-WATSLP*(XPWVXS-XX(J,K))
IF (DDIN.LT.8UBHGT) GO TO 101
IF ( VAL(1)-TOLD .LT. DELPNT ) GO TO 101
TOLD = VAL(1)
WRITE (6,100) XX(J,K), VAL(1), DD
100 FORMAT(/10X,43H WATER CONTACT WITH TOP OF BUBBLE CHAMBER AT F7.2,
-14H FT. TIME = F7.2,19H SEC. IMMERSION= F7.2,4H FT. )
101 CONTINUE
DSW(J,K)=(SIGN(1.,DD)+1.)*DD/2.
IF (DDIN) 6,8,8
IF (DSW(J,K)-PBHEAD) 7,8,8
7 GAP(J,K)=-DDIN*(1.-(DSW(J,K))/PBHEAD)
GO TO 10
8 GAP(J,K)=0.0
10 CONTINUE
LEAKAGE AREA
ALSW=0.0
DO 20 J=1,2
N=NSTA(J)-1
DO 20 I=1,N
ALSW=ALSW+(GAP(J,I)+GAP(J,I+1))*DELX/2.
20 CONTINUE

C
CROSS-FLOW DRAG ON SIDEWALLS
FYD=0.0
FKD=0.0
FND=0.0
DO 15 I=1,2
N=NSTA(I)-1
DO 15 J=1,N
DSWAV(I,J)=(DSW(I,J)+DSW(I,J+1))/2.
VREL = V+XAVG(J)*R-(ZS-DSWAV(I,J)/2.)*P
DF(I,J)=- HRHO*CDSW*VREL *ABS(VREL) *DELX *DSWAV(I,J)
FYD=FYD+DF(I,J)
FND=FND+DF(I,J)*XAVG(J)
FKD=FKD-(ZS-DSWAV(I,J)/2.)*DF(I,J)
SET UP STERN LIMIT OF FORCE DETERMINATION
XSS = -XS
GO TO 16
ENTRY SIDEWLM
XSS = XNI(IX)
IP=1.+(THETA*RAD-STH)/DTH
IP=MAXO(MINO(IP,NTH),1)
IPI=MINO(IP+1,NTH)
DTHETA=(IP-1)*DTH+STH
DIP= (THETA*RAD-DTHETA)/DTH

```



```

C      CALC REYNOLDS NO. AND DRAG COEFF.
      REY=U*XLW/ENU
      CDT=.427/(ALOG10(REY)-.407)**2.04

C      SIDEWALL FORCES, P/S
      DO 40 J=1,2
      WAREA=0.0
      N=NSTA(J)-1
      NI=(XSS+XS)*N/XLSW+1.5
      DO 21 I=NI,N
      ZORI=1.
      IF(DSWAV(J,I).EQ. 0.0) ZORI=0.0
      WAREA=WAREA+DELX*(2.*DSWAV(J,I)+ZORI*AVBMSW)
      FXH(J)=- HRHO*CDT*WAREA*U*U
      PM1=2*J-3
      YLSW=PM1*YSW
      DS=Z *ZS+YLSW*PHI
      DSS=DS-XSS*THETA
      ZORI=(SIGN(1.,DSS)+1.)/2.
      DSS=DSS*ZORI
      IDSS=1.5*(DSS-SBB)/DBB
      IUS=MINO(NBB,IDSS)
      BS=BB(1DSS)
      ZORI=(SIGN(1.,DSS)+1.)/2.
      DSS=USS*ZORI
      A33S=(RHG*PI*BS**2)/8.
      A22S=(KHO*.4*PI*DSS**2)/2.
      DSP=DS-(XREF-XS)*THETA
      IU=1.+(USR*12.-SDS)/ODS
      IU=MAXU(MINO(ID,NDS),1)
      DDSR=(ID-1)*DDS+SDS
      IUI=MINO(ID+1,NDS)
      DID=(DSR*12.-DDSR)/DDS
      BC0=AC0(1,ID,IP)
      BC2=AC2(1,ID,IP)
      BC5=AC5(1,ID,IP)
      BC6=AC6(1,ID,IP)
      BC0=BC0+UIU*(AC0(1,ID,IP)-BC0)+DIP*(AC0(1,ID,IP)-BC0)
1     BC0=BC0+UIU*(AC0(1,ID,IP)-BC0)+DIP*(AC0(1,ID,IP)-BC0)
1     BC2=BC2+UIU*(AC2(1,ID,IP)-BC2)+DIP*(AC2(1,ID,IP)-BC2)
1     BC5=BC5+UIU*(AC5(1,ID,IP)-BC5)+DIP*(AC5(1,ID,IP)-BC5)
1     BC6=BC6+UIU*(AC6(1,ID,IP)-BC6)+DIP*(AC6(1,ID,IP)-BC6)
1     I
SDWL0920
SDWL0930
SDWL0940
SDWL0950
SDWL0960
SDWL0970
SDWL0980
SDWL0990
SDWL1000
SDWL1010
SDWL1020
SDWL1030
SDWL1040
SDWL1050
SDWL1060
SDWL1070
SDWL1080
SDWL1090
SDWL1100
SDWL1110
SDWL1120
SDWL1130
SDWL1140
SDWL1150
SDWL1160
SDWL1170
SDWL1180
SDWL1190
SDWL1200
SDWL1210
SDWL1220
SDWL1230
SDWL1240
SDWL1250
SDWL1260
SDWL1270
SDWL1280
SDWL1290
SDWL1300
SDWL1310
SDWL1320
SDWL1330
SDWL1340
SDWL1350
SDWL1360
SDWL1370
SDWL1380
SDWL1390

```



```

C      SHIFT MOMENT CENTER FROM XREF TO C.G.
      BC00 = BC00-(XS-XREF)*BC0
      BC6  = BC6 -(XS-XREF)*BC5
C      HYDROSTATIC AND HYDRODYNAMIC FORCES
      FZH(J) =-G*BC0-U*U*A33S*THETA-U*A33S*W+Q*U*(-BC2+A33S*XSS)
1      FMH(J) =-U*XSS*XSS*A33S*Q+G*BC00+U*(A33S*XSS+BC2)*(W+U*THETA
1      +YLSN*P)
      FYH(J) =-A22S*U*(V+XSS*R -ZS*P)
      FNH(J) = FYH(J)*XSS-U*(V-ZS*P)*BC5+R*BC6)
      IF (IMT.EQ.2) GO TO 40
CONTINUE
      IF (IMT.EQ.2) RETURN
TOTAL SIDEWALL FORCES AND MOMENTS
FX=FXH(1)+FXH(2)
FY=FYH(1)+FYH(2)
FZ=FZH(1)+FZH(2)
FK=(FZH(2)-FZH(1))*YSW      +FKD -FY*ZS
FY=FY+FYD
FM=FMH(1)+FMH(2)+ZS*FX
FA= FND +FNH(1)+FNH(2) +(FXH(1)-FXH(2))*YSW
      IF (ISTOVL.NE.UN) RETURN
DO 41 I=1,2
DO 41 J=1,11
      GAP(I,J)=12.0*GAP(I,J)
41  OSW(I,J)=12.0*DSW(I,J)
      WRITE( 6,123) ((GAP(I,J),J=1,11),(DSW(I,J),J=1,11),I=1,2),
1  FX,FY,FZ,FK,FM,FN
123  FORMAT(/10X,8HSIDEWALL/25H GAP (FT.) (STERN TO BOW) /14H PORT SIDE
1EWALL /11F10.5/14H STBD SIDEWALL /11F10.5/37H IMMERSION DEPTH (FT.
2) (STERN TO BOW) /14H PORT SIDEWALL /11F10.5/14H STBD SIDEWALL /
3 11F10.5/10X,25HSIDEWALL FX,FY,FZ,FK,FM,FN /6E15.4)
      RETURN
END

SUBROUTINE STNSL
INTEGER CN
COMMON /AIR/ PINF,RHOINF,GAM
COMMON /CONST/ PI,RAD,UO
COMMON / FORSS/ FX,FY,FZ,FK,FM,FN,QL,FMS
COMMON /GEOM/ WIDTH,XL,XX(4,11),YY(4,11),NSTA(4),AB,VOLNOM
1,DELS(4,10),XCP,ZCP
COMMON /GEOMSS/DETADX(11),OETADT(11),ARMIS(10),DFSS(10),TSKIS(10)
1,ARMIS(10)
COMMON /KSWTCH/ ITHRST
COMMON/LEAKER/ ALEAK,CFSS

```

SDWL1400  
SDWL1410  
SDWL1420  
SDWL1430  
SDWL1440  
SDWL1450  
SDWL1460  
SDWL1470  
SDWL1480  
SDWL1490  
SDWL1500  
SDWL1510  
SDWL1520  
SDWL1530  
SDWL1540  
SDWL1550  
SDWL1560  
SDWL1570  
SDWL1580  
SDWL1590  
SDWL1600  
SDWL1610  
SDWL1620  
SDWL1630  
SDWL1640  
SDWL1650  
SDWL1660  
SDWL1670  
SDWL1680  
SDWL1690  
SDWL1700  
SDWL1710  
SDWL1720  
SDWL1730  
SDWL1740

SSL 0010  
SSL 0020  
SSL 0030  
SSL 0040  
SSL 0050  
SSL 0060  
SSL 0070  
SSL 0080  
SSL 0090  
SSL 0100  
SSL 0110



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COMMON /MASSES/ AM,AIXX,AIYY,AIZZ,AIXZ,AIMAX,G,WEIGHT,RHO,NMASS,
COMMON /PRINT/ON,IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,
- IRUD,IPROP,IAEROD,IRHS
COMMON /SLOPE/WATSLP,XPWV,XLXPWV,XPWVXS
COMMON /SOFTSS/ XLF,PSS,SINTH,CUSTH,XSS,ZSS,DELYSS,DPSS
1,ELMAXS,YAVGS(10)
COMMON /STSLK/ CPHI,CPHID
COMMON /VALOLD / YOLD(20)
COMMON /VARBLE/ VAL(40)
COMMON /WAVE/ ETA(4,11),AW(10),OMEGA(10),DVOLW,NWAVE,BETA,
1 FXWAV,FYWAV,FZWAV,FKWAV,FMWAV,FNWAV
2 ZBAR,PHIBAR,THEBAR,TC,COSBET,SINRET,PBBAR
EQUIVALENCE (VAL(1),TIME),(VAL(2),U),(VAL(3),V),(VAL(4),W),
1 (VAL(5),P),(VAL(6),Q),(VAL(7),R),(VAL(8),PHI),(VAL(9),THETA),
2 (VAL(10),Z),(VAL(11),BMASS),(VAL(2),X),(VAL(22),Y),(VAL(23),PSI),
3 (VAL(24),PB)
DIMENSION GAP(11),ELSKI(11)
DATA ENU,UWSKI,CLSKI / 1.28E-5, 0.0, 1.5703/
DO 5 J=1,11
GAP(J)=0.0
ELSKI(J)=0.0
CONTINUE
ALSS=0.0
FX=0.0
FZ=0.0
FK=0.0
FM=0.0
FN=0.0
DELP=PSS-PB
IF (DELP.LT.0.0) DELP=0.0
PBAR=PB-PINF
CALCULATE ELSKI HERE.
SINDIF=SINTH-COSTH*THETA
COSDIF=COSTH+SINTH*THETA
X1=XSS+ZSS*THETA-XLF*SINDIF
Z1=(-Z-ZSS+XSS*THETA-XLF*COSDIF)
CALCULATE GAP HERE.
N=NSTA(4)
DO 10 K=1,N
ELSKI(K)=(ETA(4,K)-DETADX(K)*(XX(4,K)-X1)-Z1)+YY(4,K)*PHI
1 XPWV*WATSLP
GAP(K)=-ELSKI(K)
IF (GAP(K) .LT. 0.0) GAP(K)=0.0
CONTINUE
N=NSTA(4)-1
DO 20 J=1,N
ELSKIA=(ELSKI(J+1)+ELSKI(J))/2.
10

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SSL 0120
SSL 0130
SSL 0140
SSL 0150
SSL 0160
SSL 0170
SSL 0180
SSL 0190
SSL 0200
SSL 0210
SSL 0220
SSL 0230
SSL 0240
SSL 0250
SSL 0260
SSL 0270
SSL 0280
SSL 0290
SSL 0300
SSL 0310
SSL 0320
SSL 0330
SSL 0340
SSL 0350
SSL 0360
SSL 0370
SSL 0380
SSL 0390
SSL 0400
SSL 0410
SSL 0420
SSL 0430
SSL 0440
SSL 0450
SSL 0460
SSL 0470
SSL 0480
SSL 0490
SSL 0500
SSL 0510
SSL 0520
SSL 0530
SSL 0540
SSL 0550
SSL 0560
SSL 0570
SSL 0580
SSL 0590

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IF (ELSKIA-LE.0.0) GO TO 15
IF (ELSKIA-GE.ELMAXS) ELSKIA=ELMAXS
ARM1S(J)=XX(4,J)+ELSKIA/2.
ARM2S(J)=ZS-ELSKIA
DFSS(J)=-DELP*ELSKIA*DELYSS
ARG=.5*RHO*U*U*ELSKIA*DELYSS
RESKI=U*ELSKIA/ENU
CDTSKI=.427/(ALUG10(RESKI)-.407)**2.64
TSKIS(J)=-ARG*CDTSKI
GO TO 18
15 DFSS(J)=0.0
TSKIS(J)=0.0
18 CONTINUE
FX=FX+TSKIS(J)
FZ=FZ+DFSS(J)
FX=FX+DFSS(J)*YAVGS(J)
FX=FX-DFSS(J)*ARM1S(J)+TSKIS(J)*ARM2S(J)
FX=FX-TSKIS(J)*YAVGS(J)
ALSS=ALSS+(GAP(J)+GAP(J+1))*DELYSS/2.0
20 CONTINUE
ALSS=ALSS+ALEAK
QL=CFSS*ALSS*SQR(2.*ABS(PBAR)/RHOINF)*SIGN(1.,PBAR)
IF (ISTNSL.NE.ON) RETURN
WRITE(6,100) GAP,ELSKI,FX,FY,FZ,FK,FM,FN
100 FORNAT(//12H STERN SEAL/26H GAP(FT.) PORT TO STBD. /11E11.3
1/28H ELSKI (FT.) PORT TO STBD. /11E11.3/10X,23HSTNSL FX,FY,FZ,FK
2,FM,FN /6E15.4)
RETURN
END

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```

SUBROUTINE WAVES(TIME)
INTEGER ON
COMMON /BNGO / IMM,IMNX,IMNY,IBMFIL,BTIME,IMT,XMI(10),YMI(7),IX,IY
COMMON /CONST/ PI,RAD,UO
COMMON /GEOG/ WIDTH,XL,XX(4,11),YY(4,11),NSTA(4),A8,VOLNCM
1,DELS(4,10),XCPO,ZCP
1,COMMON /GEOMBS/DETABX(11),DETABT(11),ARM1B(10),ARM2B(10)
1,DFBS(10),TSKIB(10)
1,COMMON /GEOMSS/DETAOX(11),DETAOT(11),ARMIS(10),DFSS(10),TSKIS(10)
1,ARM2S(10)
COMMON /MASSES/ AM,AIXX,AIYY,AIZZ,AIXZ,AIMAX,G,WEIGHT,RHQ,NMASS,
- AMI(201),XI(201),YI(201),ZI(201),XS,ZS,HRHO
COMMON /MWAVE/ FXW(2),FYW(2),FZW(2),FKW(2),FMW(2),FNW(2)
COMMON /PLENUM/XLBW,XBBW,ABW,BUBHGT
COMMON /PKTINT/ON,IACCEL,IVEL,ITRAJ,ISIDWL,IBOWSL,ISTNSL,IWAVES,
-IPFOP,IAEROD,IRHS
COMMON /RISER/ AMPTC

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WAVS0010
WAVS0020
WAVS0030
WAVS0040
WAVS0050
WAVS0060
WAVS0070
WAVS0080
WAVS0090
WAVS0100
WAVS0110
WAVS0120
WAVS0130
WAVS0140
WAVS0150
WAVS0160
WAVS0170

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COMMON /SIDE/FXSW,FYSW,FZSW,FKSW,FMSW,FNSW,ALSW,YSW,XLSW,CFSW,CDSW,WAVS0180
1,VAREA,VCHORD,VSPAN,VANGLE,VCOS,VX,VY,VZ,AVBMSW,DELX,VTC,WAVS0190
COMMON /WAVE/ VAL(40) FKWAV,FYWAV,FZWAV,FKWAV,FMWAV,FNWAV,WAVS0200
1, ZBAK,PHIBAR:THEBAR,TC,COSBET,SINBET,PBBAR,WAVS0210
2, NAL,DAL,SAL,NU,S,DDS,SUS,NTH,STH,NB,DBB,SBB,WAVS0220
1, AC1(20,5,7),AC2(20,5,7),AC3(20,5,7),AC4(20,5,7),WAVS0230
2, AC5(20,5,7),AC6(20,5,7),AC7(20,5,7),WAVS0240
3, AC0(20,5,7),AC00(20,5,7),AC3(20,5,7),WAVS0250
4, AS1(20,5,7),AS2(20,5,7),AS3(20,5,7),AS4(20,5,7),WAVS0260
5, AS5(20,5,7),AS6(20,5,7),AS7(20,5,7),WAVS0270
6, AS0(20,5,7),AS00(20,5,7),AS8(20,5,7),WAVS0280
7, BB(36),XREF,RX,WAVS0290
1, WCO(2),WCO0(2),WC1(2),WC2(2),WC3(2),WC4(2),WC5(2),WC6(2),WAVS0300
2, WC7(2),WC8(2),WAVS0310
1, WSO(2),WS0(2),WS1(2),WS2(2),WS3(2),WS4(2),WS5(2),WS6(2),WAVS0320
2, WS7(2),WS8(2),WAVS0330
1, EQUIVALENCE (VAL(16),ETACG)
2(VAL(5),P),(VAL(6),Q),(VAL(7),R),(VAL(8),PHI),(VAL(9),THETA),WAVS0340
3(VAL(10),Z),(VAL(11),BMAS),(VAL(21),X),(VAL(22),Y),(VAL(23),PSI),WAVS0350
EQUIVALENCE (VAL(16),ETACG)
IF (NWAVE.EQ.0) RETURN
XCP=XCP0
GAMMA=BETA-PSI
SIGMA=SIN(GAMMA)
CUGAM=COS(GAMMA)
FO=-X*COSBET-Y*SINBET
DVOLW=0.0
ETACG=0.0
N=NSTA(3)
DO 1 J=1,N
DETA6X(J)=0.0
CONTINUE
N=NSTA(4)
DO 2 J=1,N
DETAUX(J)=0.0
CONTINUE
DO 10 J=1,4
N=NSTA(J)
ETA(J,K)=0.0
DO 15 J=1,2
FKW(J)=0.0
FYW(J)=0.0
FZW(J)=0.0
FKW(J)=0.0

```



WAVS0660  
WAVS0670  
WAVS0680  
WAVS0690  
WAVS0700  
WAVS0710  
WAVS0720  
WAVS0730  
WAVS0740  
WAVS0750  
WAVS0760  
WAVS0770  
WAVS0780  
WAVS0790  
WAVS0800  
WAVS0810  
WAVS0820  
WAVS0830  
WAVS0840  
WAVS0850  
WAVS0860  
WAVS0870  
WAVS0880  
WAVS0890  
WAVS0900  
WAVS0910  
WAVS0920  
WAVS0930  
WAVS0940  
WAVS0950  
WAVS0960  
WAVS0970  
WAVS0980  
WAVS0990  
WAVS1000  
WAVS1010  
WAVS1020  
WAVS1030  
WAVS1040  
WAVS1050  
WAVS1060  
WAVS1070  
WAVS1080  
WAVS1090  
WAVS1100  
WAVS1110  
WAVS1120  
WAVS1130

```

FMW(J) = 0.0
FNW(J) = 0.0
15 CONTINUE
XSS = -XS
IF (IMT.EQ.2) XSS = XMI(IX)
IP = 1 + (THEBAR*RAD-STH)/DTH
IP=MAX0(MINO(IP,NTH),1)
IPI=MIN0(IP+1,NTH)
DTHETA=(IP-I)*DTH+STH
DIP= (THETA*RAD-DTHETA)/DTH
TIME RISE FACTOR FOR WAVE AMPLITUDE
AMPFAC=1.-EXP(-TIME/AMPTC)
DO 100 I=1,NWAVE
OM1=OMEGA(I)
OM2=OM1*UM1
XWK=OM2/G
AA=AV(I)*AMPFAC
FT= OM1*TIME+XWK*FO
AL=XWK*CUGAM
IAA= 1+(ABS(AL)-SAL)/DAL
IAA=MAX0(MINO(IAA,NAL),1)
IAAI=MIN0(IAA+1,NAL)
DAA= (IAA-1)*DAL+SAL
DALP= SIGN(1.,AL)
WAVE FORCES AND MOMENTS ON THE SIDEWALLS
DO 40 J=1,2
YLSW=(Z*J-3)*YSW
WE=FT+XWK*SIGAM*YLSW
ST= SIN(WE)
CT= COS(WE)
DS= ZBAR+ZS+YLSW*PHIBAR
DSR=DS-(XREF-XS)*THEBAR
ID=1.+(DSR*12.-SDS)/DDS
ID=MAX0(MINO(ID,NDS),1)
DDSR=(ID-1)*DDS +SDS
DIC=(DSR*12.-DDSR)/DDS
IDI=MIN0(ID+1,NDS)
DSS=DS-XSS*THEBAR
ZCRI=(SIGN(1.,DSS)+1.)/2.
DSS=DSS*ZCRI
IDSS=1.5+(DSS-SBB)/DBB
IDSS=MIN0(NBB,IDSS)
BS=SB(IDSS)
CK= COS(XWK*COGAM*XSS)
A33S=(RHO*PI*BS**2)/8.
SK= SIN(XWK*COGAM*XSS)
A22S=(RHO*.4*PI*DS**2)/2.

```



C  
A42S=0.0  
INTERPOLATION OF WAVE TABLES  
K=1  
L=1AA  
CONTINUE  
BC0=AC0(L, ID, IP)  
BC1=AC1(L, ID, IP)  
BC2=AC2(L, ID, IP)  
BC3=AC3(L, ID, IP)  
BC4=AC4(L, ID, IP)  
BC5=AC5(L, ID, IP)  
BC6=AC6(L, ID, IP)  
BC7=AC7(L, ID, IP)  
BC8=AC8(L, ID, IP)  
BS0=AS0(L, ID, IP)  
BS00=AS00(L, ID, IP)  
BS1=AS1(L, ID, IP)  
BS2=AS2(L, ID, IP)  
BS3=AS3(L, ID, IP)  
BS4=AS4(L, ID, IP)  
BS5=AS5(L, ID, IP)  
BS6=AS6(L, ID, IP)  
BS7=AS7(L, ID, IP)  
BS8=AS8(L, ID, IP)  
WCO(K)=BC0 + DID\*(AC0(L, ID, IP) - AC0(L, ID, IP) - BC0) + DIP\*(AC0(L, ID, IP) + BC0) - AC0(L, ID, IP) - BC0  
1 WCO0(K)=BC00 + DID\*(AC00(L, ID, IP) - AC00(L, ID, IP) - BC00) + DIP\*(AC00(L, ID, IP) + BC00) - AC00(L, ID, IP) - BC00  
1 W01(K)=BC1 + DID\*(AC1(L, ID, IP) - AC1(L, ID, IP) - BC1) + DIP\*(AC1(L, ID, IP) + BC1) - AC1(L, ID, IP) - BC1  
1 W02(K)=BC2 + DID\*(AC2(L, ID, IP) - AC2(L, ID, IP) - BC2) + DIP\*(AC2(L, ID, IP) + BC2) - AC2(L, ID, IP) - BC2  
1 W03(K)=BC3 + DID\*(AC3(L, ID, IP) - AC3(L, ID, IP) - BC3) + DIP\*(AC3(L, ID, IP) + BC3) - AC3(L, ID, IP) - BC3  
1 W04(K)=BC4 + DID\*(AC4(L, ID, IP) - AC4(L, ID, IP) - BC4) + DIP\*(AC4(L, ID, IP) + BC4) - AC4(L, ID, IP) - BC4  
1 W05(K)=BC5 + DID\*(AC5(L, ID, IP) - AC5(L, ID, IP) - BC5) + DIP\*(AC5(L, ID, IP) + BC5) - AC5(L, ID, IP) - BC5  
1 W06(K)=BC6 + DID\*(AC6(L, ID, IP) - AC6(L, ID, IP) - BC6) + DIP\*(AC6(L, ID, IP) + BC6) - AC6(L, ID, IP) - BC6  
1 W07(K)=BC7 + DID\*(AC7(L, ID, IP) - AC7(L, ID, IP) - BC7) + DIP\*(AC7(L, ID, IP) + BC7) - AC7(L, ID, IP) - BC7  
1 W08(K)=BC8 + DID\*(AC8(L, ID, IP) - AC8(L, ID, IP) - BC8) + DIP\*(AC8(L, ID, IP) + BC8) - AC8(L, ID, IP) - BC8  
1 W09(K)=BS0 + DID\*(AS0(L, ID, IP) - AS0(L, ID, IP) - BS0) + DIP\*(AS0(L, ID, IP) + BS0) - AS0(L, ID, IP) - BS0  
1 W000(K)=BS00 + DID\*(AS00(L, ID, IP) - AS00(L, ID, IP) - BS00) + DIP\*(AS00(L, ID, IP) + BS00) - AS00(L, ID, IP) - BS00

WAVS1140  
WAVS1150  
WAVS1160  
WAVS1170  
WAVS1180  
WAVS1190  
WAVS1200  
WAVS1210  
WAVS1220  
WAVS1230  
WAVS1240  
WAVS1250  
WAVS1260  
WAVS1270  
WAVS1280  
WAVS1290  
WAVS1300  
WAVS1310  
WAVS1320  
WAVS1330  
WAVS1340  
WAVS1350  
WAVS1360  
WAVS1370  
WAVS1380  
WAVS1390  
WAVS1400  
WAVS1410  
WAVS1420  
WAVS1430  
WAVS1440  
WAVS1450  
WAVS1460  
WAVS1470  
WAVS1480  
WAVS1490  
WAVS1500  
WAVS1510  
WAVS1520  
WAVS1530  
WAVS1540  
WAVS1550  
WAVS1560  
WAVS1570  
WAVS1580  
WAVS1590  
WAVS1600  
WAVS1610



```

1 +DID*(AS00(L,IDL,IPL)-AS00(L,IDL,IPL)-AS00(L,IDL,IPL)+BS00))
1 WS1 (K)=BS1 +DID*(AS1 (L,IDL,IPL)-BS1 (L,IDL,IPL)+BS1 (L,IDL,IPL)-BS1
1 WS2 (K)=BS2 +DID*(AS2 (L,IDL,IPL)-BS2 (L,IDL,IPL)+BS2 (L,IDL,IPL)-BS2
1 WS3 (K)=BS3 +DID*(AS3 (L,IDL,IPL)-BS3 (L,IDL,IPL)+BS3 (L,IDL,IPL)-BS3
1 WS4 (K)=BS4 +DID*(AS4 (L,IDL,IPL)-BS4 (L,IDL,IPL)+BS4 (L,IDL,IPL)-BS4
1 WS5 (K)=BS5 +DID*(AS5 (L,IDL,IPL)-BS5 (L,IDL,IPL)+BS5 (L,IDL,IPL)-BS5
1 WS6 (K)=BS6 +DID*(AS6 (L,IDL,IPL)-BS6 (L,IDL,IPL)+BS6 (L,IDL,IPL)-BS6
1 WS7 (K)=BS7 +DID*(AS7 (L,IDL,IPL)-BS7 (L,IDL,IPL)+BS7 (L,IDL,IPL)-BS7
1 WS8 (K)=BS8 +DID*(AS8 (L,IDL,IPL)-BS8 (L,IDL,IPL)+BS8 (L,IDL,IPL)-BS8
1 +DID*(AS9 (L,IDL,IPL)-AS8 (L,IDL,IPL)-AS8 (L,IDL,IPL)+BS8 ))
IF(K .EQ. 2) GOTO 42
K=2

```

```

L=IAA1
GOTO 41
BC0 = WC0 (1) +DIA*(WC0 (2) -WC0 (1))
BC00 = WC00 (1) +DIA*(WC00 (2) -WC00 (1))
BC1 = WC1 (1) +DIA*(WC1 (2) -WC1 (1))
BC2 = WC2 (1) +DIA*(WC2 (2) -WC2 (1))
BC3 = WC3 (1) +DIA*(WC3 (2) -WC3 (1))
BC4 = WC4 (1) +DIA*(WC4 (2) -WC4 (1))
BC5 = WC5 (1) +DIA*(WC5 (2) -WC5 (1))
BC6 = WC6 (1) +DIA*(WC6 (2) -WC6 (1))
BC7 = WC7 (1) +DIA*(WC7 (2) -WC7 (1))
BC8 = WC8 (1) +DIA*(WC8 (2) -WC8 (1))
BC9 = WC9 (1) +DIA*(WC9 (2) -WC9 (1))
BS0 = WS0 (1) +DIA*(WS0 (2) -WS0 (1))
BS1 = WS1 (1) +DIA*(WS1 (2) -WS1 (1))
BS2 = WS2 (1) +DIA*(WS2 (2) -WS2 (1))
BS3 = WS3 (1) +DIA*(WS3 (2) -WS3 (1))
BS4 = WS4 (1) +DIA*(WS4 (2) -WS4 (1))
BS5 = WS5 (1) +DIA*(WS5 (2) -WS5 (1))
BS6 = WS6 (1) +DIA*(WS6 (2) -WS6 (1))
BS7 = WS7 (1) +DIA*(WS7 (2) -WS7 (1))
BS8 = WS8 (1) +DIA*(WS8 (2) -WS8 (1))
SHIFT MOMENT CENTER FROM XREF TO C.G.
BC00 = BC0 - (XS-XREF)*BC0
BC3 = BC3 - (XS-XREF)*BC1
BC4 = BC4 - (XS-XREF)*BC2
BC6 = BC6 - (XS-XREF)*BC5
BS00 = BS0 - (XS-XREF)*BS1
BS3 = BS3 - (XS-XREF)*BS4

```

WAVS1620  
WAVS1630  
WAVS1640  
WAVS1650  
WAVS1660  
WAVS1670  
WAVS1680  
WAVS1690  
WAVS1700  
WAVS1710  
WAVS1720  
WAVS1730  
WAVS1740  
WAVS1750  
WAVS1760  
WAVS1770  
WAVS1780  
WAVS1790  
WAVS1800  
WAVS1810  
WAVS1820  
WAVS1830  
WAVS1840  
WAVS1850  
WAVS1860  
WAVS1870  
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WAVS1890  
WAVS1900  
WAVS1910  
WAVS1920  
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WAVS1950  
WAVS1960  
WAVS1970  
WAVS1980  
WAVS1990  
WAVS2000  
WAVS2010  
WAVS2020  
WAVS2030  
WAVS2040  
WAVS2050  
WAVS2060  
WAVS2070  
WAVS2080  
WAVS2090



```

BS4 = BS4 -(XS-XREF)*BS2
BS6 = BS6 -(XS-XREF)*BS5
C CALCULATE WAVE FORCES AND MOMENTS
FZC= BS1-XWK*G*(BS2+BS0)-U*QMI*(-A33S*CK-AL*BS2)
FZS= BC1-XWK*G*(BC2+BC0)+U*QMI*(-A33S*SK+AL*BC2)
FMC= BS3-XWK*G*(BS4+BS0)-U*QMI*(-A33S*XS*CK-BC2-AL*BS4)
FMS= BC3-XWK*G*(BC4+BC0)+U*QMI*(-A33S*XS*SK-BS2+AL*BC4)
FYS= XWK*G*(BS5+BS0)-U*QMI*(-A22S*CK-AL*BS5)
FNC= XWK*G*(BS6+BS0)-U*QMI*(-A22S*XS*SK-BS5+AL*BS6)
FNS= -XWK*G*(BS6+BS0)-U*QMI*(-A22S*XS*CK-BC5-AL*BS6)
FKC=XWK*G*(BC7-BC8)+U*QMI*(-A42S*SK+AL*BC8)
FKS= -XWK*G*(BS7-BS8)+U*QMI*(-A42S*CK-AL*BS8)
FZW(J)=FZW(J)-AA*(FZC*CT+FZS*ST)
FVK(J)=FVK(J)+AA*(FMC*CT+FMS*ST)
FVW(J)=FVW(J)-AA*(FVC*CT+FVS*ST)*SIGAM
FVW(J)=FVW(J)-AA*(FNC*CT+FNS*ST)*SIGAM
FVW(J)=FVW(J)-AA*(FKC*CT+FKS*ST)*SIGAM
FVR(J)=FVR(J)-2.*AA*RHU*G*BS*DS*SK*CT
40 CONTINUE
IF (LMT.EQ.2) GO TO 100
C WAVE ELEVATION AROUND THE SIDEWALLS AND SEALS
DO 20 J=1,4
N=NSTA(J)
DO 20 K=1,N
ETA(J,K)=ETA(J,K)+SIN(XWK*(-XX(J,K)*COGAM-YY(J,K)*SIGAM)+FT)*AA
20 CONTINUE
ETAGG=ETAGG+AA*SIN(FT)
N=NSTA(3)
DO 25 J=1,N
ARG=AA*COS(XWK*(-XX(3,J)*COGAM)+FT)
DETADX(J)=DETADX(J)-XWK*COGAM*ARG
25 CONTINUE
N=NSTA(4)
DO 30 J=1,N
ARG=AA*COS(XWK*(-XX(4,J)*COGAM)+FT)
DETADX(J)=DETADX(J)-XWK*COGAM*ARG
30 CONTINUE
C WAVE PUMPING
X1=XWK*XLBW*COGAM/2.
X2=XWK*XLBW*SIGAM/2.
FTT=FT-XWK*XCP*COGAM
DVCLN=DVOLW+AA*ABW*T2(X1)*T2(X2)*SIN(FTT)
100 CONTINUE
IF (LMT.EQ.2) RETURN
C TOTAL WAVE FORCES AND MOMENTS
FXAV=FXW(1)+FXH(2)
FYAV=FYW(1)+FYH(2)
WAVS2100
WAVS2110
WAVS2120
WAVS2130
WAVS2140
WAVS2150
WAVS2160
WAVS2170
WAVS2180
WAVS2190
WAVS2200
WAVS2210
WAVS2220
WAVS2230
WAVS2240
WAVS2250
WAVS2260
WAVS2270
WAVS2280
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WAVS2490
WAVS2500
WAVS2510
WAVS2520
WAVS2530
WAVS2540
WAVS2550
WAVS2560
WAVS2570

```



```

FZWAV=FZW(1)+FZW(2)+(FZW(2)-FZW(1))*YSW      +FYWAV*ZBAR
FKWAV=FKW(1)+FKW(2)-(FKW(2)-FKW(1))*ZBAR
FMWAV=FMW(1)+FMW(2)+(FMW(1)-FMW(2))*YSW
FNWAV=FNW(1)+FNW(2)+FNW(2))*YSW
IF (IWAVES.NE.ON) RETURN
WRITE(6,200) ((ETA(I,J),J=1,11),I=1,4),ETACG,DVOLW
1,FXWAV,FYWAV,FZWAV,FKWAV,FMWAV,FNWAV,RELATIONS AT CRAFT STATIONS RELATIV
200 1E TO CALM WATER (FT.) /14H WAVE ELEVATIONS AT CRAFT STATIONS RELAT
2L /11F10.5/9H BOW SEAL /11F10.5/14H PORT SIDEWALL /11F10.5/14H STBD
3L ELEVATION AT C.G. = F10.5,10X,43HPLENUM VOLUME LOST DUE TO WAVES (C
4U.FT.) = F15.5/10X,23HWAVES,FX,FY,FZ,FK,FM,FN /6E15.4)
RETURN
END
WAVS2580
WAVS2590
WAVS2600
WAVS2610
WAVS2620
WAVS2630
WAVS2640
WAVS2650
WAVS2660
WAVS2670
WAVS2680
WAVS2690
WAVS2700
WAVS2710

```



# SAMPLE INPUT DATA DECK

00101	0.0	10.0	.01	.05					
00102									
00103									
1002	.0002	.0000001	.0001	.00001	.000000001.000000001				
.0001	.0001								
00104	1								
00105	6050.0	10.05	2.54	2870.0	9320.0	10580.0	-2800.		
00201	11.0	11.0	5.0	5.0	24.7				
00301	5.37	21.9	7	1.28	63.4	1.0	4.06		
00401	3.57	1.875	26.0	0.30	63.4	4.06	0.1		
00501	23.44	0.9	1.0	1.375	20.0	10.40	1.915		
00601	20.0	10.0	17.2	10.0					
00701	0.556	5.55	-0.604	275.0	0.0				
00801	-1.275	5.55	-0.208	1.21	2.15	.68	.167		
00901	-1.125	10.0							
01001	20.0								
01101	19.6	2.0	11.5	22.33					
01201	230.		.01						
01301	230.		.01						
01401	4.1								
01501									
01601									
01701									
01801									
01901	4.0	4.0	14.0	18.5	22.0	25.0	26.0		
02001	27.0	27.0	33.0	34.0	34.0	35.0	35.5		
02101	32.0	32.0	40.0	41.0	42.0	43.0	44.0		
02201	143.75	137.5	131.25	118.75	112.5	106.25	100.0		
02301	93.75	87.5	81.25	68.75	62.5	56.25	50.0		
02401	43.75	37.5	31.25	18.75	12.5	6.25	0.0		
02501	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
02601	27.0	27.0	33.0	34.0	34.0	35.0	35.5		
02701	32.0	32.0	40.0	41.0	42.0	43.0	44.0		
02801	143.75	137.5	131.25	118.75	112.5	106.25	100.0		
02901	93.75	87.5	81.25	68.75	62.5	56.25	50.0		
03001	43.75	37.5	31.25	18.75	12.5	6.25	0.0		
03101	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
03201	27.0	27.0	33.0	34.0	34.0	35.0	35.5		
03301	32.0	32.0	40.0	41.0	42.0	43.0	44.0		
03401	143.75	137.5	131.25	118.75	112.5	106.25	100.0		
03501	93.75	87.5	81.25	68.75	62.5	56.25	50.0		
03601	43.75	37.5	31.25	18.75	12.5	6.25	0.0		
03701	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
03801	27.0	27.0	33.0	34.0	34.0	35.0	35.5		
03901	32.0	32.0	40.0	41.0	42.0	43.0	44.0		
04001	143.75	137.5	131.25	118.75	112.5	106.25	100.0		
04101	93.75	87.5	81.25	68.75	62.5	56.25	50.0		
04201	43.75	37.5	31.25	18.75	12.5	6.25	0.0		
04301	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
04401	27.0	27.0	33.0	34.0	34.0	35.0	35.5		
04501	32.0	32.0	40.0	41.0	42.0	43.0	44.0		
04601	143.75	137.5	131.25	118.75	112.5	106.25	100.0		
04701	93.75	87.5	81.25	68.75	62.5	56.25	50.0		
04801	43.75	37.5	31.25	18.75	12.5	6.25	0.0		
04901	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
05001	27.0	27.0	33.0	34.0	34.0	35.0	35.5		
05101	32.0	32.0	40.0	41.0	42.0	43.0	44.0		
05201	143.75	137.5	131.25	118.75	112.5	106.25	100.0		
05301	93.75	87.5	81.25	68.75	62.5	56.25	50.0		
05401	43.75	37.5	31.25	18.75	12.5	6.25	0.0		
05501	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
05601	27.0	27.0	33.0	34.0	34.0	35.0	35.5		
05701	32.0	32.0	40.0	41.0	42.0	43.0	44.0		
05801	143.75	137.5	131.25	118.75	112.5	106.25	100.0		
05901	93.75	87.5	81.25	68.75	62.5	56.25	50.0		
06001	43.75	37.5	31.25	18.75	12.5	6.25	0.0		



26.0  
35.5  
44.0  
100.0  
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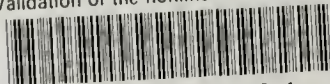
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